Environmental Technology Verification Report

NO_x Control Technologies

Catalytica Combustion Systems, Inc. XononTM Flameless Combustion System

Prepared by





Under a Cooperative Agreement with





THE ENVIRONMENTAL TECHNOLOGY VERIFICATION PROGRAM







U.S. Environmental Protection Agency

Research Triangle Institute

ETV Joint Verification Statement

TECHNOLOGY TYPE: NO_x AIR POLLUTION CONTROL TECHNOLOGY

APPLICATION: A PROCESS-INHERENT NO_x EMISSION CONTROL SYSTEM

FOR GAS TURBINE APPLICATIONS

TECHNOLOGY NAME: XONONTM COOL COMBUSTION

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The U.S. Environmental Protection Agency (EPA) has created the Environmental Technology Verification (ETV) Program to facilitate the deployment of innovative or improved environmental technologies through performance verification and dissemination of information. The goal of the ETV Program is to further environmental protection by substantially accelerating the acceptance and use of improved and cost-effective technologies. ETV seeks to achieve this goal by providing high-quality, peer-reviewed data on technology performance to those involved in the design, distribution, financing, permitting, purchase, and use of environmental technologies.

ETV works in partnership with recognized standards and testing organizations; with stakeholder groups that consist of buyers, vendor organizations, permitters, and other interested parties; and with the full participation of individual technology developers. The program evaluates the performance of innovative technologies by developing test plans that are responsive to the needs of stakeholders, conducting field or laboratory tests (as appropriate), collecting and analyzing data, and preparing peer-reviewed reports. All evaluations are conducted in accordance with rigorous quality assurance protocols to ensure that data of known and adequate quality are generated and that the results are defensible.

The Air Pollution Control Technology (APCT) program, one of 12 technology areas under ETV, is operated by the Research Triangle Institute (RTI) in cooperation with EPA's National Risk Management Research Laboratory. Midwest Research Institute, on behalf of the APCT program, has evaluated the performance of a nitrogen oxides (NO_x) control technology utilizing flameless catalytic combustion for stationary gas turbines, XononTM Cool Combustion (formally known as XononTM flameless combustion.)

VERIFICATION TEST DESCRIPTION

All tests were performed in accordance with general guidance given by the APCT program "Generic Verification Protocol for NO_x Control Technologies for Stationary Combustion Sources" and the specific technology test plan "Verification Test/QA Plan for XononTM flameless combustion system." These documents include requirements for quality management, quality assurance, auditing of the test laboratories, and test reporting format.

XononTM

The XononTM Cool Combustion system was tested as installed and operating on a Kawasaki M1A-13A gas-turbine-generator set (1.5 MW) located in Santa Clara, California, on July 18 and 19, 2000. NO_x concentrations were measured using continuous emission monitors (CEMs) following EPA Reference Method 20 for gas turbines. Other gaseous emissions were monitored using the applicable EPA test method. Other process variables were monitored using calibrated plant instrumentation.

Tests were conducted to meet the data quality objective of a 95 percent confidence interval with a width of ± 10 percent or less of the mean NO_x emission concentration for concentrations above 5 ppmvd, ± 25 percent or less below 5 ppmvd and above 2 ppmvd, and ± 50 percent or less below 2 ppmvd. In addition to outlet NO_x concentration and the primary process variables, carbon monoxide and unburned hydrocarbon emission concentrations were also measured using EPA reference methods, and the installation efforts, site modifications, staffing, maintenance requirements, and similar issues were noted qualitatively.

A single test run consisted of measuring outlet NO_x concentration and the other parameters over a 32-min steady-state process condition with the primary variable, ambient temperature, at either its low point or high point (i.e., early morning or late afternoon). The test design was a replicated 2×1 factorial using two levels of ambient temperature and greater than 97 percent of the rated full load. A total of 12 test runs were conducted over the 2-day field test period. Ambient temperature variation was small over the test period. Table 1 gives the operating performance envelope over which the XononTM Cool Combustion system was verified.

Verification Statement Table 1. Verification Test Performance Envelope^a

	Ambient Temperature, °C
Low	15
High	25

^aAt >97 percent of full turbine load.

DESCRIPTION OF XONONTM TECHNOLOGY

This verification statement is applicable to the XononTM Cool Combustion system for gas turbine applications without the air management system. The XononTM Cool Combustion system is completely contained within the combustion chamber of the gas turbine. XononTM Cool Combustion completely combusts fuel to produce a high-temperature mixture, typically about 1300 °C (2400°F). Dilution air is added to shape the temperature profile required at the turbine inlet.

The XononTM Cool Combustion system consists of four sections:

- **Preburner.** The preburner is used to preheat the air before it enters the catalyst module and during startup for acceleration of the turbine. The preburner tested as part of this verification was a lean, premixed combustor.
- Fuel injection and fuel/air mixing system. This unit injects the fuel and mixes it with the main air flow to provide a very well mixed, uniform fuel/air mixture to the catalyst.
- **Xonon**[™] **catalyst module.** In the catalyst module, a portion of the fuel is combusted without a flame to produce a high-temperature gas.
- **Homogeneous combustion region.** Located immediately downstream of the catalyst module, the homogeneous combustion region is where the remainder of the fuel is combusted, and carbon monoxide and unburned hydrocarbons are reduced to very low levels (also a flameless combustion process).

XononTM

The overall combustion process in the XononTM system is a partial combustion of fuel in the catalyst module followed by complete combustion downstream of the catalyst in the burnout zone. Partial combustion within the catalyst produces no NO_x . Homogeneous combustion downstream of the catalyst usually produces no NO_x , because combustion occurs at a uniformly low temperature. A small amount of fuel is combusted in the preburner to raise the compressed air temperature to about 470° C (880° F). NO_x in the turbine exhaust is usually from the preburner.

The design of each XononTM combustor is customized to the particular turbine model and operating conditions of the application and would typically be defined through a collaborative effort with the manufacturer of the turbine to integrate the hardware into the design. Catalytica Energy Systems, Inc. expects that the XononTM Cool Combustion technology incorporated in a XononTM combustion system for a natural-gas-fueled Kawasaki M1A-13A gas turbine is capable of achieving emissions of NO_x of less than 2.5 ppmvd (corrected to 15 percent oxygen $[O_2]$) on a 1-hour rolling average basis, and less than 2.0 ppmvd (corrected to 15 percent O_2) on a 3-hour rolling average basis. Under the same conditions, the XononTM combustion system is expected to achieve carbon monoxide (CO) emissions of less than 6 ppmvd (corrected to 15 percent O_2). The footprint may vary depending on the implementation, although generically the XononTM combustion system would likely be somewhat larger than the combustor that is typically supplied as standard equipment by the turbine manufacturer. Each unit could have multiple fuel inputs from separate control valves, and additional instrumentation for control and monitoring would be integrated into the turbine control system.

This verification statement covers application of the XononTM Cool Combustion system to small gas turbines operated at full load when combusting natural gas within the stated operating condition envelope. This unit was operated at the test site by the vendor, Catalytica Energy Systems, Inc., for over 4,000 hours before the verification test. Data from this long-term operating period have been submitted to a number of regulatory authorities for their review and evaluation. While these data and the instruments used were not verified during this test, within the operating condition envelope the results are generally consistent with the verification test results. Catalytica Energy Systems, Inc. should be contacted for these data or other information.

VERIFICATION OF PERFORMANCE

The verified NO_x emission results are given in Table 2. The analysis of variance between NO_x and ambient temperature indicated that ambient temperature did not affect NO_x emissions over the narrow range encountered during this verification test.

Verification Statement Table 2. NO_x Control Performance

Ambient Temperature Range	Percent of Full Turbine Load Range	Mean Outlet NO _x Concentration ppmvd @ 15% O ₂	Half-Width of 95% Confidence Interval on Mean Outlet NO _x ppmvd @ 15% O ₂
15 to 25°C (59 to 77°F)	98-99%	1.13	0.026

ppmvd = parts per million by volume dry basis.

CO emissions averaged 1.36 ppmvd at 15 percent O₂. Unburned hydrocarbon (UHC) emissions averaged 0.16 ppmv (wet basis reported as propane).

XononTM

The APCT quality assurance (QA) Officer has reviewed the test results and quality control data and has concluded that data quality objectives given in the NO_x Control Technology generic verification protocol and test/QA plan have been attained. During the verification tests, the EPA and APCT QA staffs conducted a performance evaluation and a technical system audit at the field test site, which confirm that the verification test was conducted in accordance with the EPA-approved test/QA plan.

This verification statement verifies the NO_x emissions characteristics of the XononTM Cool Combustion system within the range of application tested (see Table 2). Extrapolation outside that range should be done with an understanding of the scientific principles that control the performance of the XononTM Cool Combustion system. Gas turbine users with NO_x control requirements should also consider other performance parameters such as service life and cost when selecting a NO_x control system.

In accordance with the NO_x Control Technology generic verification protocol, this verification report is valid indefinitely for application of the XononTM Cool Combustion system within the range of applicability of the statement.

Original signed by Hugh W. McKinnon 12/15/00
Hugh W. McKinnon Date
Acting Director
National Risk Management Research Laboratory
Office of Research and Development
United States Environmental Protection Agency

Original signed by Jack R. Farmer 12/22/00

Jack R. Farmer Date

Program Manager

Air Pollution Control Technology Program

Research Triangle Institute

NOTICE: ETV verifications are based on an evaluation of technology performance under specific, predetermined criteria and the appropriate quality assurance procedures. EPA and RTI make no expressed or implied warranties as to the performance of the technology and do not certify that a technology will always operate as verified. The end user is solely responsible for complying with any and all applicable federal, state, and local requirements. Mention of commercial product names does not imply endorsement.

Environmental Technology Verification Report

NO_x Control Technologies

Catalytica Combustion Systems, Inc. XononTM Flameless Combustion System

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EPA Cooperative Agreement CR 826152-01-2

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Notice

This document was prepared by Midwest Research Institute (MRI) under a contract with Research Triangle Institute (RTI) with funding from Cooperative Agreement No. CR826152-01-2 with the U.S. Environmental Protection Agency (EPA). The document has been subjected to RTI/EPA's peer and administrative reviews and has been approved for publication. Mention of corporation names, trade names, or commercial products does not constitute endorsement or recommendation for use of specific products.

Catalytica Combustion Systems, Inc. becomes Catalytica Energy Systems, Inc.

Catalytica Combustion Systems, Inc. (abbreviated in this report as CCSI), a subsidiary of Catalytica, Inc., reorganized into stand-alone, publicly-traded Catalytica Energy Systems, Inc., on December 18, 2000. The XononTM Cool Combustion technology, referred to in this report as XononTM flameless combustion, remains the same, and all references to CCSI should be understood to refer to Catalytica Energy Systems, Inc. Contact information in the verification statement and report has been updated.

Availability of Verification Statement and Report

Copies of the public Verification Statement and Verification Report are available from

1. Research Triangle Institute

P.O. Box 12194

Research Triangle Park, NC 27709-2194

Web site: http://etv.rti.org/apct/index.html

or http://www.epa.gov/etv/ (click on partners)

2. USEPA/APPCD

MD-4

Research Triangle Park, NC 27711

Web site: http://www.epa.gov/etv/library.htm (electronic copy)

http://www.epa.gov/ncepihom/

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Abstract

Nitrogen oxides (NO_x) air pollution control technologies (APCTs) are among the technologies evaluated by the APCT Environmental Technology Verification (ETV) Program. The APCT program developed the *Generic Verification Protocol for NO_x Control Technologies for Stationary Combustion Sources* to provide guidance on the verification of specific technologies. The critical performance factor for this verification is the NO_x emission concentration within the performance envelope of the test. This protocol was developed by RTI and MRI, reviewed and discussed by a technical panel of experts, and approved by EPA. The protocol states the critical data quality objectives for a NO_x control technology verification, as well as noncritical but still important measurements of other performance parameters.

The Catalytica Combustion Systems, Inc., XononTM flameless combustion system was submitted to the APCT ETV program for verification. A test/quality assurance (QA) plan, prepared in accordance with the generic verification protocol, addressed the site specific issues associated with the verification test. The verification was conducted the week of July 17, 2000, at the XononTM installation on a 1.5-MW gas turbine in Santa Clara, CA. The mean outlet NO_x concentration during the verification was determined to be 1.13 ppmvd at 15% O_2 . The measured NO_x concentration was well within the stated data quality objective for the NO_x measurement. Other important performance and operating parameters were also measured.

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Acronyms/Abbreviations

ADQ Audit of data quality

ANSI American National Standards Institute
APCT Air Pollution Control Technology

ASME American Society of Mechanical Engineers

CCSI Catalytica Combustion Systems, Inc., renamed Catalytica Energy Systems, Inc.

cfm Cubic feet per minute
CO Carbon monoxide
CV Coefficient of variance
DQO Data quality objective

EED MRI's Environmental Engineering Division

EPA Environmental Protection Agency
ETV Environmental Technology Verification

fpm Feet per minute

GVP Generic Verification Protocol HMI Human/machine interface

IR Infrared

ISO International Standards Organization

MFC Mass flow controller

MRI Midwest Research Institute

NESHAP National Emission Standard for Hazardous Air Pollutants

NIST National Institute of Standards and Technology

NO_x Nitrogen oxides
 OD Outside diameter
 PE Performance evaluation
 ppmv Part per million by volume

ppmvd Part per million by volume dry basis ppmvw Part per million by volume wet basis

QA Quality assurance

QAO Quality assurance officer

QC Quality control

QMP Quality management plan QSM Quality system manual RH Relative humidity

RTI Research Triangle Institute SOP Standard operating procedure

SS Stainless steel

TEI Thermo Environmental Instruments, Inc. (sometimes identified as TECO)

TSA Technical systems audit

UHCs Unburned hydrocarbons (same as total hydrocarbons)

Section 1.0

Introduction

The objective of the Air Pollution Control Technology (APTC) Environmental Technology Verification (ETV) Program is to verify, with high data quality, the performance of air pollution control technologies. A subset of air pollution control technologies is nitrogen oxides (NO_x) emission control technologies. One of these NO_x emission control technologies is the flameless combustion system known as $Xonon^{TM}$, developed by Catalytica Combustion Systems, Inc. (CCSI) of Mountain View, California. The $Xonon^{TM}$ flameless combustion system is an advanced combustion process designed for gas turbines that is capable of producing NO_x emissions below the current level of 9 to 25 parts per million by volume on a dry basis (ppmvd) at 15 percent oxygen (O_2) obtainable with dry, low- NO_x combustion techniques.

Control of NO_x emissions is of increasing interest, particularly related to the National Ambient Air Quality Standard for ozone. The Environmental Protection Agency (EPA) recently completed a rulemaking to reduce more than 1 million tons of NO_x each ozone season and offered to develop and administer a multistate NO_x trading program to assist the affected states. Additionally, many state and local permitting agencies are requiring unprecedentedly low NO_x emission levels.

To evaluate the performance of the XononTM flameless combustion system, a field test program was designed by Research Triangle Institute (RTI) and Midwest Research Institute (MRI) with assistance from CCSI. A site visit to the host facility was completed on April 17, 2000, and a test/QA plan was developed and approved by EPA on June 28, 2000. The verification field test was conducted on July 18 and 19, 2000.

The host facility was the Silicon Valley Power Gianera generating station located at 4948 Centennial Drive in Santa Clara, California. The XononTM flameless combustion system was installed on a 1,500-kW gas-turbine-generator set manufactured by Kawasaki (Model M1A-13A).

The verification statement for the XononTM flameless combustion system verification test is presented in the preceding section. A detailed description of the XononTM flameless combustion system is presented in Section 2. The procedures and methods used for the verification test are discussed in Section 3. The operating range over which the verification test was conducted is presented in Section 4. The results of the verification test are summarized and discussed in Section 5.

Appendices describing QA/QC activities and results (Appendix A), raw test data (Appendix B), and equipment calibration results (Appendix C) are attached.

Section 2.0

Description and Identification of XononTM Flameless Combustion System

The XononTM flameless combustion system is completely contained within the combustion chamber of the gas turbine. The XononTM system completely combusts fuel to produce a high-temperature gaseous mixture, typically over 1300 °C (2400°F). Dilution air is added to shape the temperature profile required at the turbine inlet.

The XononTM combustor consists of four sections:

- 1. **Preburner**. The preburner is used for startup preheat of air before it enters the catalyst module and acceleration of the turbine. The preburner could be a conventional, diffusion flame burner or could be a dry, low-NO_x type (lean, premixed) burner. For this Kawasaki turbine, the preburner was a lean premix burner.
- 2. **Fuel injection and fuel/air mixing system**. This system injects the fuel and mixes it with the main air flow to provide a very well-mixed, uniform fuel/air mixture to the catalyst.
- 3. **Xonon**TM **catalyst module**. In the catalyst module, a portion of the fuel is combusted without a flame to produce a high-temperature gas.
- 4. **Homogeneous combustion region**. Located immediately downstream of the catalyst module, the homogeneous combustion region is where the remainder of the fuel is combusted, and carbon monoxide and unburned hydrocarbons are reduced to very low levels (also a flameless combustion process).

The overall combustion process in the XononTM system is a partial combustion of fuel in the catalyst module followed by complete combustion downstream of the catalyst in the burnout zone. Partial combustion within the catalyst produces no NO_x . Homogeneous combustion downstream of the catalyst usually produces no NO_x , because combustion occurs at a uniformly low temperature. A small amount of fuel is combusted in the preburner to raise the compressed air temperature to about 470°C (880°F). NO_x in the turbine exhaust is usually from the preburner.

The design of each XononTM combustor is customized to the particular turbine model and operating conditions of the application and would typically be defined through a collaborative effort with the manufacturer of the turbine to integrate the hardware into the design. The footprint may vary depending on the implementation, although generically the XononTM combustion system would likely be somewhat larger than the combustor that is typically supplied as standard equipment by the turbine manufacturer. Each unit could have multiple fuel inputs from separate control valves, and additional instrumentation for control and monitoring would be integrated into the turbine control system.

When a XononTM combustion system is installed, initial startup and shakedown are supervised by CCSI personnel, and the requisite training to operate and service the equipment is provided at that time. Maintenance procedures and spare parts requirements are identified during design of the combustor for the specific turbine model, and this information is provided upon delivery of the equipment. CCSI indicates the elapsed time between installation and commissioning to be less than 1 month.

After initial commissioning, the XononTM combustion system is expected to require minimal ongoing service. CCSI expects the catalyst module to have a useful life of approximately 8,000 operating hours, requiring a replacement of the module at this interval.

This verification report covers application of the XononTM flameless combustion system to small gas turbines operated at full load when combusting natural gas within the stated operating condition envelope. The same pilot unit was operated at the test site by the vendor, CCSI, for over 4,000 hours before the verification test. Data from this long-term operating period have been submitted to a number of regulatory authorities for their review and evaluation. While these data and the instruments used were not verified during this test, within the operating condition envelope the results are generally consistent with the verification test results. CCSI should be contacted for these long-term data or other information.

CCSI XononTM **Product Performance Expectations**

CCSI expects that the XononTM flameless combustion technology incorporated in a XononTM combustion system for a natural-gas-fueled Kawasaki M1A-13A gas turbine is capable of achieving emissions of NO_x of less than 2.5 ppmvd (corrected to 15 percent oxygen $[O_2]$) on a 1-hour rolling average basis, and less than 2.0 ppmvd (corrected to 15 percent O_2) on a 3-hour rolling average basis. Under the same conditions, this XononTM combustion system is also expected to achieve carbon monoxide (CO) emissions of less than 6 ppmvd (corrected to 15 percent O_2).

Section 3.0

Procedures and Methods Used in Testing

A generic verification protocol (GVP) for testing NO_x control technologies was prepared and approved by the NO_x Control Technology Technical Panel (RTI, 2000a). The GVP established the guidelines for the verification test design, the data quality objective (DQO) for the primary verification parameter (for this verification test, NO_x concentration corrected to 15 percent O₂), and the test methods to be used. A test/QA Plan (RTI, 2000b) was written to apply the GVP to the XononTM verification. This section details the test design and the test methods used for the verification test of the XononTM flameless combustion system.

3.1 Test Design

The GVP for NO_x Control Technologies provides extended discussions on the experimental design approach for NO_x control technologies verification testing. The specific design for this test is described below.

The critical measurement for the XononTM flameless combustion system verification was the level of NO_x emitted in ppmvd at 15 percent O_2 . This verification test was designed to measure the outlet NO_x emission concentration under targeted field test conditions with the XononTM flameless combustion system operating at a specified high load and the encountered low and high ambient temperature for the test days. Historical ambient temperature data suggested that its effect might be detectable by conducting sets of tests at dawn (cold) and in the afternoon (hot).

Associated emissions concentrations were also measured using EPA reference methods, but the test was not designed around acquisition of these data. Ambient temperature was an important measurement for establishing the bounds of the verification test design.

A 2×1 factorial experimental design was used with each of the parameters. Two replications of the factorial design (six test runs in each replication) was used for a total of 12 test runs. Table 1 gives the factorial design with the target values for each parameter. As required by the DQO, the product of this test design was the verified mean NO_x emission concentration(s) and the achieved 95 percent confidence interval of the mean for the specified operating range.

The factorial design allowed for statistical significance tests to determine whether the outlet NO_x concentration varied significantly with ambient temperature. Further, since two replicates were done, the significance of interactions between ambient temperature and outlet NO_x concentration

Table 1. Verification Test Design (Target Values)^a

Test Run	Ambient Temperature (time of day)
1	Low (dawn)
2	Low (dawn)
3	Low (dawn)
4	High (afternoon)
5	High (afternoon)
6	High (afternoon)
7	Low (dawn)
8	Low (dawn)
9	Low (dawn)
10	High (afternoon)
11	High (afternoon)
12	High (afternoon)
- II	1 0=0/

^a Turbine load >95% maximum.

could also be tested. If the outlet NO_x concentration did not change significantly with ambient temperature, the results are valid for the range of ambient temperature covered by the test. If the outlet NO_x concentration did vary significantly with ambient temperature, the results need to include information indicating the dependence of outlet NO_x concentration on ambient temperature. The results of the statistical significance tests are presented in Section 5.1.1.

Because the turbine was operated at constant full load (>97%) during the entire testing period, the process was assumed to be at equilibrium during all testing.

3.2 Sampling Methods

Table 2 lists all the measurement parameters for this verification test. They are categorized in the table as performance factors (e.g., direct emission measurements), associated impacts (e.g., CO and UHC emissions), and test conditions that were documented. Included in Table 2 are the factors to be verified, parameters to be measured for each factor, the measurement method for each parameter, and explanatory comments. The facility contact provided data for process condition parameters collected from the turbine human/machine interface (HMI) computer. Measurement methods and procedures are described in Sections 3.2.2 through 3.2.5.

3.2.1 Sampling Locations

Sample locations were chosen so that they met the minimum specified sample location criteria of the sample methods used or yielded a representative sample. The pollutant emission sampling location, process operating condition measurement locations, and ambient conditions measurement location are presented in Sections 3.2.1.1 through 3.2.1.3, respectively.

3.2.1.1 Pollutant Emission Sampling Location—

The NO_x, CO, UHC, O₂, and CO₂ concentrations were measured in the turbine exhaust stack (see Figure 1). Two sets of sampling ports were available, but neither met Method 20 criteria. As noted in the test/QA plan, the top set of sampling ports were judged as the most likely to yield a representative sample; therefore, the top sampling ports were used.

3.2.1.2 Process Conditions Measurement Locations—

Several parameters related to the operating conditions of the gas turbine during the verification test runs were recorded. These include electric power output, fuel flow rate, inlet temperature to the compressor, compressor discharge pressure, compressor discharge temperature, temperature into the catalyst, temperature out of the catalyst, and the exhaust gas temperature. The measurement locations for process and turbine parameters are identified in Figure 2 and are in relation to where the measurements are taken in the gas turbine.

Table 2. Summary of Measurements

Factors to be Verified	Parameter to be Measured	Measurement Method	Comments
Performance factors	•	-	
NO _x emissions	Outlet NO _x conc., ppmv	EPA Ref. Method 20 (40 CFR 60 App. A)	MRI provided and operated analyzer
Associated impacts		•	•
CO emissions	Outlet CO conc., ppmv	EPA Ref. Method 10 (40 CFR 60 App. A)	MRI provided and operated analyzer
UHC emissions	Outlet THC conc., ppmvw	EPA Ref. Method 25A (40 CFR 60 App. A)	MRI provided and operated analyzer
O ₂ /CO ₂ emissions	Outlet O ₂ /CO ₂ conc.,%	EPA Ref. Method 20 (40 CFR 60 App. A)	MRI provided and operated analyzer
Test conditions docur	nentation	•	•
Percent of turbine's rated capacity	Electrical power ÷ turbine rating	Real power sensor	MRI collected data from facility contact
Fuel type			Natural gas
Fuel flow	Fuel flow rate	Coriolis-type flowmeter	Facility contact provided data from turbine HMI computer
Fuel sample results	Natural gas composition	Chromatographic analysis	From fuel sample results obtained from CCSI
Ambient conditions	Air temperature	Thermocouple or Thermohygrometer following EPA Quality Assurance Handbook for Air Pollution Measurement Systems, Volume IV: Meteorological Measurements	MRI conducted temperature, pressure, and humidity measurements concurrently
	Air pressure	ASTM D3631-95: aneroid barometer or equivalent	
	Air humidity	Thermohygrometer equivalent to ASTM E337- 84(1996)e1	
Compressor parameters	Inlet temperature	Array of thermocouples on turbine	Facility contact provided data from turbine HMI computer
	Discharge temperature	Array of thermocouples on turbine	Facility contact provided data from turbine HMI computer
	Discharge pressure	Pressure gauge	Facility contact provided data from turbine HMI computer
Catalyst inlet condition	Temperature at catalyst inlet	Array of thermocouples on turbine	Facility contact provided data from turbine HMI computer
Catalyst outlet condition	Temperature out of the catalyst	Array of thermocouples on turbine	Facility contact provided data from turbine HMI computer
Catalyst hours of operation	Hours of operation since catalyst installed	Clock counter	Information provided by CCSI facility contact
Exhaust temperature	Exhaust gas temperature	Array of thermocouples on turbine	Facility contact provides data from turbine HMI computer
Compressor/turbine status		Pressure ratio compared to rated value	Information provided by CCSI facility contact

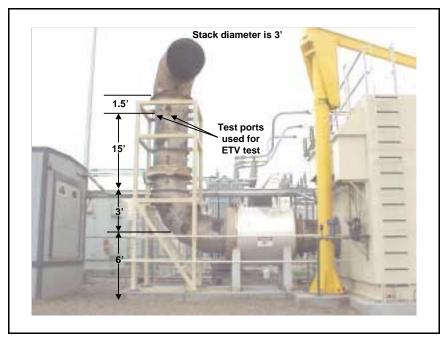


Figure 1. Turbine exhaust sampling location.

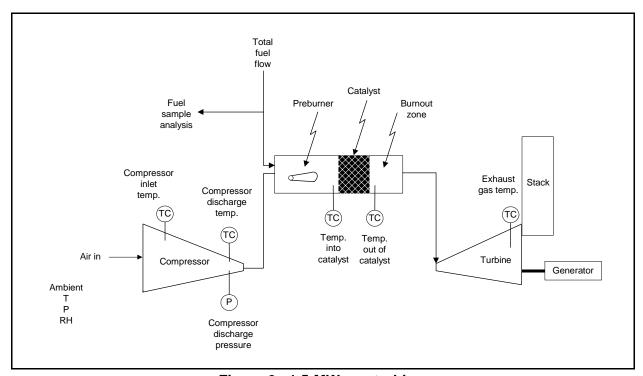


Figure 2. 1.5-MW gas turbine.

3.2.1.3 Ambient Conditions Measurement Location—

Parameters related to the ambient conditions during the verification test runs include the ambient air temperature, ambient air pressure, and ambient relative humidity. The measurement location for the ambient conditions is shown in Figure 3. The temperature (T), pressure (P), and relative humidity (RH) measurement devices were placed on the platform just below the gas turbine air inlet filters. In this location, the measurements are representative of the inlet air conditions (as recommended in Section 4.3.4 of *EPA Quality Assurance Handbook for Air Pollution Measurement Systems, Volume IV: Meteorological Measurements*, Templeman, 1995). An aspirated radiation shield was used to prevent biases caused by direct sunlight exposure.



Figure 3. Ambient conditions sampling location.

3.2.2 NO_x, CO, UHC, and O₂/CO₂ Sampling Procedures

Turbine exhaust gas was sampled for NO_x, CO, UHC, and O₂/CO₂ using EPA reference methods. All sampling followed the requirements of the specific test method being used unless otherwise stated in this document or approved by RTI before the verification test. The analytical systems were calibrated before and after each 32-min test run following the procedures in each applicable EPA Reference Method (40 CFR 60 App. A).

3.2.2.1 Sampling System—

A diagram of the extractive gaseous measurement system used for the testing is shown in Figure 4. Two independent sampling systems were used, one for CO, O_2 , CO_2 , and NO_x and

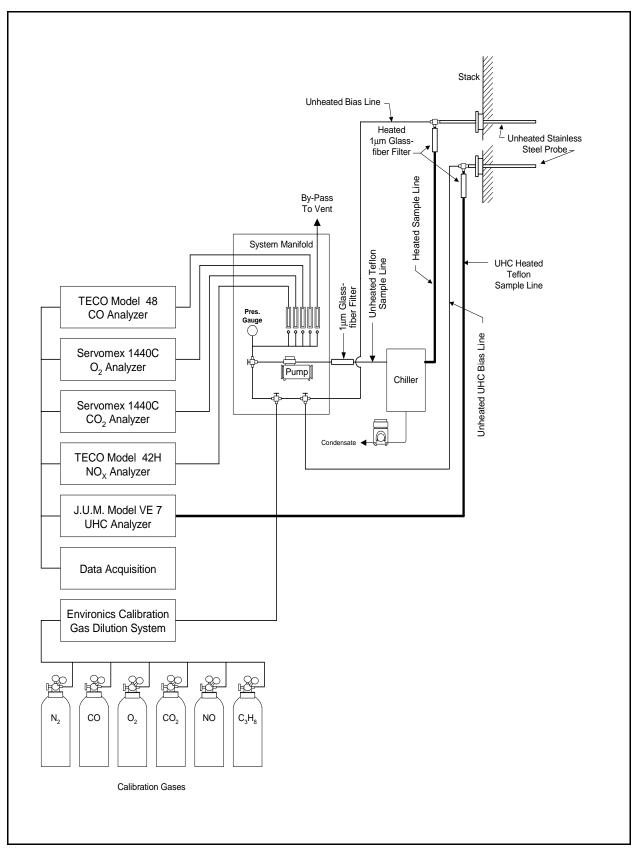


Figure 4. Extractive sampling system

another for UHC. All analyzers, calibration gases, and the sampling manifold were housed in an environmentally controlled trailer. The sampling system components were stainless steel (SS), Teflon, or glass. These materials have been proven to be inert for the gases of interest.

The sampling system for measurement of CO, O₂, CO₂, and NO_x consisted of

- Unheated stainless steel probe; 1.27 cm (0.5 in.) outside diameter (OD) (since the stack gas temperature was ~ 510°C [950°F], the probe was not heated);
- Heated (\sim 121°C [250°F]) glass-fiber filter to remove particles with a diameter >1 μ m;
- Heated (~121°C [250°F]) Teflon sample line (~3 m [10 ft] long and 0.95 cm [0.38 in.] OD) to transport the sample gas to the moisture removal condenser; temperature of the sample line was regulated with a thermostatic heat controller;
- Chiller condenser system submerged in an ice bath to condense and remove moisture in the sample gas; the condenser is a two-pass system to condense moisture while minimizing the liquid/air interface; a peristaltic pump was used to continually remove condensed water vapor; the water vapor dewpoint after the chiller was estimated to be ~ 3.5 °C (38 °F);
- Unheated Teflon sample line (~ 2.3 m [75 ft] long and 0.95 cm [0.38 in.] OD) to transport the sample gas from the chiller (located on the scaffold platform near the sample ports) to the sample manifold; just upstream of the sample extraction pump was a second glass-fiber filter;
- Teflon-lined sample pump to extract sample gas from the stack; sampling rate was
 10 L/min; and
- Individual rotameters regulated the sample flow to each analyzer and excess sample gas was dumped through the bypass.

The sampling system for measurement of UHCs consisted of

- Unheated SS probe; 1.27 cm (0.5 in.) OD;
- Heated (\sim 121 °C [250 °F]) glass-fiber filter to remove particles with a diameter >1 μ m;
- Heated (~121 °C [250 °F]) Teflon sample line (~23 m [75 ft] long and 0.63 cm [0.25 in.] OD) to transport the sample gas directly to the hydrocarbon analyzer; temperature of the sample line was regulated with a thermostatic heat controller; and
- Sample gas was extracted by a heated pump contained within the hydrocarbon analyzer.

The sampling system was calibrated by directing each calibration gas to the probe through an unheated Teflon tube. The probe was "flooded" with calibration gas, and the sample pump pulled as much of the calibration gas as needed to the system manifold. Excess calibration gas was dumped out the probe. This process of calibrating the system does not pressurize the sampling system and mask any leaks (see Section 3.2.3.5.2 for description of CO analyzer calibration).

Calibration gases were generated from a single, high-concentration EPA protocol gas with an Environics Model 2020 gas dilution system. The Environics system consists of four electronic

mass flow controllers (MFCs). MFC 1 was used for the nitrogen dilution gas. MFC 2 (0 to 10 L/min) and MFC 3 (0 to 1 L/min) are used in combination with MFC 1 to generate the specified calibration gas concentration by diluting a high concentration standard gas. MFC 4 (0 to 0.1 L/min) was not used. The Environics system was calibrated at the factory on July 11, 2000. Also, the calibration of the combined MFCs that were used for this test (e.g., 1 + 2 and 1 + 3) was checked in accordance with EPA Method 205 the day before the field test began. The Method 205 data are summarized in Section 5.

3.2.2.2 Reference Analyzers—

The reference analyzers used for quantifying the gaseous concentrations are listed in Table 3. The table also includes a description of the analyzer and the measurement ranges used for this test. Measured pollutant concentrations were extremely low relative to the measurement ranges. Most notably, the UHC concentrations were about 0.1 to 0.2 part per million by volume on a wet basis (ppmvw) as measured on a 0- to 100-ppmvw range. Method 25A specifies a measurement range of 1.5 times the expected concentration, which is unfeasible at extremely low concentrations.

Table 3. Reference Analyzers and Measurement Ranges

			<u> </u>
Pollutant	Reference Analyzer	Measurement Range	Description
NO _x	Thermo Environmental Instruments (TEI) 42H	0-20 ppmv	Uses the principle of chemiluminescence to measure the concentration of NO_x in the sample stream. The instrument uses a heated can NO_2 converter.
СО	Thermo Environmental Instruments (TEI) 48	0-50 ppmv	Uses the principle of gas filter correlation and non- dispersive infrared (GFC-NDIR) to measure the concentration of CO in the sample stream.
UHC	J.U.M VE 7	0-100 ppmvw	Uses the principle of flame ionization detection (FID) to measure the concentration of hydrocarbons in the sample stream.
O ₂ /CO ₂	Servomex 1440C	0-25% / 0-20%	The O_2 detector uses the principle of paramagnetics, and the CO_2 detector uses a single-beam, dual-wavelength IR technique.

3.2.3 Sampling Methods Requirements

Each of the sampling methods has different criteria to ensure the quality of the sample and the data collected. Each of these requirements is presented in the following sections.

3.2.3.1 Analyzer Interference Test—

An initial interference check was completed on the NO_x , CO, O_2 , and CO_2 analyzers before their first use. For the interference test, the gases listed in Table 4 were injected into each analyzer. For acceptable analyzer performance, the sum of the interference responses to all of the interference gases must be ≤ 2 percent of the analyzer span value. The interference test results are presented in Section 5.

3.2.3.2 NO₂ Converter Efficiency Test—

The NO₂ converter efficiency is tested as part of routine analyzer QC Method 20. The test relies on the oxidation reaction of NO in the presence of oxygen. NO reacts to form NO₂ in equilibrium with NO. For the test, a clean, leak-free Tedlar bag was filled half full with the mid-level NO calibration gas. The bag was then filled with 20.9 percent O₂ gas. The bag was attached directly to the NO_x analyzer sample inlet. After approximately a 2-min stabilization period, 30 1-min average NO_x analyzer

Table 4. Gas Analyzers Interference Test
Gas Concentrations

СО	SO ₂	CO ₂	02						
NC	NO _x Analyzer Interference Gases								
498 ppmv	201 ppmv	9.98%	20.9%						
CC	O Analyzer Inte	rference Gas	ses						
NA	NA	9.98%	NA						
0,	Analyzer Inte	rference Gas	es						
498 ppmv	197 ppmv	9.98%	NA						
CO ₂ Analyzer Interference Gases									
498 ppmv	197 ppmv	NA	20.9%						
	·	·	<u> </u>						

NA = Not applicable.

readings were recorded. For an acceptable converter, the 1-min average response at the end of 30 min is required to not decrease more than 2 percent of the highest peak 1-min value. That is, the analyzer should be capable of converting all the NO to NO_2 . The results of the NO_2 converter efficiency check are presented in Section 5.

3.2.3.3 Response Time Test—

3.2.3.3.1 Method 20 Response Time - NO_x and O_2/CO_2. To determine the response time according to Method 20 procedures, the zero gas (i.e., N_2) was injected into the sampling system at the probe. When the analyzer's readings were stable, the zero gas was turned off so the effluent could be sampled. When a stable reading was obtained, the upscale response time was determined as the time required for the computer readout to record a 95 percent step change from the zero reading to the stable effluent concentration. Then the high-level calibration gas for each analyzer was injected into the sampling system at the probe. When the analyzer's readings were stable, the high-level gas was turned off so that the effluent could be sampled. When a stable reading was obtained, the downscale response time was determined as the time required for the computer readout to record a 95 percent step change from the calibration gas reading to the stable effluent concentration. This procedure was repeated until three upscale and three downscale response times were completed. The longest of all the upscale and downscale response times was reported as the system response time for that analyzer. For Method 20, the response time must be 30 s or less. The response times are presented in Section 5, Table 13.

3.2.3.3.2 Method 25A Response Time - UHC. For EPA Method 25A, only an upscale response time test is required. To determine the upscale response time, the zero gas was injected into the sampling system at the probe. Then, the high-level calibration gas was injected into the sampling system. The upscale response time was determined as the time required for the computer readout to reach 95 percent of the high-level calibration gas reading. This procedure

was repeated three times, and the average was reported as the response time. The response time is presented in Section 5, Table 13.

3.2.3.4 Preliminary O₂ Traverse—

Method 20 requires a preliminary O_2 traverse to be conducted at multiple sample points across the stack's cross-sectional area. The preliminary O_2 traverse determines the eight lowest O_2 concentration sampling points from an array of multiple points. These eight low O_2 points are used as the traverse points for the individual test runs. However, since this stack had a cross-sectional area of 0.66 m^2 (7.1 ft²), only eight traverse points would be used for the preliminary O_2 traverse. Therefore, a preliminary O_2 traverse was not necessary and was not done, and eight traverse points for the test runs were selected in accordance with EPA Method 1.

3.2.3.5 Calibrations—

Table 5 lists the calibration gas concentrations used for the reference method testing. EPA protocol gas was used to calibrate the analyzers. Each of the reference methods has different calibration procedures. The individual method calibration procedures are described in Sections 3.2.3.5.1 through 3.2.3.5.3. The gaseous pollutant measurement system was calibrated before and after each test run. Also, no test run started more than 2 hours after a pretest calibration, and all post-test calibrations were completed within 1 hour of the end of a test run.

Calibration point 0, **UHC** CO, NO. CO Pure N₂ Pure N₂ Pure N₂ Pure N₂ Zero Pure N₂ Low-level NA NA 5.02 ppmv 15.0 ppmv 29.9 ppmv 10.03 ppmv Mid-level 11.99% 3.01% 29.9 ppmv 49.9 ppmv High-level 20.9% 9.98% 17.04 ppmv 44.9 ppmv 84.9 ppmv

Table 5. Calibration Gas Concentrations

3.2.3.5.1 Method 20 Calibration Procedures. The NO_x calibration gas was 201.85 ppmv NO in a balance of N_2 . The O_2 calibration gas was 38.4 percent O_2 in a balance of N_2 . The CO_2 calibration gas was 40.05 percent CO_2 in a balance of N_2 . Copies of the calibration gas certifications are attached in Appendix A. As noted earlier, a gas dilution system was used to make the targeted gas concentration levels shown in Table 5 from the single, high-concentration EPA protocol gas.

For calibration error checks of both the NO_x and diluent analyzers, the zero gas and mid-level gas were introduced separately into the sampling system at the probe. Each analyzer's response was adjusted to the appropriate level. Then the remainder of the calibration gases were introduced into the sampling system, one at a time. The acceptable response of the analyzer to each calibration gas must be within ± 2 percent of span.

At the conclusion of a test run, the zero and mid-level calibration gases for each analyzer were introduced separately into the sampling system. Both the zero drift and calibration drift, calculated in accordance with Equation 1, must be within ± 2 percent of span. If a drift was greater than 2 percent of span, the test run would have been considered invalid and the measurement system would have been repaired to satisfy drift tolerances before additional test runs were conducted. Method 20 calibration results are summarized in Section 5. Individual pre- and post-test run calibrations are presented in Appendix B.

Percent drift = (Final response - Initial response) / Span value
$$\times$$
 100 (1)

3.2.3.5.2 Method 10 Calibration Procedures. The CO calibration gas was 199.8 ppmv CO in a balance of N_2 . The calibration gas certification is shown in Appendix A. The gas dilution system was used to make the targeted gas concentration levels from the single, high-concentration EPA protocol gas.

CO analyzer calibration error checks were conducted before the start of each day's testing. The calibration error check was conducted (after final calibration adjustments were made) by separately injecting each of the four calibration gases (zero, low-, mid-, and high-level) directly into the analyzer and recording the response. If the calibration error was greater than 2 percent, the analyzer would have been repaired or replaced and recalibrated to an acceptable calibration error limit before proceeding.

Zero and upscale sampling system calibration checks were performed both before and after each test run to quantify the reference measurement system calibration drift and the sampling system bias. Upscale calibration checks were performed using the mid-level gas. During these checks, the calibration gases were introduced into the sampling system at the probe so that they were sampled and analyzed in the same manner as the sample gas. Drift means the difference between the pre- and post-test run system calibration check responses. Sampling system bias means the difference between the system calibration check response and the initial calibration error response (direct analyzer calibration) at the zero and upscale calibration gas levels. Method 10 calibration results are summarized in Section 5. Individual pre- and post-test run calibrations are presented in Appendix B.

3.2.3.5.3 Method 25A Calibration Procedures. The UHC calibration gas was 190.6 ppmv propane in a balance of nitrogen. Copies of the calibration gas certification are located in Appendix B. The gas dilution system was used to make the targeted gas concentration levels shown in Table 5 from the single, high-concentration EPA protocol gas.

For calibration error checks, the zero gas and high-level gas were introduced separately into the sampling system at the probe. The UHC analyzer's response was adjusted to the appropriate level. Then the low- and mid-level calibration gases were introduced into the sampling system, one at a time. The acceptable response of the analyzer to each calibration gas must be within ±5 percent of the calibration gas value.

At the conclusion of a test run, the zero and mid-level calibration gases were introduced separately into the sampling system. Both the zero drift and calibration drift, calculated in accordance with Equation 1, must be within ± 3 percent of span. If a drift was greater than 3 percent of span, the test run would have been considered invalid, and the measurement system would have been repaired before additional test runs were conducted. Method 25A calibration results are summarized in Section 5. Individual pre- and post-test run calibrations are presented in Appendix B.

3.2.3.6 CO₂ Trap—

Method 10 requires that CO₂ be removed from the sample gas that is sent to the CO analyzer. The CO₂ is removed because the commonly used, nondispersive infrared technology instrument for measurement of CO exhibits an interference from CO₂. However, the TEI Model 48 incorporates the technique of gas filter correlation to eliminate the CO₂ interference from the measurement of CO. Since the TEI Model 48 does not have a CO₂ interference (see the interference test results in Section 5), the CO₂ trap was not used.

3.2.3.7 Sample Location by Method 20 and Traverse Point Selection by Method 1—

Two sets of sampling ports were available on the turbine exhaust stack. One set was located immediately after a long 90° horizontal-to-vertical upward bend in the stack. The second set was located approximately 4.6 m (5 duct diameters) downstream of the 90° horizontal-to-vertical upward bend and 0.5 m (0.5 duct diameters) upstream of the stack exit. Neither of these port locations is ideal; however, the top ports were used (see Figure 1). Only one of the top ports was used for the Method 20 traverse because the scaffold was only set up on one side of the circular stack. Therefore, MRI did not have safe access to the second port for the

Table 6. Method 20 Traverse Points

Point	Percent of Stack Diameter	Distance from Stack Wall (cm)
1	6.7	(0.9)
2	25.0	(3.5)
3	75.0	(10.6)
4	93.3	(13.2)

Method 20 traverse. Because the gas concentration was not stratified across the one available diagonal traverse, all parties agreed that double traversing across the single port was acceptable. Table 6 shows the point locations.

3.2.4 Process Data Collection

Process data were collected from the turbine control's HMI computer to document the test conditions. The CCSI facility contact provided the data from the HMI computer. Table 2 identifies the parameters that were measured and the party responsible. The test condition documentation parameters taken from the HMI computer were retrieved at 1-min intervals for each test run. Process data, at 1-min intervals for each test run, are presented in Appendix C. The process data measurements are summarized in Sections 3.2.4.1 through 3.2.4.6.

3.2.4.1 Electrical Power Generation by Turbine —

To determine the operating rate of the turbine during the verification test, the electrical power production from the electrical generator was recorded. This measurement was taken with a Real Power Sensor that determines the electrical power supplied at the generator terminals. At this writing, CCSI is not aware of any calibration of this device since commissioning of the site in October 1998. The output has been noted by CCSI to be consistent with the City of Santa Clara meter on several occasions.

3.2.4.2 Fuel Flow Rate—

The fuel flow rate into the combustion system was measured with a Coriolis-mass flowmeter. The flowmeter was calibrated for natural gas at the factory and was recalibrated on June 28, 2000. (The flowmeter is periodically compared to the City of Santa Clara's main turbine flowmeter.)

3.2.4.3 Compressor Inlet Temperature—

Compressor inlet temperature (also referred to as "ambient temperature" by the facility) was measured with two 1/8-in. diameter sheathed K-type thermocouples located in the inlet air duct. These devices are calibrated on a semiannual basis using a calibrated thermowell device.

3.2.4.4 Compressor Discharge Pressure—

Compressor discharge pressure was measured using two pressure taps and two absolute pressure transducers. The transducers were originally calibrated at the factory and are periodically recalibrated by CCSI personnel using specially maintained and calibrated pressure-sensing devices. The absolute pressure transducers were last calibrated in March 2000.

3.2.4.5 Catalyst Inlet/Catalyst Outlet Temperatures—

The air temperature just upstream of the catalyst and the gas temperature just downstream of the catalyst were measured by separate thermocouple arrays. The catalyst outlet temperature was measured with a series of four to eight thermocouples installed at the exit from the catalyst bed. The thermocouples are calibrated by CCSI personnel whenever the thermocouple hardware is changed.

3.2.4.6 Turbine Exhaust Temperature—

The turbine outlet temperature was measured by four 1/8-in. diameter sheathed K-type thermocouples installed at the exit of the turbine, just upstream of the stack's silencer. These thermocouples were factory calibrated, were recalibrated by CCSI personnel upon receipt, and were recalibrated upon installation in the spring of 2000.

3.2.5 Ambient Conditions Sampling

Three ambient air conditions were measured three times during each test run: temperature, pressure, and relative humidity. Temperature and humidity were measured using an equivalent technique to ASTM E337-84(1996)e1. ASTM E337-84(1996)e1 uses an aspirated wet-bulb and dry-bulb device to determine relative humidity, but MRI used a thermohygrometer to obtain the relative humidity and ambient temperature. Pressure was measured using the ASTM D3631-95 method. Ambient pressure was measured with an aneroid barometer. The thermohygrometer and aneroid barometer were placed in a mechanically aspirated, grey steel box. The accuracy of the thermohygrometer measurements are ± 3 percent for relative humidity and $\pm 0.7\,^{\circ}$ F for ambient temperature based on the manufacturer's performance specifications. The relative humidity is detected using the principle of changes in the capacitance of the sensor as its thin polymer film absorbs water molecules. Temperature is measured with a negative temperature coefficient thermistor. Results of the ambient conditions measurements are shown in Appendix C.

The equipment used to make the ambient conditions measurements is carefully maintained by MRI's Field Measurements section. The instrumentation was calibrated according to MRI standard operating procedures (SOPs): MRI-0721 - Calibration of Thermocouple Probes, Thermocouple Indicators and Digital Thermometers, MRI-0722 - Calibration of Pressure Gauges, and MRI-0729 - Qualification and Calibration of Hygrometers at MRI's laboratory before being transported to the field measurement site. Results of those calibrations are presented in Appendix C.

3.3 Data Acquisition and Data Management

Data to document the process operating conditions of the turbine and XononTM system were recorded by the turbine's HMI computer. These data were provided by the facility contact to MRI's Field Team Leader in electronic format after each three-run test series. Process data are shown in Appendix B. Data to document the ambient conditions were recorded manually on the sheets shown in Appendix B. A Labtech Notebook was used to record the concentration signals from the individual analyzers. The Labtech Notebook recorded the analyzer output at 1-s intervals and averaged those signals into 1-min averages. At the conclusion of a test run, the preand post-test calibration results were manually transcribed into a Microsoft Excel spreadsheet to calculate drift and system bias. After a series of test runs, the test run values were electronically transferred from the Labtech Notebook into a Microsoft Excel spreadsheet for data calculations and averaging. The calculations done by Microsoft Excel used the default rounding convention. The raw data printouts from the Labtech Notebook and the test run averages are shown in Appendix B.

For Method 20, the first 1-min average, after moving to a new traverse point, is typically disregarded as not representing the concentration at that traverse point. However, for this test program, since gaseous stratification was not present and test runs were 32 min in length, all data were used in the NO_x and O_2 concentration averages.

For this test program, the data measurement and collection activities for the Method 20 measurements shown in Figure 5 were used. This flow chart includes all data activities from the initial pretest QA steps to the passing of the data to the Task Leader. These steps were followed in the field. Data for other methods used during this verification test were collected and handled in the same manner as the Method 20 data.

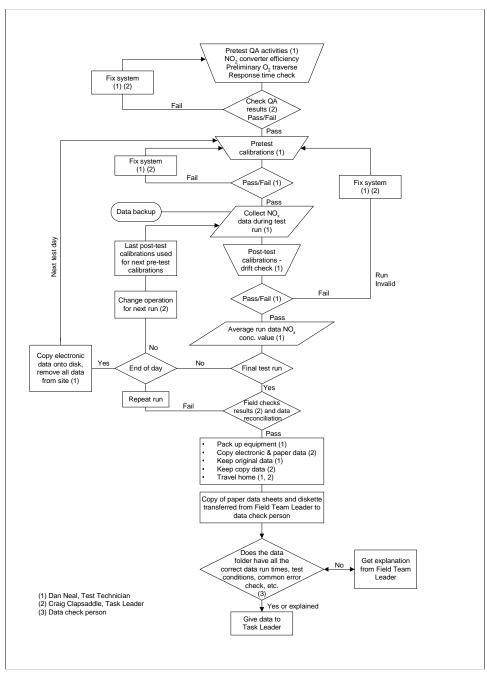


Figure 5. Method 20 NO_x/O₂ gas turbine emissions measurement flowchart.

Section 4.0

Statement of Operating Range of Test

For this verification test of the XononTM flameless combustion system, the CCSI representative indicated that the emissions performance of the technology was guaranteed to be less than 2.5 ppmvd NO_x at 15 percent O_2 and to be less than 6 ppmvd CO at 15 percent O_2 . Without the air management system, this emission guarantee was valid only at full turbine load conditions. Therefore, the verification test was done at full turbine load.

During consultation with the CCSI representative, the only parameter identified that could possibly have an effect on emissions was ambient temperature. In general, lower ambient temperatures result in slightly higher NO_x emissions for XononTM -equipped turbines because slightly more fuel must be used in the pre-burner to achieve the desired inlet temperature to the catalyst. To evaluate the effect of ambient temperature on NO_x emissions, the verification test was conducted during and after sunrise (to achieve the lowest ambient temperature of the day) and during the afternoon (to achieve the highest ambient temperature of the day). The ambient temperature range experienced during the 12 test runs was from 15.1 to 25.3°C (58.8 to 77.2°F).

Data to document the process operating conditions of the turbine and XononTM flameless combustion system were recorded by the turbine's HMI computer. The operating conditions during the 12 test runs are presented in Table 7. The bottom two rows of Table 7 show the minimum and maximum values for each parameter. These minimum and maximum values form the operating range over which this verification test was conducted.

The natural gas collected during the test showed that the fuel had a dry gas higher heating value of 3.778×10^7 gross J/m³ (1012.9 Btu/ft³). The gas analysis is attached in Appendix B.

Table 7. Operating Parameter Ranges

	Amb Ter		Turbin	e Load		Flow ate		ressor Temp.	Disc	ressor harge ssure		ressor narge np.		p. at st Inlet		o. Out italyst		st Gas mp.
Run	°C	°F	(MW)	(%) ^a	kg/h	lb/h	°C	°F	kPa	psig	°C	°F	°C	°F	°C	°F	°C	°F
1	15.2	59	1.39	97.9	428	944	17	62	910	132	356	672	480	895	847	1557	524	980
2	16.3	61	1.38	98.1	425	937	17	63	903	131	356	673	480	895	847	1557	527	981
3	17.4	63	1.37	97.9	423	932	19	65	896	130	357	675	480	896	848	1558	529	983
4	25.2	77	1.25	98.9	406	894	26	78	869	126	364	686	484	903	850	1562	535	994
5	24.1	75	1.27	98.6	405	893	25	77	869	126	364	686	484	903	851	1564	534	993
6	21.3	70	1.29	98.4	411	907	22	72	876	127	361	682	481	898	849	1560	532	989
7	14.6	58	1.36	98.2	428	944	16	60	910	132	355	670	480	896	846	1555	526	979
8	16.3	61	1.35	98.3	425	938	17	63	910	132	356	673	480	896	847	1556	527	981
9	17.4	63	1.33	98.2	423	932	19	65	896	130	357	674	480	896	847	1556	529	983
10	20.7	69	1.29	98.4	412	908	22	72	882	128	361	681	481	898	846	1555	531	988
11	21.9	71	1.25	99.0	408	899	25	76	876	127	362	684	481	898	847	1556	533	991
12	23.5	74	1.23	98.4	407	898	25	76	869	126	362	684	482	900	849	1559	533	991
Minimum	15.2	59	1.23	97.9	405	893	16	60	869	126	355	670	480	895	846	1555	526	979
Maximum	25.2	77	1.39	99.0	425	944	26	78	910	132	364	686	484	903	851	1564	535	994

^aNote: Turbine load (%) is the percent of turbine capability at the prevailing ambient conditions.

Section 5.0

Summary and Discussion of Results

A verification test of the XononTM flameless combustion system was conducted on July 18 and 19, 2000, in Santa Clara, California. The purpose of the verification test was to evaluate the NO_x emission performance for the XononTM flameless combustion system as claimed by CCSI. The test was conducted according to a test/QA plan that was approved by EPA on June 28, 2000.

The results of the verification test are summarized in Section 5.1. An important part of the verification test was the extensive QA applied to this field test. The results of all the QA and quality control (QC) checks performed during this verification test are summarized in Section 5.2. A few minor deviations from the test plan were encountered, and those are discussed in Section 5.3.

5.1 Results Supporting Verification Statement

The pollutant emission concentrations measured for the 12 test runs are presented in Table 8. As can be seen, the NO_x emission concentration was below the 2.5 ppmvd at 15 percent O_2 performance claim offered by CCSI. Also, the CO emission concentration is well below 6 ppmvd at 15 percent O_2 . In addition, the unburned hydrocarbons concentrations were very low and virtually undetectable during the 12 test runs.

Table	e 8. Pollutant E	mission Concentrati	ons for Xonon™ V	erification Test
	Ambient	NO _x	CO (nnmyd @ 15% O.)	UHC (as pro

Run	Ambient Temp. (°F)	NO _x (ppmvd @ 15% O ₂)	CO (ppmvd @ 15% O₂)	UHC (as propane) (ppmvw)
1	59	1.15	1.19	0.17
2	61	1.14	1.71	0.16
3	63	1.08	1.50	0.17
4	77	1.06	1.10	0.15
5	75	1.11	1.03	0.17
6	70	1.13	1.22	0.15
7	58	1.22	1.10	0.18
8	61	1.17	1.02	0.13
9	63	1.13	1.19	0.20
10	69	1.14	1.91	0.12
11	71	1.12	1.88	0.18
12	74	1.13	1.46	0.19

5.1.1 Statistical Analysis of Variance

This section describes the statistical analysis of the verification test data. As discussed in Section 3.1, detection of ambient temperature effects required wide swings in daily temperature,

which did not occur during the test period. The measured values from the verification test are compared to the performance capability range specified by CCSI. The first step in the statistical analysis was to perform the analysis of variance of NO_x concentration on ambient temperature. This step determines if ambient temperature has a significant effect on NO_x emissions at the 95 percent confidence level.

The analysis of variance produced a P-value of 0.1647. Only when the P-value is less than 0.05 would the ambient temperature have a significant effect on NO_x at the 95 percent confidence level. Therefore, the turbine's NO_x emissions were not affected by ambient temperature over the range of 58°F to 77°F.

5.1.2 Variability of NO_x Emissions

Because NO_x emissions were not a function of ambient temperature, the 95 percent confidence interval was calculated for the entire 12-run data set. The 95 percent confidence interval was found to be ± 0.026 ppmvd at 15 percent O_2 . Therefore, the NO_x emission concentration for this verification test can be stated as follows:

 1.13 ± 0.026 ppmvd at 15 percent O₂ at the 95 percent confidence level.

5.2 Discussion of QA/QC and QA Statement

Extensive QA/QC was applied to this verification test, much more than is typically applied to an emissions test. The following QA and QC activities were part of this test:

- A DQO for the NO_x concentration measurement,
- Reference method QC checks,
- A technical system audit to evaluate all components of the data gathering and data management system,
- A performance evaluation sample to check the operation of the NO_x measurement system, and
- A data audit of 30 percent of the critical measurement (NOx concentration) and 10 percent of the noncritical measurement.

The results of each of these QA and QC checks are presented in Sections 5.2.1 through 5.2.3.

5.2.1 NO_x Measurement DQO

The DQO for the NO_x emission concentration measurement was stated in the test/QA plan as follows:

For the NO_x emission concentration measurements, the overall NO_x emission must be within ± 10 percent of the mean emission concentration above 5 ppmvd, ± 25 percent below 5 and above 2 ppmvd, and ± 50 percent below 2 ppmvd.

The DQO was computed as the half-width of the 95 percent confidence interval of the mean divided by the mean. Since ambient temperature was not significant, all 12 test runs were included in the DQO assessment.

As presented in Section 5.1.2, the half-width of the 95 percent confidence interval was 0.026 ppmvd at 15 percent O_2 and the mean NO_x concentration was 1.13 ppmvd at 15 percent O_2 . Therefore, the DQO for NO_x equates to 2.3 percent, well within the DQO limit of 50 percent below 2 ppmvd.

5.2.2 Reference Method QC

The reference methods used to measure emission concentrations of NO_x, O₂/CO₂, CO, and UHCs have specific QC criteria that must be met. The QC criteria ensure the accuracy and stability of the measurement system and are summarized in Table 9. The results of the reference method QC checks are summarized in Sections 5.2.2.1 through 5.2.2.7. The raw data for the OC checks are in Appendix A.

Table 9. Reference Method QC Criteria

Method	Check	Criteria
wethod	Check	Criteria
Method 205	Dilution error	± 2% of reference value
Method 20	Interference NO ₂ converter efficiency Response time Calibration error Drift	 2% of span 98% < 30 s ± 2% of span ± 2% of span
Method 10	Calibration error System bias Drift	\pm 2% of span \pm 5% of span \pm 3% of span
Method 25A	Calibration error Drift	± 5% of gas value ± 3% of span
Method 1	Traverse point	± 1 inch

5.2.2.1 Method 205 Dilution System Verification—

A gas dilution system was used to generate the targeted calibration gas concentrations from single, high-concentration EPA protocol gases specific to each analyzer. This dilution system must be verified in the field before each test program according to EPA Method 205 procedures. The dilution system verification was done with the NO_x analyzer on a 0- to 50-ppmv measurement range. The results of

Table 10. Method 205 Summary Data Verification of Mass Flow Controllers 1 and 2

Standard Calibration Points	Reference Value Concentration (ppmv)	Average Analyzer Reading (ppmv)	Error (%)	
Low dilution	24.90	24.64	1.03	
Mid-level supply	25.59	25.46	0.52	
Upper dilution	44.90	45.08	-0.40	

the verification of MFCs 1 and 2 and 1 and 3 are presented in Tables 10 and 11, respectively. For acceptable performance, the three-injection average at the low and high dilution points and

the mid-level supply gas must be within ±2 percent of the reference value. As indicated in Tables 10 and 11, all dilution points were within the required ±2 percent.

5.2.2.2 Interference Test—

Before an analyzer is used, it must be demonstrated that other gases in the effluent do not interfere with the measurement technique. This test was done for

Table 11. Method 205 Summary Data Verification of Mass Flow Controllers 1 and 3

Standard Calibration Points	Reference Value Concentration (ppmv)	Average Analyzer Reading (ppmv)	Error (%)	
Low dilution	25.07	24.64	1.73	
Mid-level supply	25.59	25.29	1.18	
Upper dilution	45.10	44.87	0.51	

the NO_x , CO, O_2 , and CO_2 analyzers as required by the reference method. For acceptable performance the total interference from all the gases injected must be ± 2 percent or less. The interference results are presented in Table 12. Those results show that none of the analyzers exhibited unacceptable interference.

5.2.2.3 NO₂ Converter Efficiency Test—

Before each test program, the NO_x analyzer must demonstrate that the NO_2 converter is at least 98 percent efficient. The performance criteria state that, during the 30-min NO_2 converter efficiency test, the last NO_x analyzer reading must not decrease by more than 2 percent from the highest reading. The NO_2 converter showed a 0.2 percent decrease (5.02 ppmv was the highest reading and 5.01 ppmv was the last reading), well within the criteria for an acceptable converter. During the entire NO_2 converter efficiency test, the readings ranged from 4.97 to 5.02 ppmv.

Table 12. Analyzer Interference Results

	Interference
Analyzer	(% span)
NO _x	-0.25
CO	-1.80
O_2	0.80
CO_2	1.50

5.2.2.4 Response Time Test—

A response time test was done for NO_x, O₂, CO₂, and UHCs. Method 20 requires a response time of 30 s or less. The results of the response time tests are summarized in Table 13.

	Table 13.	Response	Times	(seconas)
_	NO _x	O ₂	CO ₂	UHCs
_	27	25	24	19
-				

5.2.2.5 Method 20 Calibrations—

For Method 20, the two calibration criteria are calibration error (± 2 percent of span) and drift (± 2 percent of span). The largest calibration error and drift for the NO_x, O₂, and CO₂ analyzers are presented in Table 14. See Appendix A, Pre- and Post-test Calibration Results. As shown in Table 14, all calibration criteria were met.

5.2.2.6 Method 10 Calibrations—

For Method 10 as performed for this test, the three calibration criteria are calibration error (±2 percent of span), system bias (±5 percent of span), and drift (±3 percent of span). The largest absolute calibration error was 0.46 percent, the largest system bias was -1.28 percent, and the largest drift was -0.44 percent. See Appendix A, Pre- and Post-Test Calibration Results. All calibration criteria were met.

Table 14. Method 20 Calibration
Error and Drift Results

	Largest Absolute Calibration Error (%)	Largest Drift (%)
NO _x	-0.55	1.15
O_2	0.46	0.32
CO ₂	0.43	1.20

5.2.2.7 Method 25A Calibrations—

For Method 25A, the two calibration criteria are calibration error (±5 percent of the gas value) and drift (±3 percent of span). The largest calibration error was -0.39 percent and the largest drift was -0.42 percent. See Appendix A, Pre- and Post-test Calibration Results. All calibration criteria were met.

5.2.3 Audits

Independent systematic checks to determine the quality of the data were performed throughout this project. These checks consisted of a technical system audit, a performance evaluation audit, and a data audit as described in Sections 5.2.3.1 through 5.2.3.3. The combination of these three audits and the evaluation of the method's QC data allowed the assessment of the overall quality of the data for this project. MRI's Task Leader managed the collection of and reviewed the field data as detailed in Sections B10.1, C1.1, and C1.2 of the test/QA plan.

5.2.3.1 Technical System Audit—

The technical system audit (TSA) was conducted by Robert Wright, RTI Quality Manager, and Michael Tufts of ARCADIS Geraghty and Miller, an EPA contractor. This audit evaluated all components of the data gathering and management system to determine if these systems had been properly designed to meet the QA objectives for this study. The TSA included a careful review of the experimental design, the test plan, and procedures. This review included personnel qualifications, adequacy and safety of the facilities and equipment, standard operating procedures (SOPs), and the data management system.

The TSA began with the review of study requirements, procedures, and experimental design to ensure that they met the data quality objectives for the study. During the system audit, the Task QA Officer inspected the analytical activities and determined their adherence to the SOPs and the test/QA plan.

The draft summary of Wright's TSA is provided in Appendix A. In general, the TSA found that the test program, as conducted, met all the data quality objectives for the study.

5.2.3.2 Performance Evaluation Audit—

A performance evaluation (PE) audit was conducted by Mike Tufts for EPA. For the PE audit, a performance evaluation sample (PES) was supplied to check the operation of the NO_x analytical system. The PES was measured for 6 continuous minutes on two occasions for a total of 12 measurements. The NO_x measurement systems read the 1.00 ppmv NO_x PES as 0.991 ± 0.012 ppmv at the 95 percent confidence level. A summary of the performance evaluation audit is presented in Table 15.

The method performance also was assessed using the method QC samples described in Sections 5.2.2.1 through 5.2.2.7.

5.2.3.3 Data Audit—

The data audit, an important component of a total system audit, was completed to determine if systematic errors were introduced. The data audit was performed by Jack Balsinger, the MRI task QA officer, by randomly selecting approximately 30 percent of the NO_x data and 10 percent of the remaining data and following them through the calculations. The scope of the data audit was to verify that the data-handling

Table 15. NO_x Analyzer Performance Evaluation Audit

Time	NO _x System Readings (ppmv)
10:27	1.02
10:28	1.02
10:29	0.99
10:30	0.99
10:31	0.98
10:32	0.98
16:29	1.01
16:30	1.00
16:31	0.99
16:32	0.98
16:33	0.97
16:34	0.96
Mean	0.9908
Confidence Interval (95 percent)	0.0119

system was correct and to assess the quality of the data generated. The data review and data audit were conducted in accordance with MRI standard procedures.

In addition to the data audit, a data check was performed by James Surman of MRI. The data check was conducted to find errors in transposing data from the raw data printouts to the calculation sheets in the Microsoft Excel spreadsheets. Data were reviewed for completeness, and the method QC results were checked for acceptability. The Microsoft Excel spreadsheets were checked for accuracy relative to the reference method requirements, and simulated data were used to check the accuracy of the computations. Three minor errors were found and corrected. Two errors were typographical, and one error was a spreadsheet format error.

5.3 Deviations from Test Plan

One deviation from the test plan was experienced during the field test, and one corrective action was taken.

The test/QA plan indicated that an eight-point traverse—four points on one diagonal traverse and four points on another diagonal traverse—was to be done during the Method 20 sampling.

However, because of the arrangement of the scaffolding, only one of the sampling ports could be reached safely. Therefore, only four traverse points on the one diagonal traverse were used. Each point was sampled for 4 minutes during two passes to maintain the 32-min test duration.

While attempting to perform the Method 205 validation test on the dilution system, the NO_x analyzer's output was nonlinear. This issue was resolved by making an adjustment to the analyzer's photomultiplier tube in accordance with the operator's manual. Once the adjustment was made, the analyzer response was linear across the measurement range.

In addition, the auditors noted that the test/QA plan (RTI, 2000b) incorrectly stated that the CO_2 calibration gas consisted of CO_2 in air. It was actually CO_2 in nitrogen.

Section 6.0

References

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APPENDIX A

QA/QC Activities and Results

- A.1 Pre- and Post-test Calibration Results
- A.2 Reference Method Performance Audit Results
- A.3 Letter Summarizing Results of Technical System Audit and Performance Evaluation

A.1 Pre- and Post-test Calibration Results

Job No. 101494.1.004.02 Operator: Daniel Neal Client: CCSI Date: 18-Jul-00 Plant: Gianera Generating Station Location: Gas Turbine Outlet Analyzer Type: Analyzer Mfgr.: Thermo Environmental Instr. Chemiluminescent 20 ppmv NO_X Analyzer Span: Model No. 42H

 Zero Gas:
 Prepurified nitrogen
 Serial No. 42H-41111-264

 High-level Gas:
 Nitrogen oxide in nitrogen

Mid-level Gas: Nitrogen oxide in nitrogen

Low-level Gas: Nitrogen oxide in nitrogen

	System Calibration Check Data						Start	<u>End</u>
Run No. 1	1 Load	Condition:	100				7:00	7:32
Calibration After Run	Calibration Gas		Response Agreement	Difference (Drift)	Drift			
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	ppmv NO _x	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
5:11	Zero Gas	0.00	N/A	-0.03	0.04		0.35%	Pass
5:53	High-level	17.04	ALM048090	17.14		Pass		
5:50	Mid-level	10.03	ALM048090	10.03	10.03		0.00%	Pass
5:58	Low-level	5.02	ALM048090	4.94		Pass		
_	Predicted value from linear curve, ppmv NO _X				Difference as % of Span			
Hig	gh-level: 17.06	Low-level:	5.01		High-level:	0.40%	Low-level:	-0.33%

a. Responses before run must agree with predicted value on linear curve within 2% of the span value.

1	Reading	Dow	nscale Response,	seconds	Upscale	Response, s	econds
١	1	26			24		
١	2	29			24		
ı	3	26	Average:	27	25	Average:	24
	System Response Time (slower average time) = 27 seconds						

	System Calibration Check Data (continued)						Start	End
Run No.	2 Load	Condition:	100				8:10	8:42
Calibration After Run Calibration Gas		Analyzer Response Value, ppmv NO _x		Response Agreement	Difference (Drift)	Drift		
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	ppmv NO _x	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
8:48	Zero Gas	0.00	N/A	0.04	0.04		0.00%	Pass
	High-level	N/A	N/A	N/A		N/A	, in the second	
9:01	Mid-level	10.03	ALM048090	10.03	9.92		-0.55%	Pass
	Low-level	N/A	N/A	N/A		N/A		
	Predicted value from linear curve, ppmv NO _X					ifference as	% of Span	
H	igh-level: N/A	Low-level:	N/A		High-level:	N/A	Low-level:	N/A

Run No.	3 Load	d Condition:	100			Run Time:	9:20	9:52
Calibration After Run	Ca	Calibration Gas		Analyzer Response Value, ppmv NO _x		,		Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	ppmv NO _x	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
9:55	Zero Gas	0.00	N/A	0.04	0.04		0.00%	Pass
	High-level	N/A	N/A	N/A		N/A		
10:07	Mid-level	10.03	ALM048090	9.92	9.86		-0.30%	Pass
	Low-level	N/A	N/A	N/A		N/A		
	Predicted value fi	om linear cur	ve, ppmv NO _x			Difference as	% of Span	
Н	igh-level: N/A	Low-level:	N/A		High-level:	N/A	Low-level:	N/A

b. Drift check must not exceed ±2% of the span value.

Job No. 101494.1.004.02 Operator: Daniel Neal

Client: CCSI Date: 18-Jul-00

Plant: Gianera Generating Station

Location: Gas Turbine Outlet

Analyzer Type: Chemiluminescent Analyzer Mfgr.: Thermo Environmental Instr.

Analyzer Span: 20 ppmv NO_X Model No. 42H

Zero Gas: Prepurified nitrogen Serial No. 42H-41111-264

High-level Gas: Nitrogen oxide in nitrogen

Mid-level Gas:

Nitrogen oxide in nitrogen

Nitrogen oxide in nitrogen

Nitrogen oxide in nitrogen

System Calibration Check Data Run Time: **Start End** Run No. 4 **Load Condition:** 16:40 17:12 Calibration Analyzer Response Response Difference **Calibration Gas** Value, ppmv NO_X After Run Agreement (Drift) Drift **Ending** Concentration Value, Cylinder Before After with After Run, Check Level Time ppmv NO_x **ID Number** Run Run Curve^a % of Span Result^b 15:20 0.00 Zero Gas N/A 0.02 0.03 0.05% Pass 15:50 High-level 17.04 ALM048090 16.93 Pass 15:46 Mid-level 10.03 ALM048090 9.94 9.91 -0.15% **Pass** 15:53 Low-level 5.02 ALM048090 4.92 Pass Predicted value from linear curve, ppmv NO_x Difference as % of Span High-level: 16.87 Low-level: 4.98 0.28% High-level: Low-level: -0.32%

Reading	Downscale Response, seconds			Upscale Response, seconds				
1	N/A			N/A				
2	N/A			N/A				
3	N/A	Average:	N/A	N/A	Average:	N/A		
	System Response Time (slower average time) = N/A seconds							

	System Calib	ration Che	ck Data (cont	inued)		Run Time:	Start	<u>End</u>
Run No.	5 Load	Condition:	100				17:50	18:22
Calibration After Run	Cal	bration Gas		-	Response pmv NO _x	Response Agreement	Difference (Drift)	Drift
Ending	Concentration Value, Cylinder				After	with	After Run,	Check
Time	Level	ppmv NO _x	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
18:28	Zero Gas	0.00	N/A	0.03	0.03		0.00%	Pass
	High-level	N/A	N/A	N/A		N/A		
18:41	Mid-level	10.03	ALM048090	9.91	9.93		0.10%	Pass
	Low-level	N/A	N/A	N/A		N/A		
	Predicted value from		ifference as	% of Span				
н	igh-level: N/A	Low-level:	N/A		High-level:	N/A	Low-level:	N/A

Run No.	6 Load	Condition:	100			Run Time:	18:58	19:30
Calibration	Cali	Calibration Gas		Analyzer	Analyzer Response		Difference	
After Run	Call	Calibration Gas			pmv NO _x	Agreement	(Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	ppmv NO _X	ID Number	Run	Run	Curve ^a	% of Span	Result
19:35	Zero Gas	0.00	N/A	0.03	0.03		0.00%	Pass
	High-level	N/A	N/A	N/A		N/A		
19:47	Mid-level	10.03	ALM048090	9.93	9.90		-0.15%	Pass
	Low-level	N/A	N/A	N/A		N/A		
	Predicted value from linear curve, ppmv NO _X					ifference as	% of Span	
н	ligh-level: N/A	N/A		High-level:	N/A	Low-level:	N/A	

a. Responses before run must agree with predicted value on linear curve within 2% of the span value.

b. Drift check must not exceed ±2% of the span value.

Job No. 101494.1.004.02 Operator: Daniel Neal

Client: CCSI Date: 19-Jul-00

Plant: Gianera Generating Station

Location: Gas Turbine Outlet

Analyzer Type: Chemiluminescent Analyzer Mfgr.: Thermo Environmental Instr.

 Analyzer Span:
 20
 ppmv NO_X
 Model No.
 42H

 Zero Gas:
 Prepurified nitrogen
 Serial No.
 42H-41111-264

High-level Gas: Nitrogen oxide in nitrogen

Mid-level Gas: Nitrogen oxide in nitrogen

Low-level Gas: Nitrogen oxide in nitrogen

	System	Calibratio	n Check Data	1		Run Time:	<u>Start</u>	End
Run No.	7 Load	Condition:	100				6:40	7:12
Calibration After Run	Cali	bration Gas			Response opmv NO _X	Response Agreement	Difference (Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	ppmv NO _x	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
4:41	Zero Gas	0.00	N/A	0.00	0.02		0.10%	Pass
5:56	High-level	17.04	ALM048090	16.80	}	Pass		
5:53	Mid-level	10.03	ALM048090	9.95	9.74		-1.05%	Pass
6:00	Low-level	5.02	ALM048090	4.87		Pass		
	Predicted value from linear curve, ppmv NO _X					Difference as	s % of Span	
+	ligh-level: 16.90	Low-level:	4.98	'	High-level:	-0.52%	Low-level:	-0.55%

a. Responses before run must agree with predicted value on linear curve within 2% of the span value.

Reading	Dow	nscale Response,	seconds	Upscal	e Response, s	econds
1	N/A			N/A		
2	N/A			N/A		
3	N/A	Average:	N/A	N/A	Average:	N/A
	Systen	n Response Time	e (slower ave	rage time) =	N/A	seconds

	System Calib	ration Che	ck Data (cont	inued)		Run Time:	Start	End
Run No.	8 Load	Condition:	100				7:45	8:17
Calibration After Run	Cali	bration Gas		-	Response pmv NO _x	Response Agreement	Difference (Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	ppmv NO _x	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
8:21	Zero Gas	0.00	N/A	0.02	0.03		0.05%	Pass
	High-level	N/A	N/A	N/A		N/A		
8:33	Mid-level	10.03	ALM048090	9.74	9.58		-0.80%	Pass
	Low-level	N/A	N/A	N/A		N/A		
	Predicted value from	om linear cur	ve, ppmv NO _x			Difference as	% of Span	
н	igh-level: N/A	Low-level:	N/A		High-level:	N/A	Low-level:	N/A

Run No.	9 Load	Condition:	100			Run Time:	8:50	9:22
Calibration After Run	Calil	oration Gas		Analyzer Response Value, ppmv NO _X		Response Agreement	Difference (Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	ppmv NO _x	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
9:30	Zero Gas	0.00	N/A	0.03	0.03		0.00%	Pass
	High-level	N/A	N/A	N/A		N/A		
9:43	Mid-level	10.03	ALM048090	9.58	9.55		-0.15%	Pass
	Low-level	N/A	N/A	N/A		N/A		
	Predicted value fro	m linear cur			Difference as	s % of Span		
Нī	ah-level: N/A	Low-level:	N/A		High-level:	N/A	Low-level:	N/A

b. Drift check must not exceed ±2% of the span value.

${ m NO_X}$ Measurement System Calibration Data By Method 20

Job No.	101494.1.004.02	Operator:	Daniel Neal	
Client:	CCSI	Date:	19-Jul-00	
Plant:	Gianera Generating Station			
Location:	Gas Turbine Outlet			

	System Calib	ration Che	ck Data (con	tinued)		Run Time:	Start	End
Run No.	10 Load	Condition:	100				11:20	11:52
Calibration After Run	Cal	ibration Gas		1	Response pmv NO _X	Response Agreement	Difference (Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run.	
Time	Level	ppmv NO _x	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
11:58	Zero Gas	0.00	N/A	0.03	0.02		-0.05%	Pass
	High-level	N/A	N/A	N/A		N/A		
12:09	Mid-level	10.03	ALM048090	9.55	9.78		1.15%	Pass
	Low-level	N/A	N/A	N/A		N/A		
	Predicted value fr	ve, ppmv NO _X			ifference as	% of Span		
۲	ligh-level: N/A	Low-level:	N/A		High-level:	N/A	Low-level:	N/A

Run No.	11 Load	Condition:	100			Run Time:	12:30	13:02
Calibration After Run	Calil	oration Gas		•	Response pmv NO _x	Response Agreement	Difference (Drift)	Drift
Ending Time	Concentration Level	Value, ppmv NO _x	Cylinder ID Number	Before Run	After Run	with Curve ^a	After Run, % of Span	Check Result ^b
13:10	Zero Gas	0.00	N/A	0.02	0.00		-0.10%	Pass
	High-level	N/A	N/A	N/A		N/A		
13:21	Mid-level	10.03	ALM048090	9.78	9.78		0.00%	Pass
	Low-level	N/A	N/A	N/A		N/A		
	Predicted value fro	m linear cur	ve, ppmv NO _x			ifference as	% of Span	
Hi	gh-level: N/A	Low-level:	N/A		High-level:	N/A	Low-level:	N/A

Run No.	12 Load	Condition:	100			Run Time:	13:36	14:08
Calibration	Cali	Calibration Gas			Response	Response	Difference	
After Run	Jan	Calibration Gas			pmv NO _x	Agreement	(Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	ppmv NO _x	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
14:12	Zero Gas	0.00	N/A	0.00	0.02		0.10%	Pass
	High-level	N/A	N/A	N/A		N/A		
14:25	Mid-level	10.03	ALM048090	9.78	9.77		-0.05%	Pass
	Low-level	N/A	N/A	N/A		N/A		
Predicted value from linear curve, ppmv NO _x Difference as % of Span								
н	igh-level: N/A	Low-level:	N/A		High-level:	N/A	Low-level:	N/A

Job No.	101494.	.1.004.02		Operator:	Daniel Neal
Client:	CCSI Gianera Generating Station Gas Turbine Outlet Zer Type: NDIRS with GFC		Date:	18-Jul-00	
Plant:	Gianera	a Generating	Station	<u>-</u>	
Location:	Gas Tu	rbine Outlet		- -	
Analyzer 7	Гуре:	NDIRS with	GFC	_ Analyzer Mfgr.:	Thermo Environmental Instr.
Analyzer S	Span:	50	_ppmv CO	Model No.	48
Zero Gas:		Prepurifie	d nitrogen	Serial No.	48-29095-233
Cal. Gas I	Mixture:	Carbon m	onoxide in nitrogen	_	

Ana	alyzer Calibratio	termination	Run Time:	Start	End		
Run No. 1	Load	Condition:	100			7:00	7:32
Calibration	Calil	oration Gas		Analyzer Response	Response	Cal. Error	Linearity
Ending	Concentration	Value,	Cylinder	Value Following	Difference,	Check	Check
Time	Level	ppmv CO	ID Number	Calibration, ppmv CO	% of Span	Result	Result ^b
4:50	Zero Gas	0.00	N/A	0.07	0.14%	Pass	
4:58	High-range	44.90	AAL17607	45.13	0.46%	Pass	
5:01	Mid-range	29.90	AAL17607	30.03	0.26%	Pass	Pass
5:04	Low-range	15.00	AAL17607	15.01	0.02%	Pass	Pass
	Predicted value	ם	Difference as	s % of Span			
Range	e: Mid = 30.08	Low =	15.12	Mid =	-0.09%	Low =	-0.23%

a. Calibration error check must not exceed ±2% of the span value.

Measurement System Calibration Bias, Response Time, and Drift

	Initial Bias and Response Time Determinations									
Calibration	Calibration Gas	Analyzer	System	Response	System	Bias				
Ending	Concentration	Response,	Response,	Time ^c ,	Cal. Bias,	Check				
Time	Level	ppmv CO	ppmv CO	seconds	% of Span	Result ^d				
5:13	Zero Gas	0.07	0.03	62	-0.08%	Pass				
6:01	Mid-range	30.03	29.79	56	-0.48%	Pass				

	Final Bias and Drift Determinations									
Calibration Ending Time	Calibration Gas Concentration Level	System Response, ppmv CO	System Cal. Bias, % of Span	Bias Check Result ^d	Drift, % of Span	Drift Check Result ^e				
7:37 7:54	Zero Gas Mid-range	0.00 29.57	-0.14% -0.92%	Pass Pass	-0.06% -0.44%	Pass Pass				

c. Response time check according to Method 6C. The longer time is used.

b. Responses before run must agree with predicted value on linear curve within 2% of the span value.

d. System bias check must not exceed $\pm 5\%$ of the span value.

e. Drift check must not exceed ±3% of the span value.

 Job No.
 101494.1.004.02
 Operator:
 Daniel Neal

 Client:
 CCSI
 Date:
 18-Jul-00

 Plant:
 Gianera Generating Station

Analyzer Calibration Error and Linearity Determination Run Time: <u>Start</u> **End** Load Condition: Run No. 2 100 8:10 8:42 **Calibration Gas** Calibration **Analyzer Response** Response Cal. Error Linearity Ending Concentration Value, Cylinder Value Following Difference, Check Check ppmv CO **ID Number** Time Level Calibration, ppmv CO % of Span Result Result 4:50 Zero Gas 0.00 N/A 0.07 0.14% **Pass** 4:58 AAL17607 High-range 44.90 45.13 0.46% **Pass** 5:01 29.90 Mid-range AAL17607 30.03 0.26% **Pass Pass** 5:04 15.00 AAL17607 15.01 Low-range 0.02% Pass Pass Predicted value from linear curve, ppmv CO Difference as % of Span 30.08 Range: Mid = Low = 15.12 Mid = -0.09% Low = -0.23%

Measurement System Calibration Bias and Drift

Initial Bias Determination							
Calibration Ending	Calibration Gas Concentration	Analyzer Response,	System Response,	System Cal. Bias,	Bias Check		
Time	Level	ppmv CO	ppmv CO	% of Span	Result		
7:37	Zero Gas	0.07	0.00	-0.14%	Pass		
7:54	Mid-range	30.03	29.57	-0.92%	Pass		

	Final Bias and Drift Determinations								
Calibration	Calibration Gas	System	System	Bias		Drift			
Ending	Concentration	Response,	Cal. Bias,	Check	Drift,	Check			
Time	Level	ppmv CO	% of Span	Result	% of Span	Result			
8:48	Zero Gas	0.00	-0.14%	Pass	0.00%	Pass			
9:06	Mid-range	29.55	-0.96%	Pass	-0.04%	Pass			

Analyzer Calibration Error and Linearity Determination						<u>Start</u>	<u>End</u>
Run No.	3 Load	Condition:	100			9:20	9:52
Calibration	Cali	oration Gas		Analyzer Response	Response	Cal. Error	Linearity
Ending	Concentration	Value,	Cylinder	Value Following	Difference,	Check	Check
Time	Level	ppmv CO	ID Number	Calibration, ppmv CO	% of Span	Result	Result
4:50	Zero Gas	0.00	N/A	0.07	0.14%	Pass	
4:58	High-range	44.90	AAL17607	45.13	0.46%	Pass	
5:01	Mid-range	29.90	AAL17607	30.03	0.26%	Pass	Pass
5:04	Low-range	15.00	AAL17607	15.01	0.02%	Pass	Pass
Predicted value from linear curve, ppmv CO					Difference as	% of Span	
Rang	ge: Mid = 30.08	Low =	15.12	Mid =	-0.09%	Low =	-0.23%

Measurement System Calibration Bias and Drift

			Initial Bias De	termination	
Calibration	Calibration Gas	Analyzer	System	System	Bias
Ending	Concentration	Response,	Response,	Cal. Bias,	Check
Time	Level	ppmv CO	ppmv CO	% of Span	Result
8:48	Zero Gas	0.07	0.00	-0.14%	Pass
9:06	Mid-range	30.03	29.55	-0.96%	Pass

Final Bias and Drift Determinations									
Calibration Ending Time	Calibration Gas Concentration Level	System Response,	System Cal. Bias, % of Span	Bias Check Result	Drift, % of Span	Drift Check Result			
9:56 10:10	Zero Gas Mid-range	-0.07 29.39	-0.28% -1.28%	Pass Pass	-0.14% -0.32%	Pass Pass			

Location:

Gas Turbine Outlet

Job No.	101494.	1.004.02	Operator:	Daniel Neal
Client:			_ Date:	18-Jul-00
Plant:			_	
Location: Gas Turbin		bine Outlet	<u>-</u>	
Analyzer T	уре:	NDIRS with GFC	_ Analyzer Mfgr.:	Thermo Environmental Instr.
Analyzer S	Span:	ppmv CO	Model No.	48
Zero Gas:		Prepurified nitrogen	Serial No.	48-29095-233
0-1 0 1	disduser.	Onethan managed to the other way		

Ana	alyzer Calibratio	Run Time:	Start	End			
Run No. 4	Load	Condition:	100			16:40	17:12
Calibration	Cali	bration Gas		Analyzer Response	Response	Cal. Error	Linearity
Ending	Concentration	Value,	Cylinder	Value Following	Difference,	Check	Check
Time	Level	ppmv CO	ID Number	Calibration, ppmv CO	% of Span	Result	Result ^b
15:01	Zero Gas	0.00	N/A	-0.07	-0.14%	Pass	
15:06	High-range	44.90	AAL17607	44.98	0.16%	Pass	
15:10	Mid-range	29.90	AAL17607	30.01	0.22%	Pass	Pass
15:14	Low-range	15.04	AAL17607	14.90	-0.28%	Pass	Pass
	Predicted value		Difference as	% of Span			
Rang	e: Mid = 29.93	Low =	15.02	Mid =	0.16%	Low =	-0.24%

a. Calibration error check must not exceed ±2% of the span value.

Measurement System Calibration Bias, Response Time, and Drift

	Initial Bias and Response Time Determinations									
Calibration	Calibration Gas	Analyzer	System	Response	System	Bias				
Ending	Concentration	Response,	Response,	Time ^c ,	Cal. Bias,	Check				
Time	Level	ppmv CO	ppmv CO	seconds	% of Span	Result ^d				
15:58	Zero Gas	-0.07	0.09	56	0.32%	Pass				
16:05	Mid-range	30.01	29.95	57	-0.12%	Pass				

Final Bias and Drift Determinations								
Calibration Ending	Calibration Gas Concentration	System Response,	System Cal. Bias,	Bias Check Result ^d	Drift,	Drift Check		
17:19	Level Zero Gas	ppmv CO	% of Span 0.14%	Pass	% of Span -0.18%	Result*		
17:37	Mid-range	29.88	-0.26%	Pass	-0.14%	Pass		

c. Response time check according to Method 6C. The longer time is used.

System Calibration Bias	= System Cal. Response - Analyzer Cal. Response Span	— x 100
Drift =	Final System Cal. Response - Initial System Cal. Response	— x 100
Dill -	Span	× 100

b. Responses before run must agree with predicted value on linear curve within 2% of the span value.

d. System bias check must not exceed $\pm 5\%$ of the span value.

e. Drift check must not exceed ±3% of the span value.

 Job No.
 101494.1.004.02
 Operator:
 Daniel Neal

 Client:
 CCSI
 Date:
 18-Jul-00

 Plant:
 Gianera Generating Station
 Date:
 18-Jul-00

Ana	alyzer Calibratio	n Error and	Linearity De	etermination	Run Time:	Start	End
Run No. 5	Load	Condition:	100			17:50	18:22
Calibration	Cal	ibration Gas		Analyzer Response	Response	Cal. Error	Linearity
Ending	Concentration	Value,	Cylinder	Value Following	Difference,	Check	Check
Time	Level	ppmv CO	ID Number	Calibration, ppmv CO	% of Span	Result	Result
15:01	Zero Gas	0.00	N/A	-0.07	-0.14%	Pass	
15:06	High-range	44.90	AAL17607	44.98	0.16%	Pass	
15:10	Mid-range	29.90	AAL17607	30.01	0.22%	Pass	Pass
15:14	Low-range	15.04	AAL17607	14.90	-0.28%	Pass	Pass
	Predicted value	from linear o	urve, ppmv CO		Difference as	% of Span	
Range	e: Mid = 29.93	Low =	15.02	Mid =	0.16%	Low =	-0.24%

Measurement System Calibration Bias and Drift

			Initial Bias De	etermination		
Calibration Ending Time	Calibration Gas Concentration Level	Analyzer Response, ppmv CO	System Response, ppmv CO	System Cal. Bias, % of Span	Bias Check Result	
17:19 17:37	Zero Gas Mid-range	-0.07 30.01	0.00 29.88	0.14% -0.26%	Pass Pass	

		Final	Bias and Drif	t Determin	ations	
Calibration	Calibration Gas	System	System	Bias		Drift
Ending	Concentration	Response,	Cal. Bias,	Check	Drift,	Check
Time	Level	ppmv CO	% of Span	Result	% of Span	Result
18:29	Zero Gas	0.02	0.18%	Pass	0.04%	Pass
18:45	Mid-range	29.81	-0.40%	Pass	-0.14%	Pass

Ana	alyzer Calibratio	n Error and	l Linearity De	termination	Run Time:	Start	End
Run No. 6	Load	Condition:	100			18:58	19:30
Calibration	Cali	bration Gas		Analyzer Response	Response	Cal. Error	Linearity
Ending	Concentration	Value,	Cylinder	Value Following	Difference,	Check	Check
Time	Level	ppmv CO	ID Number	Calibration, ppmv CO	% of Span	Result	Result
15:01	Zero Gas	0.00	N/A	-0.07	-0.14%	Pass	
15:06	High-range	44.90	AAL17607	44.98	0.16%	Pass	
15:10	Mid-range	29.90	AAL17607	30.01	0.22%	Pass	Pass
15:14	Low-range	15.04	AAL17607	14.90	-0.28%	Pass	Pass
	Predicted value	from linear o	urve, ppmv CO		Difference as	% of Span	
Rang	e: Mid = 29.93	Low =	15.02	Mid =	0.16%	Low =	-0.24%

Measurement System Calibration Blas and Drift

			Initial Bias De	etermination	
Calibration	Calibration Gas	Analyzer	System	System	Bias
Ending	Concentration	Response,	Response,	Cal. Bias,	Check
Time	Level	ppmv CO	ppmv CO	% of Span	Result
18:29	Zero Gas	-0.07	0.02	0.18%	Pass
18:45	Mid-range	30.01	29.81	-0.40%	Pass

		Final	Bias and Drift	t Determin	ations	
Calibration	Calibration Gas	System	System	Bias		Drift
Ending	Concentration	Response,	Cal. Bias,	Check	Drift,	Check
Time	Level	ppmv CO	% of Span	Result	% of Span	Result
19:36	Zero Gas	0.10	0.34%	Pass	0.16%	Pass
19:52	Mid-range	29.86	-0.30%	Pass	0.10%	Pass

Location: Gas Turbine Outlet

Job No.	101494	.1.004.02	Operator:	Daniel Neal
Client:	CCSI		Date:	19-Jul-00
Plant:	Gianera	a Generating Station	_	
Location:	Gas Tu	rbine Outlet		
Analyzer 1	уре:	NDIRS with GFC	Analyzer Mfgr.:	Thermo Environmental Instr.
Analyzer S	Span:	50 ppmv CO	Model No.	48
Zero Gas:		Prepurified nitrogen	_ Serial No.	48-29095-233
Cal. Gas I	Mixture:	Carbon monoxide in nitrogen		

An	alyzer Calibration	Error and	l Linearity De	termination	Run Time:	<u>Start</u>	<u>End</u>
Run No. 7	7 Load	Condition:	100			6:40	7:12
Calibration	Calib	ration Gas		Analyzer Response	Response	Cal. Error	Linearity
Ending	Concentration	Value,	Cylinder	Value Following	Difference,	Check	Check
Time	Level	ppmv CO	ID Number	Calibration, ppmv CO	% of Span	Resultª	Result ^b
4:25	Zero Gas	0.00	N/A	-0.07	-0.14%	Pass	
4:28	High-range	44.90	AAL17607	45.04	0.28%	Pass	
4:31	Mid-range	29.90	- AAL17607	30.12	0.44%	Pass	Pass
4:35	Low-range	15.04	AAL17607	14.98	-0.12%	Pass	Pass
	Predicted value	rom linear o	curve, ppmv CO		Difference as	% of Span	
Rang	je: Mid = 29.97	Low =	15.04	Mid =	0.30%	Low =	-0.12%

a. Calibration error check must not exceed ±2% of the span value.

Measurement System Calibration Bias, Response Time, and Drift

		Initial Bias	and Response	e Time Dete	rminations	
Calibration	Calibration Gas	Analyzer	System	Response	System	Bias
Ending	Concentration	Response,	Response,	Time ^c ,	Cal. Bias,	Check
Time	Level	ppmv CO	ppmv CO	seconds	% of Span	Result ^d
6:02	Zero Gas	-0.07	-0.03	60	0.08%	Pass
6:05	Mid-range	30.12	29.83	56	-0.58%	Pass

		Final	Bias and Drift	Determina	itions	
Calibration	Calibration Gas	System	System	Bias		Drift
Ending	Concentration	Response,	Cal. Bias,	Check	Drift,	Check
Time	Level	ppmv CO	% of Span	Result ^d	% of Span	Result*
7:17	Zero Gas	0.01	0.16%	Pass	0.08%	Pass
7:32	Mid-range	29.85	-0.54%	Pass	0.04%	Pass

c. Response time check according to Method 6C. The longer time is used.

b. Responses before run must agree with predicted value on linear curve within 2% of the span value.

d. System bias check must not exceed ±5% of the span value.

e. Drift check must not exceed ±3% of the span value.

 Job No.
 101494.1.004.02
 Operator:
 Daniel Neal

 Client:
 CCSI
 Date:
 19-Jul-00

 Plant:
 Gianera Generating Station
 19-Jul-00

An	alyzer Calibration	n Error and	Linearity De	termination	Run Time:	Start	End
Run No. 8	B Load	Condition:	100			7:45	8:17
Calibration	Calib	ration Gas		Analyzer Response	Response	Cal. Error	Linearity
Ending	Concentration	Value,	Cylinder	Value Following	Difference,	Check	Check
Time	Level	ppmv CO	ID Number	Calibration, ppmv CO	% of Span	Result	Result
4:25	Zero Gas	0.00	N/A	-0.07	-0.14%	Pass	
4:28	High-range	44.90	AAL17607	45.04	0.28%	Pass	
4:31	Mid-range	29.90	AAL17607	30.12	0.44%	Pass	Pass
4:35	Low-range	15.04	AAL17607	14.98	-0.12%	Pass	Pass
	Predicted value t	from linear c	urve, ppmv CO		Difference as	% of Span	
Rang	e: Mid = 29.97	Low =	15.04	Mid =	0.30%	Low =	-0.12%

Measurement System Calibration Bias and Drift

			Initial Bias De	termination	
Calibration	Calibration Gas	Analyzer	System	System	Bias
Ending	Concentration	Response,	Response,	Cal. Bias,	Check
Time	Level	ppmv CO	ppmv CO	% of Span	Result
7:17	Zero Gas	-0.07	0.01	0.16%	Pass
7:32	Mid-range	30.12	29.85	-0.54%	Pass

		Final	Bias and Drift	Determina	ations	
Calibration	Calibration Gas	System	System	Bias		Drift
Ending	Concentration	Response,	Cal. Bias,	Check	Drift,	Check
Time	Level	ppmv CO	% of Span	Result	% of Span	Result
8:21	Zero Gas	0.02	0.18%	Pass	0.02%	Pass
8:37	Mid-range	29.67	-0.90%	Pass	-0.36%	Pass

Ar	nalyzer Calibration	Error and	d Linearity De	termination	Run Time:	Start	End
Run No.	9 Load	Condition:	100			8:50	9:22
Calibration	Calib	ration Gas		Analyzer Response	Response	Cal. Error	Linearity
Ending	Concentration	Value,	Cylinder	Value Following	Difference,	Check	Check
Time	Level	ppmv CO	ID Number	Calibration, ppmv CO	% of Span	Result	Result
4:25	Zero Gas	0.00	N/A	-0.07	-0.14%	Pass	
4:28	High-range	44.90	AAL17607	45.04	0.28%	Pass	
4:31	Mid-range	29.90	AAL17607	30.12	0.44%	Pass	Pass
4:35	Low-range	15.04	AAL17607	14.98	-0.12%	Pass	Pass
	Predicted value t	rom linear c	urve, ppmv CO		Difference as	% of Span	
Rang	ge: Mid = 29.97	Low =	15.04	Mid =	0.30%	Low =	-0.12%

Measurement System Calibration Bias and Drift

	Initial Bias Determination						
Calibration	Calibration Gas	Analyzer	System	System	Bias		
Ending	Concentration	Response,	Response,	Cal. Bias,	Check		
Time	Level	ppmv CO	ppmv CO	% of Span	Result		
8:21	Zero Gas	-0.07	0.02	0.18%	Pass		
8:37	Mid-range	30.12	29.67	-0.90%	Pass		

		Final	Bias and Drift	Determina	ations	
Calibration	Calibration Gas	System	System	Bias		Drift
Ending	Concentration	Response,	Cal. Bias,	Check	Drift,	Check
Time	Level	ppmv CO	% of Span	Result	% of Span	Result
9:31	Zero Gas	-0.02	0.10%	Pass	-0.08%	Pass
9:49	Mid-range	29.48	-1.28%	Pass	-0.38%	Pass

Location: Gas Turbine Outlet

 Job No.
 101494.1.004.02
 Operator:
 Daniel Neal

 Client:
 CCSI
 Date:
 19-Jul-00

Plant: Gianera Generating Station

Location: Gas Turbine Outlet

Αı	nalyzer Calibratio	n Error and	Linearity De	termination	Run Time:	<u>Start</u>	<u>End</u>
Run No.	10 Load	Condition:	100			11:20	11:52
Calibration	Calil	oration Gas		Analyzer Response	Response	Cal. Error	Linearity
Ending	Concentration	Value,	Cylinder	Value Following	Difference,	Check	Check
Time	Level	ppmv CO	ID Number	Calibration, ppmv CO	% of Span	Result	Result
4:25	Zero Gas	0.00	N/A	-0.07	-0.14%	Pass	
4:28	High-range	44.90	AAL17607	45.04	0.28%	Pass	
4:31	Mid-range	29.90	AAL17607	30.12	0.44%	Pass	Pass
4:35	Low-range	15.04	AAL17607	14.98	-0.12%	Pass	Pass
	Predicted value	from linear c	urve, ppmv CO		Difference as	% of Span	
Ran	ge: Mid = 29.97	Low =	15.04	Mid =	0.30%	Low =	-0.12%

Measurement System Calibration Bias and Drift

			Initial Bias De	termination	
Calibration	Calibration Gas	Analyzer	System	System	Bias
Ending	Concentration	Response,	Response,	Cal. Bias,	Check
Time	Level	ppmv CO	ppmv CO	% of Span	Result
9:31	Zero Gas	-0.07	-0.02	0.10%	Pass
9:49	Mid-range	30.12	29.48	-1.28%	Pass

		Final	Bias and Drift	t Determina	ations	
Calibration	Calibration Gas	System	System	Bias		Drift
Ending	Concentration	Response,	Cal. Bias,	Check	Drift,	Check
Time	Level	ppmv CO	% of Span	Result	% of Span	Result
11:58	Zero Gas	-0.03	0.08%	Pass	-0.02%	Pass
12:15	Mid-range	29.68	-0.88%	Pass	0.40%	Pass

Ar	nalyzer Calibratio	n Error and	l Linearity De	termination	Run Time:	<u>Start</u>	End
Run No.	11 Load	Condition:	100			12:30	13:02
Calibration	Cali	oration Gas		Analyzer Response	Response	Cal. Error	Linearity
Ending	Concentration	Value,	Cylinder	Value Following	Difference,	Check	Check
Time	Level	ppmv CO	ID Number	Calibration, ppmv CO	% of Span	Result	Result
4:25	Zero Gas	0.00	N/A	-0.07	-0.14%	Pass	
4:28	High-range	44.90	AAL17607	45.04	0.28%	Pass	
4:31	Mid-range	29.90	AAL17607	30.12	0.44%	Pass	Pass
4:35	Low-range	15.04	AAL17607	14.98	-0.12%	Pass	Pass
	Predicted value	from linear o	urve, ppmv CO		Difference as	s % of Span	
Rang	ge: Mid = 29.97	Low =	15.04	Mid =	0.30%	Low =	-0.12%

Measurement System Calibration Bias and Drift

			Initial Bias De	termination	
Calibration Ending	Calibration Gas Concentration	Analyzer Response,	System Response,	System Cal. Bias,	Bias Check
Time	Level	ppmv CO	ppmv CO	% of Span	Result
11:58	Zero Gas	-0.07	-0.03	0.08%	Pass
12:15	Mid-range	30.12	29.68	-0.88%	Pass

		Final	Bias and Drift	Determina	tions	
Calibration Ending Time	Calibration Gas Concentration Level	System Response, ppmv CO	System Cal. Bias, % of Span	Bias Check Result	Drift, % of Span	Drift Check Result
13:10 13:25	Zero Gas Mid-range	-0.03 29.67	0.08% -0.90%	Pass Pass	0.00% -0.02%	Pass Pass

 Job No.
 101494.1.004.02
 Operator:
 Daniel Neal

 Client:
 CCSI
 Date:
 19-Jul-00

 Plant:
 Gianera Generating Station
 39-Jul-00
 39-Jul-00

Location: Gas Turbine Outlet

Ar	nalyzer Calibration	n Error and	l Linearity De	termination	Run Time:	<u>Start</u>	<u>End</u>
Run No. 1	12 Load	Condition:	100			13:36	14:08
Calibration	Calib	oration Gas		Analyzer Response	Response	Cal. Error	Linearity
Ending	Concentration	Value,	Cylinder	Value Following	Difference,	Check	Check
Time	Level	ppmv CO	ID Number	Calibration, ppmv CO	% of Span	Result	Result
4:25	Zero Gas	0.00	N/A	-0.07	-0.14%	Pass	
4:28	High-range	44.90	AAL17607	45.04	0.28%	Pass	
4:31	Mid-range	29.90	AAL17607	30.12	0.44%	Pass	Pass
4:35	Low-range	15.04	AAL17607	14.98	-0.12%	Pass	Pass
	Predicted value	from linear c	urve, ppmv CO] ِ	Difference as	% of Span	
Rang	je: Mid = 29.97	Low =	15.04	Mid =	0.30%	Low =	-0.12%

Measurement System Calibration Bias and Drift

			Initial Bias De	termination	
Calibration	Calibration Gas	Analyzer	System	System	Bias
Ending	Concentration	Response,	Response,	Cal. Bias,	Check
Time	Level	ppmv CO	ppmv CO	% of Span	Result
13:10	Zero Gas	-0.07	-0.03	0.08%	Pass
13:25	Mid-range	30.12	29.67	-0.90%	Pass

		Final	Bias and Drift	Determina	itions		
Calibration	Calibration Gas	System	System	Bias		Drift	
Ending	Concentration	Response,	Cal. Bias,	Check	Drift,	Check	l
Time	Level	ppmv CO	% of Span	Result	% of Span	Result	l
14:12	Zero Gas	-0.06	0.02%	Pass	-0.06%	Pass	•
14:31	Mid-range	29.73	-0.78%	Pass	0.12%	Pass	L

Job No.

101494.1.004.02

Operator: Daniel Neal

Client:

CCSI

Date:

18-Jul-00

Plant: Location: **Gianera Generating Station**

Gas Turbine Outlet

Analyzer Type:

Magnetopneumatic

Analyzer Mfgr.: Servomex

Analyzer Span:

25. %O₂ by volume

Model No. 01440CISTD Serial No. 1391

Zero Gas:

Prepurified nitrogen

Oxygen in nitrogen

High-level Gas: Mid-level Gas:

Oxygen in nitrogen

	System	Calibration	on Check Data	a		Run Time:	<u>Start</u>	End
Run No.	1 Load	Condition:	100				7:00	7:32
Calibration	Cal	ibration Ga		Analyzer	Response	Response	Difference	
After Run Calibration Gas				Value	e, %O ₂	Agreement	(Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%O ₂	ID Number	Run	Run	Curve	% of Span	Result ^b
5:11	Zero Gas	0.00	N/A	0.04	0.11		0.28%	Pass
5:31	High-level	20.90	ALM007829	21.05		Pass		
5:29	Mid-level	11.99	ALM007829	12.06	11.99		-0.28%	Pass
	Predicted value from linear curve, %O ₂				C	ifference as	% of Span:	0.23%

a. High-level response before run must agree with predicted value on linear curve within 2% of the span value.

Reading	Dowr	nscale Response	, seconds		Response, s	
1	25			23		
2	25			25		
3	24	Average:	25	26	Average:	25
	System I	Response Time	(slower ave	rage time) =	25	seconds

	System Calib	ration Che	eck Data (cont	tinued)		Run Time:	<u>Start</u>	<u>End</u>
Run No.	2 Load	Condition:	100				8:10	8:42
Calibration	Cal	ibsotion Co		Analyzer	Response	Response	Difference	
After Run	After Run Calibration Gas			Value	e, %O ₂	Agreement	(Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%O ₂	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
8:48	Zero Gas	0.00	N/A	0.11	0.11		0.00%	Pass
	High-level	N/A	N/A	N/A		N/A		
8:53	Mid-level	11.99	ALM007829	11.99	11.98		-0.04%	Pass
	Predicted value from linear curve, %O				D	ifference as	% of Span:	N/A

Run No.	3 Load	Condition:	100			Run Time:	9:20	9:52
Calibration After Run	Cal	Calibration Gas			Response e, %O ₂	Response Agreement		Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%O₂	ID Number	Run	Run	Curve	% of Span	Result ^b
9:56	Zero Gas	0.00	N/A	0.11	0.14		0.12%	Pass
	High-level	N/A	N/A	N/A		N/A		
10:00	Mid-level	11.99	ALM007829	11.98	12.06		0.32%	Pass
	Predicted value from linear curve, %O ₂				. D	ifference as	% of Span:	N/A

b. Drift check must not exceed ±2% of the span value.

Job No.

101494.1.004.02

Date:

Operator: Daniel Neal

18-Jul-00

Client: Plant:

CCSI

Gianera Generating Station

Location:

Gas Turbine Outlet

Analyzer Type:

Magnetopneumatic

Analyzer Mfgr.: Servomex

Analyzer Span:

%O₂ by volume

Zero Gas:

Model No. 01440CISTD

Prepurified nitrogen

Serial No. 1391

High-level Gas:

Oxygen in nitrogen

Mid-level Gas:

Oxygen in nitrogen

	System	Calibration	on Check Data	a		Run Time:	Start	End
Run No.	4 Load	Condition:	100				16:40	17:12
Calibration	Calibration Gas				Response	Response	Difference	
After Run	After Run			Value	e, %O₂	Agreement	(Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%O ₂	ID Number	Run	Run	Curve	% of Span	Result ^b
15:20	Zero Gas	0.00	N/A	0.05	0.12		0.28%	Pass
· 15:25	High-level	20.90	ALM007829	20.98		Pass		
15:22	Mid-level	11.99	ALM007829	12.01	12.00		-0.04%	Pass
	Predicted value from linear curve, %O ₂				0	ifference as	% of Span:	0.33%

a. High-level response before run must agree with predicted value on linear curve within 2% of the span value.

Reading	Down	scale Response	, seconds	Upscale	Response, s	econds
1	N/A			N/A		
2	N/A			N/A		
3	N/A	Average:	N/A	N/A	Average:	N/A
	System F	Response Time	(slower ave	rage time) =	N/A	seconds

	System Calib	ration Che	eck Data (cont	tinued)		Run Time:	<u>Start</u>	<u>End</u>
Run No.	5 Load	Condition:	100				17:50	18:22
Calibration	Calibration Gas				Response	Response	Difference	
After Run	After Run Calibration Gas			Value	e, %O ₂	Agreement	(Drift)	Drift
Ending	ling Concentration Value, Cylinder				After	with	After Run,	Check
Time	Level	%O ₂	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
18:28	Zero Gas	0.00	N/A	0.12	0.12		0.00%	Pass
	High-level	N/A	N/A	N/A		N/A		
18:34	Mid-level	11.99	ALM007829	12.00	11.95		-0.20%	Pass
	Predicted value from linear curve, %C				C	ifference as	% of Span:	N/A

Run No.	6 Load	Condition:	100			Run Time:	18:58	19:30
Calibration	alibration Calibration Gas			Analyzer	Response	Response	Difference	
After Run	fter Run			Value, %O₂		Agreement	(Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%O₂	ID Number	Run	Run	Curve	% of Span	Result ^b
19:34	Zero Gas	0.00	N/A	0.12	0.08		-0.16%	Pass
	High-level	N/A	N/A	N/A		N/A		
19:39	Mid-level	11.99	ALM007829	11.95	11.95		0.00%	Pass
	Predicted value from linear curve, %O			N/A		ifference as	% of Span:	N/A

b. Drift check must not exceed ±2% of the span value.

 Job No.
 101494.1.004.02
 Operator:
 Daniel Neal

 Client:
 CCSI
 Date:
 19-Jul-00
 .

Plant: Gianera Generating Station

Location: Gas Turbine Outlet

Analyzer Type: Magnetopneumatic Analyzer Mfgr.: Servomex

Analyzer Span: 25 %O₂ by volume Model No. 01440CISTD

Zero Gas: Prepurified nitrogen Serial No. 1391

 Zero Gas:
 Prepurified nitrogen
 Serial No. 1391

 High-level Gas:
 Oxygen in nitrogen

Mid-level Gas: Oxygen in nitrogen

	System	Calibration	on Check Data	a .	•	Run Time:	<u>Start</u>	End
Run No.	7 Load	Condition:	100				6:40	7:12
Calibration	Calibration Gas				Analyzer Response		Difference	
After Run	After Run				e, %O ₂	Agreement	(Drift)	Drift
Ending Concentration Value, Cylinder				Before	After	with	After Run,	Check
Time	Level	%O ₂	ID Number	Run	Run	Curve	% of Span	Result ^b
4:41	Zero Gas	0.00	N/A	0.02	0.07		0.20%	Pass
4:51	High-level	20.90	ALM007829	20.93		Pass		
4:46	Mid-level	11.99	ALM007829	11.95	11.98		0.12%	Pass
	Predicted value from linear curve, %O ₂ :				0	ifference as	% of Span:	0.46%

a. High-level response before run must agree with predicted value on linear curve within 2% of the span value.

Reading	Dow	nscale Response	, seconds	Upscale	Response, s	seconds
1	N/A			N/A		
2	N/A			N/A		
3	N/A	Average:	N/A	N/A	Average:	N/A
	System	Response Time	(slower ave	rage time) =	N/A	seconds

	System Calib	ration Che	eck Data (cont	inued)		Run Time:	<u>Start</u>	End
Run No.	8 Load	Condition:	100				7:45	8:17
Calibration After Run	Cal	ibration Ga	s	-	Response e, %O ₂	Response Agreement	Difference	
Ending	Concentration	Value,	Cylinder	Before	After	with	(Drift) After Run,	Drift Check
Time	Level	%O₂	ID Number	Run	Run	Curve	% of Span	Result ^b
8:21	Zero Gas	0.00	N/A	0.07	0.12		0.20%	Pass
	High-level	N/A	N/A	N/A		N/A		
8:25	Mid-level	11.99	ALM007829	11.98	12.01		0.12%	Pass
	Predicted val	ear curve, %O₂:	N/A	0	ifference as	% of Span:	N/A	

Run No.	9 Load	Condition:	100			Run Time:	8:50	9:22
Calibration	n Colibration Cos			Analyzer	Response	Response	Difference	
After Run	Cai	Calibration Gas		Value, %O₂		Agreement	(Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%O₂	ID Number	Run	Run	Curve	% of Span	Result ^b
9:30	Zero Gas	0.00	N/A	0.12	0.14		0.08%	Pass
	High-level	N/A	N/A	N/A		N/A		
9:36	Mid-level	11.99	ALM007829	12.01	11.96		-0.20%	Pass
	Predicted value from linear curve, %O ₂				D	ifference as	% of Span:	N/A

b. Drift check must not exceed ±2% of the span value.

Job No.

101494.1.004.02

Operator: <u>Daniel Neal</u> Date:

19-Jul-00

Client: Plant:

CCSI

Gianera Generating Station

Location:

Gas Turbine Outlet

	System Calib	ration Ch	eck Data (con	tinued)		Run Time:	Start	End
Run No.	10 Load	Condition:	100				11:20	11:52
Calibration	Cal	ibration Ga		Analyzer	Response	Response	Difference	
After Run	- Cai	ibration Ga		Value	e, %O ₂	Agreement	(Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%O₂	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
11:58	Zero Gas	0.00	N/A	0.14	0.12		-0.08%	Pass
	High-level	N/A	N/A	N/A		N/A		
12:01	Mid-level	11.99	ALM007829	11.96	11.97		0.04%	Pass
	Predicted value from linear curve, %O ₂					ifference as	% of Span:	N/A

Run No.	11 Load	Condition:	100			Run Time:	12:30	13:02
Calibration	Calibration Gas		s .	Analyzer Response		Response	Difference	
After Run		Galibration Gas			e, %O ₂	Agreement	(Drift)	Drift
Ending	Concentration	Value, .	Cylinder	Before	After	with	After Run,	Check
Time	Level	%O₂	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
13:10	Zero Gas	0.00	N/A	0.12	0.05		-0.28%	Pass
	High-level	N/A	N/A	N/A		N/A		
13:13	Mid-level	11.99	ALM007829	11.97	12.00		0.12%	Pass
	Predicted value from linear curve, %O ₂				C	ifference as	% of Span:	N/A

Run No.	12 Load	Condition:	100			Run Time:	13:36	14:08
Calibration	Cal	Calibration Gas			Response	Response	Difference	
After Run	Campration Gas			Value	e, %O ₂	Agreement	(Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%O₂	ID Number	Run	Run	Curve	% of Span	Result ^b
14:12	Zero Gas	0.00	N/A	0.05	0.11		0.24%	Pass
	High-level	N/A	N/A	N/A		N/A		
14:16	Mid-level	11.99	ALM007829	12.00	11.93		-0.28%	Pass
	Predicted val	ue from line	ear curve, %O₂:	N/A	D	ifference as	% of Span:	N/A

Job No.

101494.1.004.02

Operator: Daniel Neal

Client:

CCSI

Gianera Generating Station

Date:

18-Jul-00

Plant: Location:

Gas Turbine Outlet

Analyzer Type:

Single beam, dual wavelength IR

Analyzer Mfgr.: Servomex

Analyzer Span:

%CO₂ by volume 20

Zero Gas:

Prepurified nitrogen

Model No. 01440CISTD

High-level Gas:

Carbon dioxide in nitrogen

Serial No. 1382

Mid-level Gas:

Carbon dioxide in nitrogen

	System		Run Time:	<u>Start</u>	<u>End</u>			
Run No.	1 Load	Condition:	100				7:00	7:32
Calibration After Run	Cal	ibration Gas	s	. •	Response , %CO₂	Response Agreement	Difference (Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%CO₂	ID Number	Run	Run	Curve	% of Span	Result ^b
5:18	Zero Gas	0.00	N/A	-0.04	-0.03		0.05%	Pass
· 5:38	High-level	9.98	AAL19060	10.35		Pass		
5:35	Mid-level	3.01	AAL19060	3.08	3.06		-0.10%	Pass
	Predicted valu	e from linea	ır curve, %CO₂:	10.30	C	ifference as	% of Span:	0.23%

a. High-level response before run must agree with predicted value on linear curve within 2% of the span value.

Reading	Dowr	nscale Response	, seconds	Upscale	Response, s	econds
1	25			22		
2	24			22		
3	23	Average:	24	21	Average:	22
	System I	Response Time	(slower aver	rage time) =	24	seconds

	System Calib	ration Che	eck Data (cont	inued)		Run Time:	Start	<u>End</u>
Run No.	2 Load	Condition:	condition: 100				8:10	8:42
Calibration After Run	Cal	ibration Ga	s	•	Response e, %CO₂	Response Agreement	Difference (Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%CO₂	ID Number	Run	Run	Curve	% of Span	Result ^b
8:50	Zero Gas	0.00	N/A	-0.03	0.12		0.75%	Pass
	High-level	N/A	N/A	N/A		N/A		
8:56	Mid-level	3.01	AAL19060	3.06	3.06		0.00%	Pass
<u> </u>	Predicted value from linear curve, %CO2:					Difference as	% of Span:	N/A

Run No.	3 Load	Condition:	100			Run Time:	9:20	9:52
Calibration After Run	Cal	ibration Ga	s	_	Response , %CO₂	Response Agreement	Difference (Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%CO₂	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
9:56	Zero Gas	0.00	N/A	0.12	0.16		0.20%	Pass
	High-level	N/A	N/A	N/A		N/A		
10:03	Mid-level	3.01	AAL19060	3.06	3.07		0.05%	Pass
	Predicted value from linear curve, %CO ₂					ifference as	% of Span:	N/A

b. Drift check must not exceed ±2% of the span value.

Job No.

101494.1.004.02

Date:

Operator: Daniel Neal

18-Jul-00

Client:

CCSI

Plant:

Gianera Generating Station

Location:

Gas Turbine Outlet

Analyzer Type:

Single beam, dual wavelength IR

Analyzer Mfgr.: Servomex

Analyzer Span:

20 %CO₂ by volume

Zero Gas:

Prepurified nitrogen

Model No. 01440CISTD Serial No. 1382

High-level Gas:

Carbon dioxide in nitrogen

Mid-level Gas:

Carbon dioxide in nitrogen

System	Calibration	Check Data
System	Cambration	Check Data

	System	Calibration	on Check Data	1		Run Time:	Start	<u>End</u>
Run No.	4 Load	Condition:	100				16:40	17:12
Calibration After Run	Cal	ibration Gas	S	-	Response , %CO₂	Response Agreement		Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%CO₂	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
15:20	Zero Gas	0.00	N/A	0.12	0.07		-0.25%	Pass
15:38	High-level	9.98	AAL19060	9.59		Pass		
15:35	Mid-level	3.01	AAL19060	2.95	3.17		1.10%	Pass
	Predicted valu	D	ifference as	% of Span:	0.43%			

a. High-level response before run must agree with predicted value on linear curve within 2% of the span value.

Reading	Dow	nscale Response	e, seconds	Upscale	Response, s	seconds
1	N/A			N/A		
2	N/A			N/A		
3	N/A	Average:	N/A	N/A	Average:	N/A
	System	Response Time	(slower ave	rage time) =	N/A	seconds

	System Calib	ration Che	eck Data (cont	tinued)		Run Time:	<u>Start</u>	<u>End</u>
Run No.	5 Load	Condition:	100				17:50	18:22
Calibration	Cal	ibration Ga		Analyzer	Response	Response	Difference	
After Run	- Cui		•	Value	, %CO₂	Agreement	(Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%CO₂	ID Number	Run	Run	Curve	% of Span	Result ^b
18:28	Zero Gas	0.00	N/A	0.07	-0.02		-0.45%	Pass
1	High-level	N/A	N/A	N/A		N/A		
18:37	Mid-level	3.01	AAL19060	3.17	2.98		-0.95%	Pass
	Predicted value from linear curve, %CO ₂ :				C	ifference as	% of Span:	N/A

Run No.	6 Load	Condition:	100		-	Run Time:	18:58	19:30
Calibration After Run	Cal	s	Analyzer Response Value, %CO ₂		Response Agreement	Difference (Drift)	Drift	
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%CO₂	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
19:35	Zero Gas	0.00	N/A	-0.02	0.07		0.45%	Pass
	High-level	N/A	N/A	N/A		N/A		
19:42	Mid-level	3.01	AAL19060	2.98	2.93		-0.25%	Pass
Predicted value from linear curve,			r curve, %CO ₂ :	N/A	D	ifference as	% of Span:	N/A

b. Drift check must not exceed ±2% of the span value.

Job No.

101494.1.004.02

Date:

Operator: Daniel Neal 19-Jui-00

Client: Plant:

CCSI

Gianera Generating Station

Location:

Gas Turbine Outlet

Analyzer Type:

Single beam, dual wavelength IR

Analyzer Mfgr.: Servomex

Analyzer Span:

%CO₂ by volume

Model No. 01440CISTD

Zero Gas:

Prepurified nitrogen

Serial No. <u>1382</u>

High-level Gas:

Carbon dioxide in nitrogen

Mid-level Gas:

Carbon dioxide in nitrogen

	System	Calibration	on Check Data	1		Run Time:	<u>Start</u>	<u>End</u>
Run No.	Run No. 7 Load Condition: 10						6:40	7:12
Calibration Calibration Gas				-	Response %CO₂	Response Agreement	i	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%CO₂	ID Number	Run	Run	Curve ^a	% of Span	· Result ^b
5:35	Zero Gas	0.00	N/A	0.16	0.07		-0.45%	Pass
5:47	High-level	9.98	AAL19060	9.21		Pass		
5:44	Mid-level	3.01	AAL19060	2.90	3.06		0.80%	Pass
	Predicted value from linear curve, %CO ₂ :					ifference as	% of Span:	-0.17%

a. High-level response before run must agree with predicted value on linear curve within 2% of the span value.

Reading	Dowr	nscale Response	, seconds	Upscale	Response, s	econds
1	N/A			N/A		
2	N/A			N/A		
3	N/A	Average:	N/A	N/A	Average:	N/A
	System I	Response Time	(slower ave	rage time) =	N/A	seconds

	System Calib	ration Che	ck Data (cont	inued)		Run Time:	<u>Start</u>	<u>End</u>
Run No.	Run No. 8 Load Condition:						7:45	8:17
Calibration	Calibration Calibration Gas				Response	Response	Difference	
After Run	Çai	Value	, %CO₂	Agreement	(Drift)	Drift		
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%CO₂	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
8:21	Zero Gas	0.00	N/A	0.07	0.04		-0.15%	Pass
	High-level	N/A	N/A	N/A		N/A		
8:28	Mid-level	3.01	AAL19060	3.06	3.05		-0.05%	Pass
	Predicted value from linear curve, %CO ₂ :				0	ifference as	% of Span:	N/A

Run No.	9 Load	Run No. 9 Load Condition:				Run Time:	8:50	9:22
Calibration After Run	Calibration Gas			•	Response , %CO₂	Response Agreement		Drift
Ending	Concentration	oncentration Value, Cylinder			After	with	After Run,	Check
Time	Level	%CO₂	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
9:30	Zero Gas	0.00	N/A	0.04	0.01		-0.15%	Pass
	High-level	N/A	N/A	N/A		N/A		
9:39	Mid-level	, 3.01	AAL19060	3.05	3.07		0.10%	Pass
	Predicted value from linear curve, %CO ₂ :					ifference as	% of Span:	N/A

b. Drift check must not exceed ±2% of the span value.

Job No.

101494.1.004.02

Date:

Operator: Daniel Neal

Client:

CCSI

19-Jul-00

Plant:

Gianera Generating Station

Location:

Gas Turbine Outlet

	System Calib		Run Time:	Start	End			
Run No.	10 Load	100				11:20	11:52	
Calibration After Run Calibration Gas					Response , %CO₂	Response Agreement	Difference (Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run.	Check
Time	Level	%CO₂	ID Number	Run	Run	Curve	% of Span	Result ^b
11:58	Zero Gas	0.00	N/A	0.01	0.01		0.00%	Pass
	High-level	N/A	N/A	N/A		N/A		
12:04	Mid-level	3.01	AAL19060	3.07	3.06		-0.05%	Pass
	Predicted value	N/A	D	ifference as	% of Span:	N/A		

Run No.	11 Load	Condition:	100			Run Time:	12:30	13:02
Calibration After Run	Calibration Gas			Analyzer Response Value, %CO₂		Response Agreement	Difference (Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%CO₂	ID Number	Run	Run	Curvea	% of Span	Result ^b
13:10	Zero Gas	0.00	N/A	0.01	0.25		1.20%	Pass
	High-level	N/A	N/A	N/A		N/A		
13:16	Mid-level	3.01	AAL19060	3.06	2.82		-1.20%	Pass
	Predicted value from linear curve, %CO2:					ifference as	% of Span:	N/A

Run No.	12 Load	Condition:	100			Run Time:	13:36	14:08
Calibration After Run	Calibration Gas			Analyzer Response Value, %CO₂		Response Agreement	Difference (Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After Run,	Check
Time	Level	%CO₂	ID Number	Run	Run	Curve ^a	% of Span	Result ^b
14:12	Zero Gas	0.00	N/A	0.25	0.21		-0.20%	Pass
	High-level	N/A	N/A	N/A		N/A		
14:19	Mid-level	3.01	AAL19060	2.82	2.83		0.05%	Pass
	Predicted valu	e from linea	r curve, %CO₂:	N/A	D	ifference as	% of Span:	N/A

 Job No.
 101494.1.004.02
 Operator:
 Daniel Neal

 Client:
 CCSI
 Date:
 18-Jul-00

 Plant:
 Gianera Generating Station
 18-Jul-00
 18-Jul-00

Location: Gas Turbine Outlet

Analyzer Type: Flame ionization using an FID Manufacturer: J.U.M. Engineering

Analyzer Span: 100 ppmv Propane Model No. VE 7

Zero Gas: Prepurified nitrogen Serial No. 102011192

Cal. Gas Mixture: Propane in nitrogen

Mea	surement Syst	Sampling	Start	<u>End</u>			
Run No. 1 Load Condition: 100				Time:	7:00	7:32	
Calibration	Ca	libration Ga	S	System Response	Predicted	Response	Cal. Error
Ending	Concentration	Value,	Cylinder	Value Following	Value,	Difference,	Check
Time	Level	ppmv	ID Number	Calibration, ppmv	ppmv	% of PV	Result ^a
6:32	Zero Gas	0.00	N/A	-0.02			
6:38	High-level	84.90	ALM023230	85.07			
6:41	Mid-level	49.90	ALM023230	49.99	49.99	0.00%	Pass
6:44	Low-level	29.90	ALM023230	29.89	29.95	-0.19%	Pass

a. The difference between the analyzer response and the predicted value on the linear curve must be less than ±5% of the predicted value (PV).

Response Time Determination

Reading	Upscale Response, seconds
1	17
2	21
3	19

System Response Time (average) = 19 seconds

Measurement System Drift

Calibration Ending	Calibration Gas Concentration	•	Response, pmv	Difference (Drift),	System Drift,	Drift Check
Time	Level	Before	After	ppmv	% of Span	Result ^b
7:58	Zero Gas	-0.02	-0.06	-0.04	-0.04%	Pass
8:01	Mid-level	49.99	49.90	-0.09	-0.09%	Pass

b. Drift must be less than ±3% of the span value.

Drift = Final System Cal. Response - Initial System Cal. Response x 100

Mea	surement Syst	Sampling	Start	<u>End</u>			
Run No.	Run No. 2 Load Condition: 100						8:42
Calibration Gas System Response					Predicted	Response	Cal. Error
Ending	Concentration	Value,	Cylinder	Value Following	Value,	Difference,	Check
Time	Level	ppmv	ID Number	Calibration, ppmv	ppmv	% of PV	Result
	Zero Gas	0.00	N/A	N/A	l		
	High-level	N/A	N/A	N/A			
	Mid-level	49.90	ALM023230	N/A	N/A	N/A	N/A
	Low-level	N/A	N/A	N/A	N/A	N/A	N/A

Calibration Ending	Calibration Gas Concentration		Response, pmv	Difference (Drift),	System Drift,	Drift Check
Time	Level	Before	After	ppmv	% of Span	Result
9:10	Zero Gas	-0.06	-0.07	-0.01	-0.01%	Pass
9:17	Mid-level	49.90	49.49	-0.41	-0.41%	Pass

Job No. 101494.1.004.02 Operator: Daniel Neal

Date:

18-Jul-00

Client:

CCSI

Gianera Generating Station

Plant:

Location: Gas Turbine Outlet

Mea	Measurement System Calibration Error Determination						End
Run No.	3 Load (Condition:	100		Time:	9:20	9:52
Calibration	Ca	libration Ga	S	System Response	Predicted	Response	Cal. Error
Ending	Concentration	Value,	Cylinder	Value Following	Value,	Difference,	Check
Time	Level	ppmv	ID Number	Calibration, ppmv	ppmv	% of PV	Result
	Zero Gas	N/A	N/A	N/A			
i i	High-level	N/A	N/A	N/A			
	Mid-level	49.90	ALM023230	N/A	N/A	N/A	N/A
	Low-level	N/A	N/A	N/A	N/A	N/A	N/A

Calibration · Ending	Calibration Gas Concentration	•	Response, pmv	Difference (Drift),	System Drift,	Drift Check
Time	Level	Before	After	ppmv	% of Span	Result
10:16	Zero Gas	-0.07	0.02	0.09	0.09%	Pass
10:18	Mid-level	49.49	49.48	-0.01	-0.01%	Pass

Job No.

101494.1.004.02

Operator: Daniel Neal

Date:

Client:

CCSI

Location: Gas Turbine Outlet

18-Jul-00

Plant:

Gianera Generating Station

Analyzer Type:

Flame ionization using an FID

Manufacturer: J.U.M. Engineering

Analyzer Span:

100 ppmv Propane

Model No. VE 7

Zero Gas:

Prepurified nitrogen

Serial No. 102011192

Cal. Gas Mixture: Propane in nitrogen

Mea	Measurement System Calibration Error Determination						<u>End</u>
Run No.	4 Load (Condition:	100		Time:	16:40	17:12
Calibration	Cal	ibration Ga	S	System Response	Predicted	Response	Cal. Error
Ending	Concentration	Value,	Cylinder	Value Following	Value,	Difference,	Check
Time	Level	ppmv	ID Number	Calibration, ppmv	ppmv	% of PV	Result ^a
16:13	Zero Gas	0.00	N/A	0.07			
· 16:17	High-level	84.98	ALM023230	85.47			
16:20	Mid-level	49.90	ALM023230	50.12	50.22	-0.19%	Pass
16:24	Low-level	29.90	ALM023230	30.00	30.12	-0.39%	Pass

a. The difference between the analyzer response and the predicted value on the linear curve must be less than ±5% of the predicted value (PV).

Response Time Determination

Reading	Upscale Response, seconds
1	N/A
2	N/A
3	N/A

System Response Time (average) =

seconds

N/A

Measurement System Drift

Calibration Ending	Calibration Gas Concentration		Response, pmv	Difference (Drift),	System Drift,	Drift Check
Time	Level	Before	After	ppmv	% of Span	Result⁵
17:40	Zero Gas	0.07	-0.06	-0.13	-0.13%	Pass
17:43	Mid-level	50.12	49.79	-0.33	-0.33%	Pass

b. Drift must be less than ±3% of the span value.

Final System Cal. Response - Initial System Cal. Response Span

Mea	Measurement System Calibration Error Determination						<u>End</u>
	Run No. 5 Load Condition: 100					17:50	18:22
Calibration		ibration Ga	s	System Response	Predicted	Response	Cal. Error
Ending	Concentration	Value,	Cylinder	Value Following	Value,	Difference,	Check
Time	Level	ppmv	ID Number	Calibration, ppmv	ppmv	% of PV	Result
	Zero Gas	N/A	N/A	N/A			
1	High-level	N/A	N/A	N/A			
	Mid-level	49.90	ALM023230	N/A	N/A	N/A	N/A
	Low-level	N/A	N/A	N/A	N/A	N/A	N/A

Calibration Ending	Calibration Gas Concentration		Response, pmv	Difference (Drift),	System Drift,	Drift Check
Time	Level	Before	After	ppmv	% of Span	Result
18:51	Zero Gas	-0.06	0.01	0.07	0.07%	Pass
18:54	Mid-level	49.79	50.15	0.36	0.36%	Pass

Job No.

101494.1.004.02

Operator: Daniel Neal

Client:

CCSI

Date:

18-Jul-00

Plant:

Gianera Generating Station

Location:

Gas Turbine Outlet

Mea	Measurement System Calibration Error Determination						End
Run No.	6 Load	Condition:	100		Time:	18:58	19:30
Calibration	Ca	libration Ga	S	System Response	Predicted	Response	Cal. Error
Ending	Concentration	Value,	Cylinder	Value Following	Value,	Difference,	Check
Time	Level	ppmv	ID Number	Calibration, ppmv	ppmv	% of PV	Result
	Zero Gas	N/A	N/A	N/A			
	High-level	N/A	N/A	N/A			
	Mid-level	49.90	ALM023230	N/A	N/A	N/A	N/A
	Low-level	N/A	N/A	N/A	N/A	N/A	N/A

Calibration	Calibration Gas	System	Response,	Difference	System	Drift
Ending	Concentration		pmv	(Drift),	Drift,	Check
Time	Level	Before	After	ppmv	% of Span	Result
19:56	Zero Gas	0.01	-0.09	-0.10	-0.10%	Pass
20:00	Mid-level	50.15	49.95	-0.20	-0.20%	Pass

Job No.

101494.1.004.02

Operator: Daniel Neal

Date:

Client:

CCSI

Plant: **Gianera Generating Station** Location: Gas Turbine Outlet

Analyzer Type:

Flame ionization using an FID

Manufacturer: J.U.M. Engineering

19-Jul-00

seconds

Analyzer Span:

100 ppmv Propane

Model No. VE 7

Zero Gas:

Prepurified nitrogen

Serial No. 102011192

Cal. Gas Mixture: Propane in nitrogen

Mea	Measurement System Calibration Error Determination						<u>End</u>
Run No.	7 Load (Condition:	100		Time:	6:40	7:12
Calibration	Cal	ibration Ga	S	System Response	Predicted	Response	Cal. Error
Ending	Concentration	Value,	Cylinder	Value Following	Value,	Difference,	Check
Time	Level	ppmv	ID Number	Calibration, ppmv	ppmv	% of PV	Result ^a
6:13	Zero Gas	0.00	N/A	0.02			
6:19	High-level	84.96	ALM023230	85.04			
6:22	Mid-level	49.94	ALM023230	49.95	50.00	-0.09%	Pass
6:25	Low-level	29.92	ALM023230	30.00	29.96	0.13%	Pass

a. The difference between the analyzer response and the predicted value on the linear curve must be less than ±5% of the predicted value (PV).

Response Time Determination

Reading	Upscale Response, seconds
1	N/A
2	N/A
3	N/A

System Response Time (average) =

Measurement System Drift

Calibration Ending	Calibration Gas Concentration	•	Response, pmv	Difference (Drift),	System Drift,	Drift Check
Time	Level	Before	After	ppmv	% of Span	Result ^b
7:36	Zero Gas	0.02	-0.07	-0.09	-0.09%	Pass
7:40	Mid-level	49.95	49.63	-0.32	-0.32%	Pass

b. Drift must be less than ±3% of the span value.

Final System Cal. Response - Initial System Cal. Response Span

Mea	surement Syst	tem Calib	ration Error D	etermination	Sampling	Start	<u>End</u>
Run No.	8 Load (Condition:	100		Time:	7:45	8:17
Calibration	Cal	ibration Ga	s	System Response	Predicted	Response	Cal. Error
Ending	Concentration	Value,	Cylinder	Value Following	Value,	Difference,	Check
Time	Level	ppmv	ID Number	Calibration, ppmv	ppmv	% of PV	Result
	Zero Gas	N/A	N/A	N/A			
1	High-level	N/A	N/A	N/A			
1	Mid-level	49.94	ALM023230	N/A	N/A	N/A	N/A
	Low-level	N/A	N/A	N/A	N/A	N/A	N/A

Calibration Ending	Calibration Gas Concentration	System Response, ppmv		Difference (Drift),	System Drift,	Drift Check
Time	Level	Before	After	ppmv	% of Span	Result
8:40	Zero Gas	-0.07	0.01	0.08	0.08%	Pass
8:44	Mid-level	49.63	49.27	-0.36	-0.36%	Pass

Job No.

101494.1.004.02

Low-level

Date:

Operator: Daniel Neal

N/A

N/A

19-Jul-00

N/A

Client: Plant:

CCSI

Gianera Generating Station

Location:

Gas Turbine Outlet

N/A

Mea	surement Syst	tem Calib	ration Error D	etermination	Sampling	Start	End
Run No. 9 Load Condition: 100					Time:	8:50	9:22
Calibration	Cal	ibration Ga	S	System Response	Predicted	Response	Cal. Error
Ending	Concentration	Value,	Cylinder	Value Following	Value,	Difference,	Check
Time	Level	ppmv	ID Number	Calibration, ppmv	ppmv	% of PV	Result
	Zero Gas	N/A	N/A	N/A			
1	High-level	N/A	N/A	N/A			
	. Mid-level	49.94	ALM023230	N/A	N/A	N/A	N/A

Measurement System Drift

N/A

N/A

Calibration Ending	Calibration Gas Concentration		Response, pmv	Difference (Drift),	System Drift,	Drift Check
Time	Level	Before	After	ppmv	% of Span	Result
9:54	Zero Gas	0.01	0.33	0.32	0.32%	Pass
9:58	Mid-level	49.27	49.07	-0.20	-0.20%	Pass

Mea	surement Syst	tem Calibi	ration Error D	etermination	Sampling	Start	End
Run No.	10 Load	Condition:	100		Time:	11:20	11:52
Calibration	Ca	libration Ga	s ·	System Response	Predicted	Response	Cal. Error
Ending	Concentration	Value,	Cylinder	Value Following	Value,	Difference,	Check
Time	Level	ppmv	ID Number	Calibration, ppmv	ppmv	% of PV	Result
	Zero Gas	N/A	N/A	N/A			
	High-level	N/A	N/A	N/A			
	Mid-level	49.94	ALM023230	N/A	N/A	N/A	N/A
1	Low-level	N/A	N/A	N/A	N/A	N/A	N/A

Measurement System Drift

Calibration	Calibration Gas	System Response,		Difference	System	Drift
Ending	Concentration		pmv	(Drift),	Drift,	Check
Time	Level	Before	After	ppmv	% of Span	Result
12:19	Zero Gas	0.33	0.07	-0.26	-0.26%	Pass
12:25	Mid-level	49.07	49.00	-0.07	-0.07%	Pass

Mea	surement Syst	tem Calibi	ration Error D	etermination	Sampling	<u>Start</u>	<u>End</u>
Run No.	11 Load	Condition:	100		Time:	12:30	13:02
Calibration	Ca	ibration Ga	S	System Response	Predicted	Response	Cal. Error
Ending	Concentration	Value,	Cylinder	Value Following	Value,	Difference,	Check
Time	Level	ppmv	ID Number	Calibration, ppmv	ppmv	% of PV	Result
	Zero Gas	N/A	N/A	N/A			
	High-level	N/A	N/A	N/A			
1	Mid-level	49.94	ALM023230	N/A	N/A	N/A	N/A
1	Low-level	N/A	N/A	N/A	N/A	N/A	N/A

Calibration Ending	Calibration Gas Concentration		Response,	Difference (Drift),	System Drift.	Drift Check
Time	Level	Before	After	ppmv	% of Span	Result
13:28	Zero Gas	0.07	0.05	-0.02	-0.02%	Pass
13:32	Mid-level	49.00	48.58	-0.42	-0.42%	Pass

 Job No.
 101494.1.004.02
 Operator:
 Daniel Neal

 Client:
 CCSI
 Date:
 19-Jul-00

 Plant:
 Gianera Generating Station

Location: Gas Turbine Outlet

Mea	asurement Syst	tem Calib	ration Error D	etermination	Sampling	Start	End
Run No.	12 Load	Condition:	100		Time:	13:36	14:08
Calibration	Cal	libration Ga	s	System Response	Predicted	Response	Cal. Error
Ending	Concentration	Value,	Cylinder	Value Following	Value,	Difference,	Check
Time	Level	ppmv	ID Number	Calibration, ppmv	ppmv	% of PV	Result
	Zero Gas	N/A	N/A	N/A			
	High-level	N/A	N/A	N/A			
	Mid-level	49.94	ALM023230	N/A	N/A	N/A	N/A
	Low-level	N/A	N/A	N/A	N/A	N/A	N/A

Calibration	Calibration Gas	System Response,		Difference	System	Drift	
Ending	Concentration	р	pmv	(Drift),	Drift,	Check	
Time	Level	Before	After	ppmv	% of Span	Result	
14:34	Zero Gas	0.05	0.02	-0.03	-0.03%	Pass	1
14:40	Mid-level	48.58	48.78	0.20	0.20%	Pass	.

A.2 Reference Method Performance Audit Results

NO_X Analyzer NO₂ To NO Converter Efficiency Check By Method 20

Operator: Daniel Neal Job No. 101494.1.004.02 Client: CCSI Date: 17-Jul-00 Plant: **Cianera Generating Station** Analyzer Mfgr.: Thermo Environmental Instr. Analyzer Type: Chemiluminescent Model No. 42H ppmv NO_X Analyzer Span: Serial No. 42H-41111-264 Zero Gas: Prepurified nitrogen

High-level Gas:

Mid-level Gas:

Nitrogen oxide in nitrogen

Nitrogen oxide in nitrogen

Low-level Gas: Nitrogen oxide in nitrogen

System Calibration Check Data

Calibration	Calib	Calibration Gas				Response	Difference	
After CEC	Calit	nation Gas		Value, ppmv NO _x		Agreement	(Drift)	Drift
Ending	Concentration	Value,	Cylinder	Before	After	with	After CEC,	Check
Time	Level	ppmv NO _x	ID Number	CEC.	CEC	Curve	% of Span	Result ^b
13:04	Zero Gas	0.00	N/A	-0.05	-0.05		0.00%	Pass
12:11	High-level	18.05	ALM048090	18.18		Pass		
13:08	Mid-level	10.03	ALM048090	10.19	9.87		-1.60%	Pass
12:15	Low-level	5.02	ALM048090	4.88		Pass		
	Predicted value fro		Difference as % of Span					
H	ligh-level: 18.38	Low-level:	5.08		High-level:	-0.99%	Low-level:	-0.99%

a. High-level response before run must agree with predicted value on linear curve within 2% of the span value.

Response Time Determination

Reading	Dowi	nscale Response,	seconds	Upscale	e Response, s	
1	N/A			N/A		
2	N/A			N/A		
3	N/A	Average:	N/A	N/A	Average:	N/A
	System	Response Time	(slower ave	rage time) =	N/A	seconds

Analyzer Converter Efficiency Determination

	Mid-level N0 in $ m N_2$ calibration gas diluted approximately 1:1 with ambient air.									
	Conversion Efficiency Check (1 min Average Readings)									
Time	Minutes	NO _X	Time	Minutes	NO _X	Time	Minutes	NOx		
24-Hr	Elapsed	Reading	24-Hr	Elapsed	Reading	24-Hr	Elapsed	Reading		
12:29	1	4.98	12:39	11	5.01	12:49	21	5.02		
12:30	2	4.97	12:40	12	5.01	12:50	22	5.01		
12:31	3	4.98	12:41	13	5.00	12:51	23	5.01		
12:32	4	4.97	12:42	14	5.00	12:52	24	5.01		
12:33	5	4.98	12:43	15	5.01	12:53	25	5.01		
12:34	6	4.98	12:44	16	5.02	12:54	26	5.01		
12:35	7	4.99	12:45	17	5.01	12:55	27	5.01		
12:36	8	5.00	12:46	18	5.00	12:56	28	5.01		
12:37	9	5.01	12:47	19	5.01	12:57	29	5.01		
12:38	10	5.01	12:48	20	5.01	12:58	30	5.01		
								·····		
Highes	st Reading:	5.02	ppmv							
	Efficiency:	99.8%	Per	cent decrease:	0.2%		Result:	Pass		

^{*} If the response at the end of 30 minutes decreases more than 2.0 percent of the highest peak value, the system is not acceptable.

b. Drift check must not exceed ±2% of the span value.

NO2 Converter Check Run 1 Time is 11:44:48.73. Date is 7-17-2000 NOx Time ppm 11:44 0.13 11:45 0.08 11:46 0.03 0.02 11:47 11:48 0 11:49 2.1 11:50 10.19 11:51 10.22 11:52 10.28 11:53 10.26 11:54 10.73 1.24 11:55 11:56 -0.03 11:57 -0.04 -0.05 11:58 -0.05 11:59 12:00 -0.05 4.61 12:01 12:02 10.11 12:03 10.19 12:04 10.2 12:05 10.2 9.86 12:06 12:07 9.98 12:08 9.98 12:09 15.67 12:10 18.19 12:11 18.18 11.18 12:12 12:13 4.95 12:14 4.89 12:15 4.88 1.93 12:16 -0.03 12:17 -0.05 12:18 12:19 -0.05 12:20 -0.06 12:21 -0.05 12:22 -0.05 12:23 -0.05 12:24 -0.05 12:25 -0.05 12:26 -0.0512:27 0.18 12:28 5.75 12:29 4.98

12:30	4.97
12:31	4.98
12:32	4.97
12:33	4.98
12:34	4.98
12:35	4.99
12:36	5
12:37	5.01
12:38	5.01
12:39	5.01
12:40	5.01
12:41	5
12:42	5
12:43	5.01
12:44	5.02
12:45	5.01
12:46	5
12:47	5.01
12:48	5.01
12:49	5.02
12:50	5.01
12:51	5.01
12:52	5.01
12:53	5.01
12:54	5.01
12:55	5.01
12:56	5.01
12:57	5.01
12:58	5.0 1
12:59	4.78
13:00	0.45
13:01	-0.02
13:02	-0.03
13:03	-0.05
13:04	-0.05
13:05	6.46
13:06	9.75
13:07	9.9
13:08	9.87
13:09	9.85

Test Events Log Method 205

Jo	b No.	101494.1.004.02	perator:	Daniel Neal		
Cli	ient:	CCSI	Date:	17-Jul-00		-
Pla	ant:	Gianera Generating Station				
Lo	cation:	Gas Turbine Outlet				
		Method 205 test - MFC's 1& 2				
	19:30	Adjusted Photo Multiplier Tube to correct non-linearity of	he analy	zer, as per o	perators	manual
	19:34	Start zero cal for NO channel		•		
	19:37	Start high-range cal for NO channel				
	19:42	Start zero cal for NOx channel				
	19:45	Record zero cal				
	19:45	Start high-range cal for NOx channel				
	19:54	Record high-range cal and 1st upper point reading,				
		switch from auto mode for cals to manual mod	le.			
	19:54	Start mid-range cal for NOx channel				
	19:57	Record mid-range cal for NOx channel and 1st lower point	t reading			
	19:57	1st mid-range gas standard injection				
	20:02	1st mid-range gas standard reading				•
	20:02	2nd lower point injection				
	20:05	2nd lower point reading				
	20:05	2nd upper point injection				
	20:08	2nd upper point reading				
	20:08	2nd mid-range gas standard injection				
	20:11	2nd mid-range gas standard reading				
	20:11	3rd lower point injection				
	20:14	3rd lower point reading				
	20:14	3rd upper point injection				
	20:18	3rd upper point reading				
	20:18	3rd mid-range gas standard injection				
	20:22	3rd mid-range gas standard reading				
	20:22	Start zero drift check injection				
	20:26	Record zero drift check reading Start mid-range drift check injection				
	20:26	Record mid-range drift check reading				
	20:30	Record mid-range drift check reading				
		Method 205 test - MFC's 1& 3				
	20:36	1st lower point injection				
	20:40	1st lower point reading				
	20:40	1st upper point injection				
	20:44	1st upper point reading				
	20:44	1st mid-range gas standard injection				
	20:48	1st mid-range gas standard reading				
	20:48	2nd lower point injection				
	20:52	2nd lower point reading				
	20:52	2nd upper point injection				
	20:56	2nd upper point reading				
	20:56	2nd mid-range gas standard injection				
	21:00	2nd mid-range gas standard reading				
	21:00	3rd lower point injection				
	21:04	3rd lower point reading				
	21:04	3rd upper point injection				
	21:08	3rd upper point reading				

ETV RTI Method 205.xls 7/26/00 1:01 PM

21:08	3rd mid-range gas standard injection
21:12	3rd mid-range gas standard reading
21:12	Start zero drift check injection
21:16	Record zero drift check reading
21:16	Start mid-range drift check injection
21:20	Record mid-range drift check reading

Method 205 Summary Data

Varification Of Mass Flow Controllers 1 and 2

Client:

CCSI

Job No.

101494.1.004.02

Plant:

Gianera Generating Station

Operator:

Daniel Neal

Location: Gas Turbine Outlet

Date:

17-Jul-00

Reference Method Analyzer

(Used During This Test)

Manufacturer: Thermo Environmental Instr.

Model No. 42H

Analyzer Type: Chemiluminescent

Analyzer Range: 0-50 ppm

Serial No. 42H-41111-264

Cal. No. NOX-1

Calibration Gas Dilution Instrument

Manufacturer: Environics, Inc.

Model No. S-2020-R

Serial No. 2073

Last Calibrated: 11-Jul-00

EPA Protocol 1 Traceable Gases

High-Level (Dilution) Gas Standard Concentration:

201.85 ppm

Cylinder I.D. Number: ALM048090

Mid-Level Gas Standard Concentration:

Cylinder I.D. Number: AAL7388

	Dilution In	Dilution Instrument		Analyzer Reading			MFC
High-Level (Dilution)	MFC Output			Corrected		Run vs	Output vs
Gas Standard	Concer	Concentration		for Cal.		Average	Average
Calibration Points	Run	Value	Per Run	Results	Average	(% Error)	(% Error)
	1	24.90	24.57	24.60		-0.18%	
Lower Point Injections	2	24.90	24.67	24.70	24.64	0.23%	1.03%
·	3	24.90	24.60	24.63		-0.05%	
	1	44.90	44.97	45.07		-0.03%	
Upper Point Injections	2	44.90	45.03	45.13	45.08	0.10%	-0.40%
	3	44.90	44.95	45.05		-0.07%	

Mid-Level			Ai	nalyzer Readi	Mid-Level	
Mid-Level Gas	Gas Standard Concentration			Corrected		Gas Standard
Standard Calibration			As Read	for Cal.		vs Average
Points	Run	Value	Per Run	Results	Average	(% Error)
	1	25.59	25.49	25.52		
Mid-Level Injections	2	25.59	25.41	25.44	25.46	0.52%
ma zevel injections	3	25.59	25.37	25.40		

All dilution points must be within ± 2% of analyzer reading

STATUS OF TEST:

PASSED

Method 205 Summary Data

Varification Of Mass Flow Controllers 1 and 3

Client: Plant:

CCSI

Gianera Generating Station

Location: Gas Turbine Outlet

Job No.

101494.1.004.02

Operator:

Daniel Neal

Date:

17-Jul-00

Reference Method Analyzer

(Used During This Test)

Manufacturer: Thermo Environmental Instr

Model No. 42H

Analyzer Type: Chemiluminescent

Analyzer Range: 0-50 ppm

Serial No. 42H-41111-264

Cal. No. NOX-2

Calibration Dilution Instrument

Manufacturer: Environics, Inc.

Model No. S-2020-R

Serial No. 2073

Last Calibrated: 11-Jul-00

EPA Protocol 1 Traceable Gases

High-Level (Dilution) Gas Standard Concentration:

503.45 ppm

Cylinder I.D. Number: ALM055608

Mid-Level Gas Standard Concentration:

25.59 ppm

Cylinder I.D. Number: AAL7388

	Dilution In	Dilution Instrument		nalyzer Readi		MFC	
High-Level (Dilution) Gas Standard		Output ntration	As Read	Corrected for Cal.		Run vs Average	Output vs Average
Calibration Points	Run	Value	Per Run	Results	Average	(% Error)	(% Error)
	1	25.07	24.51	24.68		0.16%	
Lower Point Injections	2	25.07	24.44	24.61	24.64	-0.12%	1.73%
201101111111111111111111111111111111111	3	25.07	24.46	24.63		-0.04%	
	1	45.10	44.61	44.95		0.18%	
Upper Point Injections	2	45.10	44.51	44.85	44.87	-0.04%	0.51%
	3	45.10	44.47	44.81		-0.13%	

	Mid-Level			nalyzer Readi	Mid-Level	
Mid-Level Gas	Gas Standard			Corrected		Gas Standard
Standard Calibration	Concentration		As Read	for Cal.		vs Average
Points	Run	Value	Per Run	Results	Averag e	(% Error)
	. 1	25.59	25.17	25.34		
Mid-Level Injections	2	25.59°	25.15	25.32	25.29	1.18%
	3	25.59	25.03	25.20		

All dilution points must be within ± 2% of analyzer reading

STATUS OF TEST:

PASSED

M-205 Field Test Run 1 Time is 17:27:52.44. Date is 7-17-2000. NOx Time ppm 17:27 1.05 17:28 0.29 17:29 -0.01 17:30 -0.01 17:31 -0.01 17:32 -0.01 17:33 -0.01 17:34 -0.03 17:35 6.59 17:36 44.37 17:37 46.7 17:38 46.93 17:39 47.03 17:40 47.09 17:41 42.44 17:42 0.68 17:43 3.23 17:44 44.49 17:45 45.54 17:46 45.52 17:47 42.33 17:48 1.09 17:49 -0.01 17:50 -0.03 17:51 -0.07 17:52 -0.07 17:53 -0.07 17:54 0.09 17:55 -0.15 17:56 -0.17 17:57 7.01 17:58 43.92 17:59 45.2 18:00 45.18 18:01 45.17 18:02 45.17 18:03 45.02 18:04 44.65 18:05 44.8 18:06 44.95 18:07 44.96 18:08 44.97 18:09 28.77 18:10 25.3 18:11 26.96 18:12 24.47 36.13 18:13 22.52 18:14 18:15 30.16 18:16 27.85 18:17 24.5 18:18 29.8 18:19 44.94 18:20 45 18:21 45 18:22 45

18:23

18:24

32.89

24.47

40.05	04.40
18:25	24.49
18:26	24.35
18:27	3.23
18:28	0.56
18:29	0.04
10.00	0.03
18:30	0.03
18:31	-0.06
10.51	
18:32	-0.05
18:33	0.01
18:34	12.9
18:35	46.7
18:36	47.28
10.07	
18:37	45.46
18:38	46.61
18:39	44.51
18:40	9.71
18:41	0.04
18:42	-0.03
	_
18:43	0
18:44	12.89
18:45	44.78
18:46	45.07
18:47	44.84
18:48	44.88
18:49	44.86
18:50	44.33
	25.95
18:51	25.95
18:52	24.49
18:53	24.51
10.54	04.50
18:54	24.52
18:55	30.43
18:56	44.85
10.57	44.02
18:57	44.92
18:58	44.98
18:59	45.19
19:00	45.2
19:01	44.83
19:02	44.71
19:03	28.56
19:04	24.46
19:05	21.79
10.00	14.53
19:06	14.53
19:07	14.74
19:08	28.01
19:09	29.6
19:10	29.86
19:11	43.88
	44.96
19:12	
19:13	44.78
19:14	26.16
19:15	23.95
19:16	25.27
19:17	25.01
19:18	30.81
19:19	45.78
19:20	45.52
	45.3
19:21	
19:22	45.31
19:23	45.94
	42.45
19:24	
19:25	40.23
19:26	40.19
	40.15
19:27	
19:28	40.08
. 0.20	.0.00

19:29 19:30 19:31 19:32 19:33 19:34 19:35 19:36 19:37 19:38 19:39 19:40 19:41 19:42 19:43 19:44 19:45 19:46 19:47 19:48 19:49 19:50 19:51 19:52 19:53 19:54 19:55 19:56 19:57 19:58 19:59 20:00 20:01 20:02 20:03 20:04 20:05 20:06 20:07 20:08 20:09 20:10 20:11 20:12 20:13 20:14 20:15 20:16 20:17 20:18 20:20 20:21 20:22 20:23 20:24 20:25 20:26 20:27 20:28 20:29 20:31 20:32	40.15 39.79 40.14 40.28 40.23 39.72 6.77 0.05 0.06 27.83 45.19 45.25 45.24 45.18 17.77 0.05 0.77 41.38 45.07 45.15 45.19 44.97 24.62 24.57 24.56 24.33 25.36 25.49 24.94 24.67 30 39.25 25.45 25.41 25.37 24.67 24.68 24.75 43.43 44.97 44.95 44.74 27.01 25.38 21.78 0.98 0.05 8.39 24.51 24.51 18.5
---	---

21:14 0.12 21:15 0.04	20:33 20:34 20:35 20:36 20:37 20:38 20:40 20:41 20:42 20:43 20:44 20:45 20:46 20:47 20:48 20:50 20:51 20:52 20:53 20:54 20:55 20:55 20:56 20:57 20:58 20:59 21:00 21:01 21:03 21:04 21:07 21:08 21:10 21:11 21:12 21:13	0.49 5.58 1.67 20.57 23.44 24.22 24.45 24.51 35.44 44.65 44.61 32.34 25.21 25.17 27.97 24.42 24.43 24.44 37.37 44.52 44.51 31.99 25.14 25.15 27.85 24.46 38.45 44.54 44.54 44.54 44.54 44.54 44.54 44.54 52.05 25.05 25.03 24.95
21:12 25.03 21:13 24.95 21:14 0.12 21:15 0.04	21:08 21:09	30.81
£1,10 U.U4	21:11 21:12 21:13 21:14	25.03 24.95 0.12
	21:24 21:25	-0.02 -0.04

NO_X Analyzer Calibration Data By Modified Method 7E

Job No.

101494.1.004.02

Operator: Daniel Neal

Client: Plant:

CCSI

Date:

17-Jul-00

Location:

Gianera Generating Station Gas Turbine Outlet

Analyzer Type:

Chemiluminescent

Analyzer Mfgr.: Thermo Environmental Instr.

Zero Gas:

Prepurified nitrogen

Model No. 42H

Cal. Gas Mixture:

Nitrogen oxide in nitrogen

Serial No. 42H-41111-264

Analyzer Calibration Error Determination

Γ	Cal. No.	NOX-1 Anal	yzer Span:	50	ppmv NO _x			
ſ	Calibration	Calibration Gas		Dration Calibration Gas Analyzer Respo		Analyzer Response	Gas Value - Analyzer	Cal. Error
١	Ending	Concentration	Value,	Cylind er	Value Following	Response Difference	Check	
ı	Time	Level	ppmv NO _x	ID Number	Calibration, ppmv NO _X	As % of Span	Result ^a	
ı	19:45	Zero Gas	0.00	N/A	0.05	0.10%	Pass	
ı	19:54	High-range	44.90	ALM048090	44.97	0.14%	Pass	
1	19:57	Mid-range	24.90	ALM048090	24.57	-0.66%	Pass	

a. Calibration error check must not exceed ±2% of the span value.

Analyzer Drift

Calibration After M205 Injections	Calibration Gas Concentration	Analyzer Re	Drift,	Drift Check	
Ending Time	Level	Before M205 Injections	After M205 Injections	% of Span	Result ^b
20:26	Zero Gas	0.05	0.05	0.00%	Pass
20:30	Mid-range	24.57	24.51	-0.12%	Pass

b. Drift check must not exceed ±3% of the span value.

Analyzer Calibration Error Determination

Cal. No.	NOX-2 Anal	yzer Span:	50	ppmv NO _X		
Calibration	Calibration Gas			Analyzer Response Gas Value - Ana		Cal. Error
Ending	Concentration	Value,	Cylind er	Value Following	Response Difference	Check
Time	Level	ppmv NO _x	ID Number	Calibration, ppmv NO _X	As % of Span	Result
19:45	Zero Gas	0.00	N/A	0.05	0.10%	Pass
19:54	High-range	44.90	ALM048090	44.97	0.14%	Pass
19:57	Mid-range	24.90	ALM048090	24.57	-0.66%	Pass

Analyzer Drift

Allalyzer Dilit							
Calibration After	Calibration Gas	Analyzer Ro	esponse,		Drift		
M205 Injections	Concentration	ppmv	Drift,	Check			
Ending Time	Level	Before M205 Injections	After M205 Injections	% of Span	Result		
21:16	Zero Gas	0.05	0.04	-0.02%	Pass		
21.20	Mid-range	24.57	24.24	-0.66%	Pass		

Project No.: 101494.1.004.02
Date: 7/18/00
Corrective Action Report
Project Title/Description: ETV test of Catalytica Combustion System's XONON Flameless Combustion System
Description of Problem: When attempting to calibrate the Nox analyzer for the Method 205 verification of the dilution system, the Nox analyzer was non-linear.
Originator: <u>Craig Clapsaddle</u> Date: 7/17/00
Investigation and Results: After repeated attempts to make the response linear (by adjusting calibration settings), Dan Neal recalled that TECO told him to adjust the PMT (photo multiplier tube) if the calibration set point adjustments did not fix the problem.
Investigator: <u>Crang Clapsaddle</u> Date: 7/17/00
Corrective Action Taken: Adjustment of the PMT set point was made according to the manufacturer's instructions. The PMT setpoint was off and adjusted. The ins Nox analyzer's response was linear and the Method 205 was successfully completed.
Originator: <u>Croig Clapsaddle</u> Date: 7/17/00 Reviewer: <u>Vinus Nul</u> Date: 7-18-00
Keviewer: () Date.

cc: Project Leader, Program Manager, Division Manager, QA Unit

5/2013

FLOW CONTROLLER CALIBRATION SHEET

Mf #: 1. Description: AIR

, Size: 10000. SCCM, K-factor: 1.0

SERIAL # AW9502156

This flow controller was calibrated using a Sierra Cal Bench(TM), a traceable Primary Flow Standard Calibration System. This calibration is referenced to dry air at a temperature of 32F (__C) and a pressure of 29.92 in.Hg (760Torr).

		Set F	low	True F	low
5	%	500.0	CCM	492.49	CCM
10	%	1000.0	CCM	993.99	CCM
20	%	2000.0	CCM	1993.1	CCM
30	%	3000.0	CCM	3001.5	CCM
40	*	4000.0	CCM	4013.9	CCM
50	%	5000.0	CCM	5023.3	CCM
-60	%	6000.0	CCM	6044.5	CCM
70	ૠ	7000.0	CCM	7049.0	CCM
80	%	8000.0	CCM	8093.5	CCM
90	%	9000.0	CCM	9096.6	CCM
100	3%	10000	CCM	10104.	CCM

Calibration data was last saved on

Tuesday 11 July 00

at 11:46:00

Date: 7 - 11 - 00

FLOW CONTROLLER CALIBRATION SHEET

Mf #: 2, Description: AIR

, Size: 10000. SCCM, K-factor: 1.0

SERIAL # AW9502157

This flow controller was calibrated using a Sierra Cal Bench(TM), a traceable Primary Flow Standard Calibration System. This calibration is referenced to dry air at a temperature of 32°F (__C) and a pressure of 29.92 in.Hg (760Torr).

	Set Flow	True Flow
5 %	500.0 CCM	497.4 CCM
10 %	1000.0 CCM	997.84 CCM
20 %	2000.0 CCM	1998.9 CCM
30 %	3000.0 CCM	3011.3 CCM
40 %	4000.0 CCM	4026.6 CCM
50%	5000.0 CCM	5047.7 CCM
60 %	6000.0 CCM	6066.1 CCM
70 %	7000.0 CCM	7077.7 CCM
80 %	8000.0 CCM	8124.4 CCM
90 %	9000.0 CCM	9142.1 CCM
100%	10000. CCM	10158. CCM

Calibration data was last saved on Tuesday 11 July 00 at 11:48:00

Date: 7 - 11 - 00

FLOW CONTROLLER CALIBRATION SHEET

Mf #: 3, Description: AIR

, Size: 1000.0 SCCM, K-factor: 1.0

SERIAL # AW9502153

This flow controller was calibrated using a Sierra Cal Bench(TM), a traceable Primary Flow Standard Calibration System. This calibration is referenced to dry air at a temperature of $32^{\circ}F$ (__C) and a pressure of 29.92 in.Hg (760Torr).

		Set Fl	low	True Fl	. OW
5	%	50.0	CCM	53.629	CCM
10	%	100.0	CCM	105.7	CCM
20	%	200.0	CCM	207.81	CCM
30	%	300.0	CCM	309.86	CCM
40	%	400.0	CCM	412.37	CCM
50	%	500.0	CCM	512.9	CCM
60	%	600.0	CCM	614.3	CCM
70	%	700.0	CCM	716.52	CCM
80	%	800.0	CCM	817.17	CCM
90	%	900.0	CCM	918.35	CCM
100	7%	1000.0	CCM	1020.3	CCM

Calibration data was last saved on Tuesday 11 July 00

at 12:57:00

Verified by: Karl Senterany Date: 7 - 11 - 00

FLOW CONTROLLER CALIBRATION SHEET

Mf #: 4, Description: AIR

, Size: 100.0 SCCM, K-factor: 1.0

SERIAL # AW9612049

This flow controller was calibrated using a Sierra Cal Bench(TM), a traceable Primary Flow Standard Calibration System. This calibration is referenced to dry air at a temperature of $32^{\circ}F$ (__C) and a pressure of 29.92 in.Hg (760Torr).

		Set	Flow	True F	low
5	%	5.0	CCM	5.111	CCM
10	%	10.0	CCM	10.254	CCM
20	%	20.0	CCM	20.567	CCM
30	%	30.0	CCM	30.68	CCM
40	%	40.0	CCM	41.01	CCM
50	%	50.0	CCM	50.852	CCM
60	%	60.0	CCM	61.185	CCM
70	%	70.0	CCM	71.366	CCM
80	%	80.0	CCM	81.508	CCM
90	%	90.0	CCM	91.794	CCM
100	3%	100.	O CCM	103.32	CCM

Calibration data was last saved on Thursday 16 December 99

at 14:43:00

Verified by: Kall Sentiany Date: 12 - 16 - 00

${\sf NO_X}$ Measurement System Interference Test

Operator:	Daniel Neal			Analyzer Type:	Chemiluminescent
Date:	9-Jul-00			Analyzer Manufacturer:	Thermo Environmental Instr.
Analyzer S	pan:	20	ppmv NO _X	Model No.	
				Serial No.	42H-41111-264

Measurement System Interference Determination

	Test Gas	Analyzer Output	Interference on 9/ of Succession
Component Tested	Component Concentration	Response, ppmv NO _X	Interference as % of Span
со	498.04 ppmv	-0.03	-0.15%
SO ₂	200.56 ppmv	0.09	0.45%
O ₂	20.9 % by volume	-0.05	-0.25%
CO ₂	-0.30%		
	-0.25%		
Sum of interferences mus	Pass		

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O₂ Measurement System Interference Test

Operator:	Daniel Neal			Analyzer Type:	Magnetopneumatic	
Date:	30-May-00			Analyzer Manufacturer:	-	
Analyzer Sp	an:	25	%O ₂ by volume	Model No.	01440CISTD	
				Serial No	1391	

Measurement System Interference Determination

	Test Gas	Analyzer Output	Interference on 9/ of Seen	
Component Tested Component Concentration		Response As %O ₂	Interference as % of Span	
СО	498.17 ppmv	0.10	0.40%	
SO ₂	196.65 ppmv	0.00	0.00%	
CO ₂	9.984 % by volume	0.10	0.40%	
	erference as % of Span	0.80%		
Sum of interferences must	Result:	Pass		

CO₂ Measurement System Interference Test

Operator:	Daniel Neal		Analyzer Type: single beam, dual wavelength IR		
Date:	Date: <u>30-May-00</u>		Analyzer Manufacturer:		
Analyzer Sp	an: 2	%CO ₂ by volume	Model No.	01440CISTD	
			Serial No.	1382	

Measurement System Interference Determination

	Test Gas	Analyzer Output	Interference 0/ -5 Color	
Component Tested Component Concentration		Response As %CO ₂	Interference as % of Span	
со	498.17 ppmv	0.10	0.50%	
SO ₂	196.58 ppmv	0.10	0.50%	
O ₂	20.9 % by volume	0.10	0.50%	
	erference as % of Span:	1.50%		
Sum of interferences must not exceed ±2% of span value.			Pass	

CO Measurement System Interference Test

Operator:	Daniel Neal 30-May-00			Analyzer Type:	NDIRS with GFC Thermo Environmental Instr.	
Date:				Analyzer Manufacturer:		
Analyzer S	oan: <u>1</u>	:ppmv CO Model N		48		
				Serial No.	48-29095-233	

Measurement System Interference Determination

	Test Gas	Analyzer Output	Interference as % of Span	
Component Tested	Component Concentration	Response, ppmv CO	interference as % of Span	
CO ₂	9.984 % by volume	-1.80	-1.80%	
Interference must not exc	eed ±2% of span value.	Result:	Pass	

A.3	Letter S	Summarizi	ng Result	s of Techni	cal Systen	n Audit and	Performan	ce Evaluation	
					·				



RESEARCH TRIANGLE INSTITUTE

Center for Environmental Measurements and Quality Assurance

October 17, 2000

Jack Balsinger Senior Quality Assurance Officer Midwest Research Institute 425 Volker Boulevard Kansas City, Missouri 64110-2299

Mr. Balsinger,

Please find enclosed the final report of a performance evaluation (PE) and a technical systems audit (TSA) of Midwest Research Institute's (MRI's) verification test of Catalytica Combustion System's XONON flameless combustion system at Silicon Valley Power's Gianera Generating Station in Santa Clara, California. These technical assessments were performed by Robert S. Wright of Research Triangle Institute (RTI) and Michael W. Tufts of ARCADIS Geraghty & Miller on July 17-18, 2000.

The verification testing was performed as part of the U.S. EPA's Environmental Technology Verification (ETV) Program. Under EPA Cooperative Agreement CR 826152-01-0, RTI is the prime contractor and MRI is a subcontractor in a ETV pilot project for the verification testing of air pollution control technologies. EPA's Environmental Technology Verification Program Quality and Management Plan for the Pilot Period (1995-2000) specifies that PEs are to be conducted, as applicable, for each test as provided in the test/quality assurance (QA) plan and that TSAs are to be conducted for each test as provided for in the project's test/QA plan.

The purpose of the PE and the TSA was to conduct an independent and objective technical assessment of the verification test through an in-depth evaluation of quality system documents, on-site activities, equipment, procedures, and record keeping to assure (1) that environmental data collection activities and related results comply with the project's test/QA plan and other quality system documents; (2) that these activities are implemented effectively; and (3) that these activities are suitable to achieve the project's data quality goals. These technical assessments were conducted in accordance with auditing principles and procedures in *EPA Guidance for Technical Assessments for Environmental Data Operations* (EPA Publication No. EPA QA/G-7, 2000). The basis for the TSA was MRI's *Test/QA Plan for the Verification Testing of Catalytica Combustion System, Inc. XONON Flameless Combustion System (Revision 1, July 5, 2000)*.

In general, Mr. Tufts and I found that MRI was doing a good job of testing the XONON technology. We found no deficiencies that would adversely impact the quality of results and that could have required stopping the test until they were corrected. The testing was executed according to the test/QA plan with only minor deviations. The equipment was appropriate for the testing and it was operating satisfactorily. The project personnel were well-qualified to perform the testing and conducted themselves in a professional manner. They cooperated with

Jack Balsinger October 17, 2000 Page 2

us during the TSA and the PE and took time out from their busy duties to explain to us what was happening. They helped to ensure the successful completion of the technical assessments.

A report on the results of the PE is attached to this letter. Because the only critical measurement for the verification test was the nitrogen oxides (NO_X) measurements by EPA Method 20, the PE involved only the continuous NO_X emissions monitor that MRI used during the test. The PE was performed using a compressed gas calibration standard, which was certified by its producer to contain 1.00 parts per million (ppm) of NO_X in nitrogen. This concentration approximates typical NO_X emissions levels for the XONON technology. The average response of the analyzer to the PE sample was 0.992 ppm during the morning of July 18 and 0.990 ppm during the afternoon. These responses differed by -0.8 percent and -1.0 percent, respectively, from the standard's certified concentration. They are well within the +/- 50 percent acceptance criterion that was established informally for the NO_X analyzer accuracy prior to the verification test.

The remainder of this letter summarizes TSA findings in which conditions appear to be different from the test/QA plan or in which some uncertainty exists. These conditions are unlikely to have a significant effect on data quality. They are numbered by the TSA checklist section where the question appears. The full completed checklist is attached to this letter.

Section	Findings about conditions, which do not have an significant effect on data quality.
A4	Two minor deviations from the test/QA plan were found. NO _X sampling probe traverses were performed in fewer directions than specified in the test/QA plan because of scaffolding limitations. The balance gas for one calibration standard was nitrogen, rather than air. Neither deviation effects data quality.
D4	The test/QA plan documents a data quality objective for the variability of the NO_X emission concentrations, which is the critical measurement in the verification test. It did not specify measurement performance criteria for the accuracy, precision, and completeness of the EPA Method 20, which is used to determine the NO_X emission concentrations. This omission in the plan is not a deficiency, but it produced some uncertainty regarding the acceptance criterion for the performance evaluation, which was established informally prior to the performance evaluation by RTI and MRI staff.
H19, Comments for Section H	The EPA Method 205 field evaluation was conducted on the NO _x analyzer's 50-ppm range, rather than the specified 20-ppm operating range, because of a questionable 9.92 ppm nitric oxide (NO) check standard that MRI had wanted to use on the 20-ppm range. There is something of a mystery surrounding the check standard. It was returned to the specialty gas producer for reanalysis because it produced questionable results before the test began. The recertified NO concentration was close to the original certified value. On July 18, Catalytica's NO _x analyzer measured the check standard and found it to contain 10.0 ppm, but MRI's NO _x measurement of the check standard on the same day found it to contain 9.40 ppm. Yet both analyzers produced very similar results (i.e., 1.0 ppm and 0.99 ppm, respectively) for EPA's 1.00 ppm NO _x performance evaluation sample. The discrepancy in the measured concentration of the check standard has not been resolved, but it probably does not effect on the quality of the NO _x measurements.

Jack Balsinger October 17, 2000 Page 3

Please contact me at 541-6263 or rsw@rti.org if you have any questions concerning the final report or the technical assessments.

Respectfully,

Robert S. Wright, Environmental Scientist

file: 93U-07012-032

cc: Paul Groff, EPA
Ted Brna, EPA
Craig Clapsaddle, MRI
Drew Trenholm, MRI
Jack Farmer, RTI
Doug VanOsdell, RTI
Mike Tufts, ARCADIS

APPENDIX B

Raw Test Data

- B.1 Raw Concentration Printouts from Labtech Notebook
- B.2 Raw Data Ambient Conditions
- **B.3** Emission Concentration Summaries
- B.4 Turbine Process Data

B.1 Raw Concentration Printouts from Labtech Notebook

Test Events Log Runs 1 - 3

Job No.	101494.1.004.02	Operator:	Daniel Neal	
		Date:	18-Jul-00	
Client:	CCSI	Date.	10-341-00	
Plant:	Gianera Generating Station			
Location:	Gas Turbine Outlet			
	•			
4:43	Send N ₂ direct to all analyzers			
4:50	Set Zero on the CO analyzer			
4:50	Send High CO directly to all analyzers			
4:58	Set High CO Calibration			
4:58	Send Mid CO directly to all analyzers			
5:01	Record Mid CO reading			
5:01	Send Low CO directly to all analyzers			
5:04	Record Low CO reading			
5:04	Send N2 to the system			
5:18	Set Zero on O ₂ , ĆO ₂ , and NO _X analyzers, record CO ze	ero		
5:20	Send Mid O ₂ to system			
5:29	Set Mid O ₂ on O ₂ analyzer			
5:29 5:21	Send High O ₂ to system			
5:31 5:31	Record High O_2 reading on the O_2 analyzer Send Mid CO_2 to system			
5:35	Set Mid CO ₂ to system Set Mid CO ₂ on CO ₂ analyzer			
5:35	Send High CO ₂ to system			
5:38	Record High CO ₂ reading on the CO ₂ analyzer			
5:40	Send Mid NO to the system			
5:50	Set Mid NO on NO _x analyzer			
5:50	Send High NO to system, change analyzer to Manual N	l ode		
5:53	Record High NO reading on the NO _X analyzer			
5:55	Send Low NO to the system			
5:58	Record Low NO reading on the NO _X analyzer			
5:58	Send Mid CO to system			
6:01	Record Mid CO reading on the CO analyzer			
6:30	Send Zero gas to THC system			
6:32	Set Zero on the THC analyzer			
6:32	Send High THC to THC system	•		
6:38	Set High on the THC analyzer			
6:38	Send Mid THC to THC system Record Mid THC reading on the THC analyzer			
6:41 6:41	Send Low THC to THC system			
6:44	Record Low THC reading on the THC analyzer			
5.77	1,000ia bon file foading on the file analyzar			
6:50	Turn to "Sample" and set probe at 1 st sampling point			
7:00	Start Run 1			
7:32	End Run 1			
	·			
7:33	Send N ₂ thru the system to all analyzers			
7:37	Record O2 zero			
7:36	Record CO2 zero			
7:37	Record Nox zero			
7:37	Record CO zero			
7:39	Send Mid O2 to system			
7:42	Record Mid O2 reading on the O2 analyzer			
7:43	Send Mid CO2 to system Record Mid CO2 reading on the CO2 analyzer			
7:45	Record wild CO2 reading off the CO2 analyzer			

ETV RTI Runs 1- 3.xls 7/25/00 11:26 AM

- 7:45 Send Mid NOx to system
- 7:50 Record Mid NOx reading on the NOx analyzer
- 7:50 Send Mid CO to system
- 7:54 Record Mid CO reading on the CO analyzer
- 7:55 Send zero to THC system
- 7:58 Record zero THC reading on the THC analyzer
- 7:58 Send Mid THC to system
- 8:01 Record Mid THC reading on the THC analyzer
- 8:10 Start Run 2
- 8:42 End Run 2
- 8:45 Send N₂ thru the system to all analyzers
- 8:48 Record O2 zero
- 8:50 Record CO2 zero
- 8:48 Record Nox zero
- 8:48 Record CO zero
- 8:51 Send Mid O2 to system
- 8:53 Record Mid O2 reading on the O2 analyzer
- 8:54 Send Mid CO2 to system
- 8:56 Record Mid CO2 reading on the CO2 analyzer
- 8:57 Send Mid NOx to system
- 9:01 Record Mid NOx reading on the NOx analyzer
- 9:02 Send Mid CO to system
- 9:06 Record Mid CO reading on the CO analyzer
- 9:07 Send zero to THC system
- 9:10 Record zero THC reading on the THC analyzer
- 9:13 Send Mid THC to system
- 9:17 Record Mid THC reading on the THC analyzer
- 9:20 Start Run 3
- 9:52 End Run 3
- 9:52 Send N_2 thru the system to all analyzers
- 9:56 Record O2 zero
- 9:56 Record CO2 zero
- 9:55 Record Nox zero
- 9:56 Record CO zero
- 9:58 Send Mid O2 to system
- 10:00 Record Mid O2 reading on the O2 analyzer
- 10:00 Send Mid CO2 to system
- 10:03 Record Mid CO2 reading on the CO2 analyzer
- 10:03 Send Mid NOx to system
- 10:07 Record Mid NOx reading on the NOx analyzer
- 10:07 · Send Mid CO to system
- 10:10 Record Mid CO reading on the CO analyzer
- 10:12 Send zero to THC system
- 10:16 Record zero THC reading on the THC analyzer
- 10:16 Send Mid THC to system
- 10:18 Record Mid THC reading on the THC analyzer

ETV/RTI Verification Test Runs 1 - 3 Time is 04:33:50.63. Date is 7-18-2000.

Time	7-16-20 CO	.00. O2	,	CO2	TGOC	NOx	
111116	ppm		-	%	ppm	ppm	
4	:33	-0.24	0.12			1.66	-0.03
	:34	-0.2	0.12			1.66	-0.03
	:35	-0.25	0.29			1.65	-0.04
	:36	-0.1	0.26			1.64	-0.03
	:37	0.35	0.32			1.63	-0.03
	:38	0.07	0.31			1.66	-0.03
	:39	-0.12	0.31			1.68	-0.02
	:40	-0.23	0.33			1.66	-0.03
	:41	-0.01	0.3			1.66	-0.03
	:42	-0.07	0.29			1.66	-0.02
	:43	-0.09	0.31			1.64	-0.03
	:44	-0.07	0.26			1.66	-0.04
	:45	3.28	0.26			1.61	-0.04
4	:46	0.52	0.26			1.65	-0.04
4	:47	0.49	0.26			1.79	-0.04
4	:48	0.23	0.24			1.82	-0.04
4	:49	0.19	0.24			1.76	-0.04
4	:50	0.07	0.27	(0.1 ·	1.74	-0.04
4	:51	0.21	0.29	-0.	05	1.78	-0.03
4	:52	0.27	0.18	- 0.	05	1.94	8.59
4	:53	1.2	0.3	-0.	04	1.7	11.71
4	:54	39.9	0.32	-0.	04	1.62	0.01
4	:55	46.04	0.33	-0.	07	1.62	-0.01
4	:56	45.42	0.33	-0.	07	1.62	-0.03
4	:57	45.1	0.27	0.	14 '	1.58	-0.04
4	:58	45.13	0.27	0.	14	1.6	-0.04
	:59	46.22	0.24	0.	21 -	1.63	0.04
5	:00	33.15	0.26	0.	18 -	1.59	-0.04
5	:01	30.03	0.25	0.	18	1.6	-0.04
	:02	33.27	0.16	0.		1.58	-0.02
	:03	15.64	0.27	0.		1.61	-0.03
	:04	15.01	0.29	-0.		1.63	-0.03
	:05	17.11	3.91	-0.		1.65	-0.02
	:06	2.19	0.33	-0.		1.95	-0.02
	:07	0.11	0.33	-0.		2.21	-0.03
	:08	0.15	0.35	-0.		2.24	-0.03
	:09	0.09	0.25	-0.		1.9	-0.02
	:10	0.03	0.11			1.66	-0.04
	:11	0	0.04			1.71	-0.03
	:12	0.15 0.03	0.04			1.64	-0.04
	:13 :14	0.03	0.02			1.61	-0.06
	:15	0.13	0.04 0.05			1.62	-0.06
	:16	0.07	0.05			1.69 1.74	-0.06 -0.06
	:17	0.14	0.03	-0.		1.69	-0.05
	:18	0.14	0.00	-0. -0.		1.74	-0.05
	:19	0.13	5.09	-0. -0.		1.72	-0.05
	:20	0.2	19.37	-0.		1.69	-0.05
	:21	0.83	12	-0.		1.62	-0.05
	:22	0.08	12.2	-0.		1.57	-0.05
	:23	-0.02	12.15			1.59	-0.05
	:24	-0.04	12.16			1.72	-0.06
	:25	-0.01	12.15		16	1.7	-0.06
	:26	0	12.09			1.66	-0.06
	:27	-0.02	12.08			1.59	-0.06
5	:28	0.01	12.06			1.75	-0.06
	:29	-0.03	12.06			1.87	-0.06
	:30	0.16	17.48	-0.		1.97	-0.05
5	:31	-0.02	21.05	-0.		2.21	-0.05
5	:32	0.07	14.92	0.		2.18	-0.05

5:33	0.16	0.18	3.05	1.79	-0.05
5:34	-0.05	0.14	3.05	1.92	-0.05
5:35	-0.14	0.14	3.08	2.15	-0.05
5:36	-0.01	4.05	5.11	2.03	-0.05
5:37	-0.46	-0.06	10.31	1.91	-0.06
5:38	-0.48	-0.06	10.35	2.01	-0.06
5:39	-0.44	4.54	7.97	2.1	-0.06
5:40	-0.1	19.48	0.66	2.03	-0.06
5:41	-0.05	0.99	0.49	2.04	-0.06
5:42	0.15	0.09	0.22	1.93	5.1
5:43	0.17	0.12	0.03	1.96	14.38
5:44	0.09	0.12	-0.06	1.84	9.67
5:45	0.09	0.14	-0.05	2.1	10.01
5:46	0.17	0.12	-0.05	1.61	10
5:47	0.21	0.12	-0.05	1.62	9.95
5:48	0.12	0.11	-0.09	1.59	9.96
5:49	.0.07	0.12	-0.07	1.5	10.01
5:50	0.01	0.07	0.12	1.43	10.03
5:51	0.02	4.44	0.18	1.49	8.92
5:52	0.02	0.05	0.14	1.52	16.78
5:53	0.05	0.04	0.14	1.55	17.14
5:54	0.07	2.12	0.16	1.97	13.64
5:55	0.04	10.75	0.2	1.95	3.91
5:56	0	2.74	0.12	1.87	7.27
5:57	0.11	0.14	-0.03	2.11	4.95
5:58	0.11	0.13	-0.06	1.82	4.94
5:59	2.51	4.18	-0.04	1.67	5.82
6:00	27.87	0.15	-0.07	1.84	0.7
6:01	29.79	0.14	-0.04	1.86	0.05
6:02	29.78	0.13	-0.07	1.55	0.03
6:03	16.54	15.33	0.13	1.51	0.06
6:04	0.7	16.2	0.19	1.49	0.09
6:05	25.76	0.14	0.12	1.95	0.08
6:06	19.45	10.43	2.24	2.09	0.39
6:07	1.05	15.36	3.15	2.49	1.18
6:08	2.14	6.72	1.4	1.67	0.81
6:09	0.95	10.38	2.15	2	0.77
6:10	0.39	5.43	0.99	2.45	0.41
6:11	0.54	6.87	1.24	2.03	0.54
6:12	0.41	10.25	1.96	2.58	0.77
6:13	0.26	0.19	-0.06	2.36	0.05
6:14	0.35	10.78	2.06	2.38	0.75
6:15	0.88	15.42	2.93	2.35	1.08
6:16	0.84	9.77	1.92	2.27	0.72
6:17	0.08	0.14	0.16	2.97	0.05
6:18	0.46	11.53	2.44	1.83	0.76
6:19	0.94	7.17	1.53	2.15	0.52
6:20	0.38	8.82	1.91	1.85	0.61
6:21	0.55	6.72	1.43	1.95	0.51
6:22	0.27	8.88	1.94	1.82	0.62
6:23	0.89	15.42	2.99	2.66	1.04
6:24	0.92	15.46	2.92	2.42	1.03
6:25	1.01	15.46	2.93	2.27	1.03
6:26	1	15.47	2.94	1.88	1.03
6:27	0.96	15.48	2.94	1.93	1.04
6:28	1.04	15.46	2.92	2.73	1.04
6:29	1.22	15.49	2.96	2.8	1.04
6:30	1.38	15.43	3.16	1.27	1.04
6:31	0.95	15.39	3.18	-0.01	1.09
6:32	0.64	15.41	3.19	-0.02	1.07
6:33	0.88	15.43	3.17	60.72	1.07
6:34	0.98	15.42	3.17	90.3	1.06
6:35	0.96	15.42	3.18	84.98	1.05
6:36	1.05	15.45	3.1	85.07	1.06
6:37	1	15.48	2.99	85.11	1.06
6:38	1.24	15.48	2.96	85.07	1.05

6:39	1.27	15.49	2.96	66.06	1.05
6:40	1.35	15.47	2.97	50.06	1.06
6:41	0.74	15.48	2.93	49.99	1.1
6:42	0.95	15.49	2.95	39.19	1.07
6:43	1.01	15.44	3.07	29.96	1.05
6:44	0.99	15.43	3.15	29.89	1.03
6:45	0.9	15.42	3.14	23.05	1.04
6:46	1	15.41	3.15	22	1.03
6:47	0.94	15.43	3.17	17.74	1.03
6:48	1.19	15.43	3.16	45.16	1.03
6:49	1.21	15.42	3.16	50.68	1.02
6:50	1.25	15.48	2.97	40.38	1.05
6:51	8.0	15.47	2.97	1.05	1.09
6:52	0.89	15.47	2.99	0.86	1.06
6:53	0.98	15.49	2.93	1.28	1.05
6:54	1.01	15.49	2.95	1.11	1.04
6:55	1	15.49	2.95	1.13	1.04
6:56	1	15.46	3.03	1.12	1.03
6:57	1	15.42	3.19	1.16	1.04
6:58	1.16	15.43	3.17	0.35	1.03
6:59	1.21	15.42	3.16	0.37	1.04
7:00	0.94	15.42	3.16	0.48	1.09
7:01	0.59	15.44	3.16	0.29	1.1
7:02	0.92	15.42	3.17	0.24	1.07
7:03	0.96	15.46	3	0.22	1.07
7:04	0.93	15.49	2.94	0.21	1.05
7:05	1.16	15.49	2.94	0.19	1.05
7:06	1.2	15.48	2.92	0.2	1.06
7:07	1.18	15.47	2.93	0.2	1.06
7:08	1.38	15.49	2.94	0.18	1.07
7:09	1.16	15.49	2.94	0.18	1.11
7:10	0.68	15.45	3.14	0.13	1.11
7:11	0.94	15.39	3.16	0.14	1.1
7:12	0.95	15.43	3.19	0.12	1.09
7:13	0.98	15.41	3.19	0.14	1.09
7:14	1.02	15.44	3.17	0.1	1.06
7:15	1.17	15.43	3.17	0.09	1.05
7:16	1.13	15.43	3.11	0.12	1.03
7:17	1.43	15.48	2.99	0.13	1.04
7:18 7:19	1.25 0.71	15.47	2.97	0.13	1.08
7:19	1.01	15.49 15.48	2.96 2.96	0.12 0.12	1.09
7:21	1.09	15.46	2.95	0.12	1.06
7:22	1.15	15.48	2.95	0.13	1.05 1.05
7:23	1.18	15.45	3.07	0.12	1.05
7:24	1.54	15.43	3.15	0.11	1.05
7:25	1.43	15.41	3.15	0.09	1.05
7:26	1.52	15.42	3.15	-0.11	1.07
7:27	0.91	15.44	3.14	0.09	1.12
7:28	0.89	15.44	3.17	0.09	1.11
7:29	0.98	15.41	3.15	0.1	1.11
7:30	1.27	15.49	2.98	0.11	1.09
7:31	1.36	15.49	2.95	0.1	1.09
7:32	1.4	15.49	2.93	0.11	1.07
7:33	1.6	15.49	2.97	0.11	1.06
7:34	1.78	13.15	2.42	0.1	0.92
7:35	0.43	0.25	-0.06	0.1	0.07
7:36	0.1	0.2	-0.03	0.1	0.05
7:37	0	0.11	0.14	0.09	0.04
7:38	0.07	0.09	0.19	-0.25	0.03
7:39	0.02	0.1	0.16	-0.19	0.02
7:40	0.06	3.31	0.83	0.06	0.22
7:41	0.82	12.41	1.07	0.07	0.35
7:42	-0.34	11.99	0.15	0.09	0.02
7:43	-0.04	12.75	0.73	0.09	0.24
7:44	0.4	2.32	2.99	0.09	0.22

7:45	0.15	0.14	3.06	0.09	0.03
7:46	0.06	4.48	3.04	0.09	0.03
7:47	0.53	1.76			
			0.57	0.11	7.58
7:48	0.12	0.18	-0.07	0.11	9.65
7:49	-0.2	0.17	-0.08	0.1	10.08
7:50	0.02	0.09	0.06	0.09	10.03
7:51	0.04	2.45	0.63	0.07	8.53
7:52	17.47	0.72	0.27	0.09	1.06
7:53	29.55	0.11	0.13	0.09	0.07
7:54	29.57	0.08	0.15	0.08	0.04
7:55	29.32	2.02	0.56	0.36	0.16
7:56	7.28	15.33	3.16	3.29	1.08
7:57	1.96	15.45	2.95	-0.08	1.13
7:58	1.35	15.43	2.93	-0.06	1.18
7:59	1.05	15.48	2.97	24.87	1.15
8:00	1.49	15.49	2.95	49.81	1.12
8:01	1.39	15.47	2.93	49.9	1.1
8:02	1.48	15.48	2.92	19.01	1.08
8:03	1.51	15.49	3.01	0.2	1.06
8:04	1.69	15.49	3.19		
8:05	1.77			0.14	1.05
	1.77	15.42	3.17	0.12	1.04
8:06		15.43	3.16	0.1	1.11
8:07	1.03	15.43	3.17	0.1	1.11
8:08	1.26	15.42	3.17	0.1	1.07
8:09	1.36	15.44	3.19	0.09	1.06
8:10	1.39	15.49	3.05	0.1	1.07
8:11	1.75	15.52	2.94	0.11	1.05
8:12	1.9	15.5	2.9	0.13	1.04
8:13	1.86	15.49	2.91	0.12	1.04
8:14	0.99	15.49	2.91	0.12	1.1
8:15	1.09	15.51	2.92	0.11	1.06
8:16	1.38	15.53	2.94	0.09	1.05
8:17	1.41	15.44	3.11	0.09	1.06
8:18	1.44	15.45	3.14	0.1	1.06
8:19	1.56	15.44	3.14	0.1	1.05
8:20	1.87	15.43	3.16	0.07	1.06
8:21	1.89	15.44	3.15	0.09	1.09
8:22	1.03	15.44	3.14	0.08	1.12
8:23	1.16	15.46	3.14	0.06	1.09
8:24	1.5	15.51	2.91	0.11	1.08
8:25	1.62	15.52	2.95	0.09	1.04
8:26	1.76	15.54	2.95	0.09	1.04
8:27	1.7	15.51	2.93	0.1	1.05
8:28	1.94	15.49	2.92	0.1	1.05
8:29	1.88	15.51	2.93	0.1	1.09
8:30	1.07	15.51	3.01	0.1	
8:31	1.35	15.44			1.1
8:32	1.44	15.46	3.19	0.07	1.06
8:33	1.58		3.17	0.07	1.05
8:34		15.45	3.17	0.07	1.04
	1.54	15.47	3.17	0.07	1.04
8:35	1.82	15.47	3.17	0.05	1.04
8:36	1.93	15.43	3.18	0.06	1.05
8:37	1.81	15.47	3.07	- 0.08	1.11
8:38	0.98	15.52	2.94	0.09	1.14
8:39	1.44	15.52	2.94	0.09	1.1
8:40	1.47	15.53	2.95	0.1	1.09
8:41	1.58	15.53	2.95	0.09	1.07
8:42	1.47	15.49	2.96	0.1	1.06
8:43	1.77	15.53	2.92	0.1	1.05
8:44	1.9	15.47	3.11	0.08	1.04
8:45	2.32	5.43	1.14	0.08	0.48
8:46	0.05	0.17	0.15	0.07	0.05
8:47	-0.04	0.15	0.2	0.07	0.04
8:48	0	0.11	0.15	0.08	0.04
8:49	0.02	0.11	0.14	0.06	0.03
8:50	0.02	0.12	0.12	0.06	0.02

8:51	0.01	0.16	-0.07	0.1	0.03
8:52	0.33	7.56	1.32	0.08	0.47
8:53	0.52	11.98	-0.04	0.07	0.03
8:54	0.07	12.66	0.46	0.09	0.19
8:55	0.92	10.85	2.68	0.03	
8:56	0.22	0.22			0.86
8:57			3.06	0.09	0.05
	-0.07	2.15	3.11	0.07	0.16
8:58	0.85	7.15	1.96	0.07	4.47
8:59	0.08	0.14	0.14	0.07	9.5
9:00	0.01	0.13	0.13	0.06	9.89
9:01	0	0.11	0.12	0.09	9.92
9:02	0.04	0.1	0.12	0.06	9.84
9:03	0.82	13.42	2.81	0.07	2.31
9:04	18.29	0.36	0.07	0.09	1.2
9:05	29.4	0.21	-0.08	0.09	0.11
9:06	29.55	0.21	-0.11	0.1	0.08
9:07	29.44	0.19	-0.09	0.09	0.06
9:08	14.46	13.43	2.55	2.27	0.89
9:09	1.15	15.46	2.91	-0.1	1.09
9:10	1.18	15.49	2.89	-0.07	1.07
9:11	1.29	15.45	3.06	-0.09	1.05
9:12	1.32	15.46	3.14	-0.13	1.03
9:13	1.45	15.47	3.14		1.03
9:14	1.64	15.47		-0.14	
			3.14	17.56	1
9:15	1.79	15.47	3.16	49.34	1.01
9:16	1.48	15.46	3.15	49.47	1.05
9:17	0.93	15.48	3.14	49.49	1.07
9:18	1.33	15.52	2.94	18.28	1.03
9:19	1.27	15.52	2.91	0.23	1.02
9:20	1.4	15.55	2.94	0.15	1.01
9:21	1.64	15.54	2.93	0.14	1
9:22	1.57	15.52	2.89	0.15	1
9:23	1.78	15.54	2.92	0.13	0.99
9:24	1.51	15.54	2.95	0.1	1.03
9:25	0.83	15.48	3.14	0.09	1.03
9:26	1.39	15.47	3.15	0.09	1.01
9:27	1.4	15.45	3.17	0.12	0.99
9:28	1.37	15.46	3.15	0.12	0.98
9:29	1.54	15.47	3.16	0.13	1
9:30	1.62	15.45	3.15	0.13	1
9:31	1.86	15.49	3.09	0.14	1.03
9:32	1.65	15.49	2.93	0.17	1.07
9:33	0.79	15.55	2.95	0.17	1.08
9:34	1.41	15.52	2.9	0.13	1.04
9:35	1.52	15.56	2.92		1.04
9:36	1.54			0.15	
		15.52	2.9	0.18	. 1
9:37 9:38	1.44	15.55	2.89	0.18	1
	1.34	15.51	3.04	0.16	0.98
9:39	1.56	15.48	3.16	0.12	0.98
9:40	1.45	15.49	3.16	0.11	0.99
9:41	0.59	15.46	3.16	0.12	1.04
9:42	1.28	15.49	3.16	0.11	1.01
9:43	0.98	15.45	3.16	0.14	1.01
9:44	1.09	15.45	3.19	0.14	1.01
9:45	1.17	15.52	3.04	0.15	1.02
9:46	1.33	15.52	2.94	0.16	1.02
9:47	1.25	15.54	2.93	0.16	1.02
9:48	1.6	15.54	2.94	0.14	1.02
9:49	0.91	15.54	2.93	0.15	1.06
9:50	0.82	15.53	2.96	0.15	1.03
9:51	0.9	15.54	2.92	0.15	1.01
9:52	1.09	15.47	3.11	0.14	1.01
9:53	1.08	14.14	2.85	0.14	0.98
9:54	1.48	0.27	0.16	0.14	0.07
9:55	-0.08	0.17	0.17	0.14	0.04
9:56	-0.07	0.17	0.17	0.14	
5.50	0.07	0.14	0.16	0.14	0.04

9:57	-0.1	0.14	0.15	0.14	0.03
9:58	-0.02	0.12	0.13	0.15	0.02
9:59	0.07	7.46	0.14	0.17	0.1
10:00	-0.1	12.06	-0.06	0.18	0.03
10:01	0.05	13.29	1.06	0.17	0.36
10:02	0.84	10.65	2.87	0.19	0.77
10:03	-0.01	0.2	3.07	0.19	0.05
10:04	0.22	7.39	3.07	0.2	0.5
10:05	0.42	0.58	0.22	0.2	8.71
10:06	0	0.11	0.17	0.17	9.56
10:07	-0.08	0.11	0.15	0.18	9.86
10:08	0.04	4.53	1.15	0.19	6.81
10:09	21.41	0.18	0.14	0.17	0.14
10:10	29.39	0.13	0.15	0.17	0.07
10:11	29.26	0.11	0.16	0.18	0.05
10:12	29.41	0.15	0.05	0.2	0.05
10:13	17.28	12.01	2.28	1.53	0.85
10:14	1.22	15.45	2.92	0.89	1.06
10:15	0.79	15.5	2.91	0.03	1.08
10:16	0.92	15.51	2.9	0.02	1.05
10:17	1.01	15.5	2.92	26.1	1.04
10:18	1.02	15.54	2.9	49.48	1.04
10:19	1.03	15.48	3.1	29.93	1.04
10:20	1.23 "	15.47	3.14	0.37	1.02
10:21	1.3	15.48	3.14	0.28	1.02
10:22	1.09	15.47	3.15	0.23	1.05
10:23	0.72	15.48	3.15	0.21	1.06
10:24	0.93	15.47	3.15	0.21	1.02
10:25	0.91	15.5	3.14	0.2	1
10:26	1.06	12.71	2.32	0.21	1.03
10:27	0.37	0.3	-0.08	0.21	1.02
10:28	-0.09	0.22	-0.06	0.22	1.02
10:29	-0.13	0.24	-0.07	0.2	0.99
10:30	-0.09	0.21	-0.08	0.22	0.99
10:31	-0.04	0.2	-0.06	0.19	0.98
10:32	-0.12	0.15	-0.02	0.21	0.98
10:33	-0.08	4.54	1.1	0.15	0.95
10:34	0.81	15.36	3.18	0.16	0.94
10:35	0.42	6.13	1.29	0.16	6.03
10:36	-0.28	0.15	0.14	0.19	9.4
10:37	-0.15	0.15	0.15	0.16	9.4
10:38	-0.16	0.13	0.18	0.15	9.4
10:39	-0.13	0.17	0.04	0.17	9.41
10:40	-0.08	4.26	0.81	0.2	6.9
10:41	0.83	15.39	2.89	0.19	0.99
10:42	0.89	15.5	2.93	0.2	0.98

Test Events Log Runs 4 - 6

Job No.	101494.1.004.02	Operator:	Daniel Neal
Client:	CCSI	Date:	18-Jul-00
Plant:	Gianera Generating Station		
Location:	Gas Turbine Outlet		
14:54	Send N ₂ direct to all analyzers		
15:01	Set Zero on the CO analyzer		
15:01	Send High CO directly to all analyzers		
15:06 15:06	Set High CO Calibration Send Mid CO directly to all analyzers		
15:00	Record Mid CO directly to all allaryzers		
15:10	Send Low CO directly to all analyzers		
15:14	Record Low CO reading		
15:14	Send N2 to the system	•	
15:20	Set Zero on O ₂ , ĆO ₂ , and NO _X analyzers, record CO zer	o	
15:20	Send Mid O ₂ to system		
15:22	Set Mid O ₂ on O ₂ analyzer		
15:22	Send High O ₂ to system		
15:25	Record High O ₂ reading on the O ₂ analyzer		
15:25	Send Mid CO ₂ to system		
15:35 15:35	Set Mid CO_2 on CO_2 analyzer Send High CO_2 to system		
15:38	Record High CO ₂ to system Record High CO ₂ reading on the CO ₂ analyzer		
15:38	Send Mid NO to the system		
15:46	Set Mid NO on NO _x analyzer		
15:47	Send High NO to system, change analyzer to Manual M	ode	
15:50	Record High NO reading on the NO _X analyzer		
15:50	Send Low NO to the system		
15:53	Record Low NO reading on the NO _X analyzer		
15:53	Send zero gas to system for CO		•
15:58	Record zero CO reading on the CO analyzer		
16:01	Send Mid CO to system Record Mid CO reading on the CO analyzer		
16:05 16:05	Send Zero gas to THC system		
16:03	Set Zero on the THC analyzer		
16:14	Send High THC to THC system		
16:17	Set High on the THC analyzer		
16:17	Send Mid THC to THC system		
16:20	Record Mid THC reading on the THC analyzer		
16:20	Send Low THC to THC system		
16:24	Record Low THC reading on the THC analyzer		
46.04	Turn to "Sample" and set probe at 1 st sampling point		
16:24 16:40	Start Run 4		
17:12	End Run 4		
11.14	best that I would to 1		
17:15	Send N ₂ thru the system to all analyzers		
17:18	Record O2 zero		
17:18	Record CO2 zero		
17:18	Record Nox zero		
17:19	Record CO zero		
17:21	Send Mid O2 to system		
EIVKIIK	tuns 4 - 6 7/18/00 10:34 PM		

17:23	Record Mid O2 reading on the O2 analyzer
17:23	Send Mid CO2 to system
17:26	Record Mid CO2 reading on the CO2 analyzer
17:28	Send Mid NOx to system
17:32	Record Mid NOx reading on the NOx analyzer
17:32	Send Mid CO to system
17:37	Record Mid CO reading on the CO analyzer
17:37	Send zero to THC system
17:40	Record zero THC reading on the THC analyzer
17:40	Send Mid THC to system
17:43	Record Mid THC reading on the THC analyzer
17:50	Start Run 5
18:22	End Run 5
10.22	
18:24	Send N ₂ thru the system to all analyzers
18:28	Record O2 zero
18:28	Record CO2 zero
18:28	Record Nox zero
18:29	Record CO zero
18:30	Send Mid O2 to system
18:34	Record Mid O2 reading on the O2 analyzer
18:34	Send Mid CO2 to system
18:37	Record Mid CO2 reading on the CO2 analyzer
18:37	Send Mid NOx to system
18:41	Record Mid NOx reading on the NOx analyzer
18:41	Send Mid CO to system
18:45	Record Mid CO reading on the CO analyzer
18:47	Send zero to THC system Record zero THC reading on the THC analyzer
18:51 18:51	Send Mid THC to system
18:54	Record Mid THC to system Record Mid THC reading on the THC analyzer
10.54	Record wild 1110 leading of the 1110 dilayzor
18:58	Start Run 6
19:30	End Run 6
19:32	Send N ₂ thru the system to all analyzers
19:35	Record O2 zero
19:35	Record CO2 zero
19:35	Record Nox zero
19:36	Record CO zero
19:36	Send Mid O2 to system
19:39	Record Mid O2 reading on the O2 analyzer.
19:39	Send Mid CO2 to system
19:42	Record Mid CO2 reading on the CO2 analyzer
19:43	Send Mid NOx to system
19:47	Record Mid NOx reading on the NOx analyzer
19:47	Send Mid CO to system
19:52	Record Mid CO reading on the CO analyzer
19:52	Send zero to THC system Record zero THC reading on the THC analyze
19:56	Send Mid THC to system
19:56	Record Mid THC to system Record Mid THC reading on the THC analyzer
20:00	Record wild This reading on the This alialyzer

ETV/RTI Verification Test 1st Day PM Test Time is 14:50:05.04. Date is 7-18-2000.

Date is	7-10-20		00	000	TOO	
Time	CO		O2	CO2	TGOC	NOx
	ppm) · · · · ·	%	%	ppm	ppm
14	:50	0	0.24	0.1	0.24	0.
14	:51	-0.02	0.21	0.14	0.25	0
	:52	0.37	0.16	0.15	0.24	0
	:53	0.15	0.17	0.14	0.22	Ō
	.56 :54	-0.03	0.17	0.13		0
	:55	0.46	4.86	0.85	0.25	0.32
	:56	0.22	0.21	-0.06	0.3	0.01
	:57	0.13	0.19	-0.05	0.33	0.01
14	:58	0.05	0.21	-0.07	0.28	0.01
14	:59	-0.07	0.2	-0.08	0.26	0.01
15	:00	0.07	0.19	-0.09	0.24	0.01
	:01	-0.07	0.15	0.02	0.23	0.01
	:02	12.94	0.12	0.13	0.21	0.02
	:03	44.33	0.17	0.13	0.19	0.02
	:04	44.71				
			0.17	0.13	0.19	0
	:05	44.9	0.14	0.15	0.22	0.01
	:06	44.98	0.11	0.18	0.2	0
	:07	45.86	0.13	0.15	0.18	0
15	:08	34.12	0.19	-0.05	0.24	0.01
15	:09	29.94	0.21	-0.07	0.2	0.01
15	:10	30.01	0.21	-0.06	0.2	0.01
	:11	34.52	0.12	-0.12	0.23	0.04
	:12	16	0.2	-0.11	0.07	0.02
	:13	14.9	0.23	-0.09	-0.34	0.01
	:14	14.9	0.22	0.01	-0.34	0.01
	:15	17.12				
			2.41	0.65	-0.34	0.37
	:16	2.14	0.26	0.16	-0.3	0.07
	:17	0	0.13	0.15	-0.2	0.05
	:18	0.1	0.12	0.15	-0.19	0.03
	:19	-0.03	0.06	0.16	-0.3	0.02
15	:20	0.11	0.05	0.12	-0.3	0.02
15	:21	0.68	5.23	0.11	-0.18	0.08
15	:22	0.31	12.01	-0.07	-0.21	0.03
15	:23	0.08	15.34	0.19	-0.36	0.09
	:24	-0.04	20.95	-0.04	-0.36	0.01
	:25	-0.13	20.98	-0.06	-0.3	0.02
	:26	-0.05	21	-0.07	-0.13	0.02
	.20 :27	0.16	18.85	1.02	-0.18	0.31
	:28	0.58	0.58	3.05	-0.25	0.02
	:29	-0.13	0.12	3.25	-0.3	0
	:30	-0.21	0.07	3.26	-0.29	0.01
	:31	-0.16	0.05	3.26	-0.3	0.01
	:32	-0.26	0.03	3.27	-0.24	0
15	:33	-0.23	0.02	3.2	-0.3	0
15	:34	-0.14	0.06	2.98	-0.25	0.01
15	:35	-0.16	0.11	2.95	-0.26	0.01
	:36	0.02	2.04	5.27	-0.3	0.12
	:37	-0.24	-0.04	9.56	-0.25	0.02
	:38	-0.45	0.04	9.59	-0.37	0.02
	:39	-0.42	-0.03	9.6	-0.37	0.02
		0.2	-0.03			
	:40			6.14	-0.29	0.46
15	:41	0.65	1.03	0.62	-0.3	7.59

45.40	0.00				
15:42	0.22	0.1	0.2	-0.24	10.28
15:43	0.08	0.06	0.17	-0.28	15.19
15:44	-0.14	0.06	0.17	-0.33	8.28
15:45	0.07	0.03	0.17	-0.3	10
15:46	0.12	0.04	0.13	-0.24	9.94
15:47	0.15				
		1.26	0.18	-0.26	11.16
15:48	0.2	0.12	-0.07	-0.21	12.98
15:49	0.12	0.1	-0.03	-0.27	16.95
15:50	0.04	0.1	-0.04	-0.15	16.93
15:51	0.3	1.69	0.22	-0.22	13.82
15:52	0.3	0.1	-0.06	-0.27	4.96
15:53	0.07	0.11	0.03	-0.28	4.92
15:54	0.04	0.06	0.15	-0.42	4.9
15:55	0.13	2.21			
			0.52	-0.37	2.39
15:56	-0.05	0.05	0.13	-0.28	0.05
15:57	0.11	0.03	0.13	-0.32	0.03
15:58	0.09	0.02	0.18	-0.41	0.02
15:59	0.12	0.06	0.16	-0.39	0.02
16:00	10.87	3.45	0.59	-0.28	0.96
16:01	22.33	0.81	0.08	-0.24	0.17
16:02	3.21	1.17	0.16	-0.37	0.17
16:03	28.25	0.13	-0.09	-0.23	0.05
16:04	29.95	0.13		-0.32	
			-0.1		0.04
16:05	29.95	0.13	-0.08	-0.31	0.03
16:06	30.06	1.38	0.27	-0.28	0.09
16:07	8.27	15.22	3	2.27	0.95
16:08	1.37	15.31	2.98	-0.53	1.03
16:09	0.81	15.35	2.98	-0.52	1.09
16:10	0.85	15.35	2.98	-0.61	1.06
16:11	0.89	15.36	3	0.03	1.03
16:12	0.96	15.38	2.97	-0.04	1.02
16:13	1.03	15.46	2.79	0.07	0.99
16:14	1.02	15.47	2.77	-0.17	0.96
16:15	1.19	15.45	2.78	45.44	0.97
16:16	1.53	15.42	2.8	85. 23	0.99
16:17	1.17	15.42	2.77	85.47	1.03
16:18	0.85	15.44	2.78	68. 63	1.02
16:19	1.09	15.42	2.85	50. 31	0.98
16:20	1.12	15.37	2.99	50.12	0.97
16:21	1.2	15.38	2.96	42.04	0.95
16:22	1.25	15.39	2.96	30.17	0.94
16:23	1.22	15.42	2.96	29.96	0.93
16:24	1.59	15.38	2.99	30	0.94
16:25	0.99	15.38	3	21.28	0.99
16:26	0.94	15.37	2.82	0.24	0.98
16:27	1.3	13.32	2.34	0.26	0.97
16:28	1.15	0.22	-0.04	0.11	1.02
16:29	0	0.15	-0.04	0.15	1.01
16:30	0.01	0.17	-0.08	0.15	1
16:31	0.06	0.14	-0.08	0.16	0.99
16:32	0.02	0.12	-0.04	0.26	0.98
16:33	0	0.07	0.14	0.28	0.97
16:34	-0.12	0.04	0.15	0.06	0.96
16:35	0.03	5.49	1.21	0.19	0.93
16:36	1.19				
		15.26	2.98	0.05	0.9
16:37	1.34	15.31	2.99	0.1	0.9
16:38	1.44	15.34	3.01	0.14	0.92
16:39	1.52	15.38	2.82	0.21	0.96

16:40	1.4	15.43	2.76	0.14	1
16:41	0.71	15.45	2.76	0.22	1.04
16:42	0.93	15.42	2.77	0.11	1.04
16:43	0.98	15.42	2.75	0.12	1.02
16:44	0.93	15.44	2.77	0.11	1
16:45	1.17	15.43	2.81	0.19	0.98
16:46	1.16	15.37	2.99	0.03	0.99
16:47	0.98	15.36	3.01	0.23	0.99
16:48	1.39	15.35	2.97	0.23	1
16:49	1.09	15.35	2.97	0.16	1.05
16:50	0.77	15.37	2.96	0.1	1.03
16:51	0.9	15.36	2.99	0.13	1.02
16:52	1.05	15.41	2.85	0.14	1.01
16:53	0.98	15.44	2.77	0.09	1.01
16:54	1.1	15.4	2.77	0.23	1.01
16:55	1.2	15.42	2.8		
				0.11	1
16:56	1.42	15.43	2.81	0.17	0.99
16:57	1.24	15.42	2.77	0.18	1.02
16:58	0.79	15.41	2.8	0.08	1.05
16:59	0.7	15.37	2.96	0.19	1
17:00	0.96				
		15.37	2.98	0.14	0.96
17:01	0.97	15.38	2.96	0.11	0.94
17:02	1.26	15.35	2.96	0.14	0.94
17:03	1.17	15.36	2.97	0.24	0.94
17:04	1.35	15.33	3	0.15	0.94
17:05	1.37	15.4			
			2.89	0.17	0.96
17:06	1.08	15.41	2.78	0.13	1.02
17:07	0.96	15.4	2.77	0.16	1
17:08	0.99	15.41	2.77	0.16	0.98
17:09	1.16	15.43	2.79	0.19	0.99
17:10	1.11	15.44	2.76	0.12	0.99
			•		
17:11	1.19	15.43	2.76	0.17	0.99
17:12	1.24	15.38	2.97	0.19	0.98
17:13	1.26	15.37	3.01	0.14	0.98
17:14	0.89	15.36	3.03	0.09	1.01
17:15	0.68	15.37	2.99	0.13	1.01
17:16	0.76				0.57
		7.71	1.55	0.09	
17:17	0	0.13	0.17	0.15	0.04
17:18	0.21	0.12	0.07	0.07	0.03
17:19	0	0.14	-0.07	0.23	0.04
17:20	0.07	0.13	-0.07	0.21	0.03
17:21	0.06	4	0.69	0.15	0.27
17:22	0.87	12.06	1.31	0.25	0.52
17:23	-0.03	12	-0.02	0.17	0.03
17:24	0.3	12.47	0.37	0.23	0.15
17:25	0.04	1.43	2.93	0.07	0.19
17:26	-0.13	0.06	3.17	0.18	0.02
17:27	-0.24	0.03	3.18	0.14	0.01
17:28	0.08	5.74	3.19	0.11	0.36
17:29	0.72	10.43	2.27	0.16	2.58
17:30	0.07	0.08	0.17	0.19	9.48
17:31	0.07	0.07	0.12	0.13	9.82
17:32	0.17	0.11	-0.03	0.17	9.91
17:33	0.29	3.7	0.64	0.13	7.85
17:34	15.44	1.42	0.16	0.18	1.69
17:35	29.89	0.12	-0.05	0.16	0.07
17:36	29.53	0.11	-0.06	0.14	0.05
17:37	29.88	0.11	-0.08	0.14	0.04

17:38	25.5	6.7	1.37	1.72	0.43
17:39	2.01	15.3	2.96	-0.06	0.97
17:40	1.05	15.31	3.01	-0.06	0.99
17:41	1.01	15.32	2.99	16.62	1.05
17:42	0.58	15.34	2.99	49.73	1.05
17:43	0.57	15.36	2.99	49.79	1.02
17:44					
	0.67	15.37	2.92	30.41	1.01
17:45	0.42	15.42	2.77	0.26	1
17:46	0.87	15.43	2.76	0.21`	0.99
17:47	0.68	15.42	2.76	0.27	1.01
17:48	0.94	15.43	2.76	0.16	1.01
17:49					
	0.94	15.42	2.8	0.17	1
17:50	0.96	15.43	2.78	0.21	1.04
17:51	0.48	15.36	2.96	0.14	1.05
17:52	0.73	15.37	2.99	0.15	1.02
17:53	0.7	15.36	3.01	0.12	1
17:54	0.74	15.37			
			2.97	0.14	1
17:55	0.77	15.39	2.97	0.23	1
17:56	0.9	15.38	2.97	0.14	1.01
17:57	0.91	15.38	2.91	0.15	1.04
17:58	0.96	15.45	2.8	0.14	1.05
17:59	0.85	15.42	2.79		
				0.14	1.09
18:00	0.68	15.42	2.78	0.19	1.09
18:01	0.79	15.42	2.78	0.14	1.07
18:02	0.83	15. 41	2.8	0.14	1.1
18:03	1.09	15.43	2.76	0.16	1.05
18:04	1	15.37	2.94	0.12	1.05
18:05	1.18	15.38	2.96	0.19	
					1.04
18:06	1.38	15.37	2.99	0.13	1.03
18:07	1.46	15.35	2.99	0.16	1.05
18:08	0.67	15.35	2.99	0.18	1.08
18:09	0.78	15.37	2.99	0.1	1.04
18:10	1.07	15.36	2.93	0.09	1.03
18:11	1.07	15.4	2.81		
				0.24	1.03
18:12	1.19	15.44	2.76	0.19	1.04
18:13	1.16	15.44	2.76	0.25	1.03
18:14	1.28	15.45	2.76	0.17	1.02
18:15	1.3	15.42	2.78	0.22	1.04
18:16	0.91	15.42	2.78	0.14	1.09
18:17	0.73	15.39	2.93	0.15	1.08
18:18					
	0.87	15.37	2.98	0.1	1.06
18:19	0.97	15.35	3.01	0.17	1.06
18:20	1.05	15.34	3	0.11	1.05
18:21	1.04	15.37	2.97	0.03	1.05
18:22	1.23	15.36	2.97	0.05	1.04
18:23	1.3	15.39			
			2.91	0.15	1.06
18:24	1.05	15.41	2.8	0.15	1.12
18:25	1.7	11.83	2.07	0.14	0.96
18:26	0.77	0.18	-0.05	0.13	0.05
18:27	-0.01	0.15	-0.05	0.06	0.03
18:28	0.17	0.12	-0.02	0.13	0.03
18:29	0.02				
		0.1	-0.03	0.05	0.03
18:30	0.03	0.06	0.09	0.18	0.01
18:31	0.33	3.43	0.31	0.12	0.09
18:32	0.13	11.9	0.14	0.09	0
18:33	0	11.94	0.16	0.04	0
18:34	0	11.95	0.15	0.21	0.01
18:35	0.14	9.14	1.72	0.19	0.38
.0.00	0.17	J. 14	1.12	0.19	0.36

18:36 18:37	-0.07 -0.03	0.06	3.1	0.05	0.02
18:38	0.22	0.06	2.98	0.08	0.01
18:39		6.77	2.85	0	0.44
18:40	0.66 0.23	1.08	0.3	0.05	8.34
18:41		0.11	-0.07	0.15	9.76
	0.05	0.09	-0.06	0.25	9.93
18:42 18:43	0.32	5.36	0.95	0.18	6.29
18:44	23.16	0.09	0.09	0.18	0.1
18:45	29.72 29.81	0.05	0.15	0.12	0.04
18:46		0.02	0.16	0.16	0.03
	29.79	0.04	0.19	0.01	0.02
18:47 18:48	19.73	10.4	2.09	14.72	0.67
18:49	1.29 0.77	15.29	2.97	26.17	1.06
18:50	1	15.32 15.4	2.9	-0.05	1.09
18:51	1.16	15.4	2.79	-0.01	1.06
18:52	1.10	15.39	2.77	0.01	1.06
18:53	1.27	15.43	2.78	25.43	1.06
18:54	1.37	15.43	2.78 2.8	50.05	1.05
18:55	1.5	15.42		50.15	1.04
18:56	1.43	15.38	2.8 2.93	24.6	1.04
18:57	0.95	15.35	2.93 2.96	0.2	1.08
18:58	1.11	15.35	2.96	0.28 0.24	1.07
18:59	1.12	15.34			1.04
19:00	1.32	15.37	2.99 2.98	0.1	1.03
19:01	1.09	15.37	2.99	0.12	1.02
19:02	1.57	15.36	2.99	0.13	1.02
19:03	1.52	15.42	2.82	0.08 0.12	1.02 1.04
19:04	0.96	15.42	2.8	0.12	
19:05	1.28	15.41	2.76	0.17	1.09 1.1
19:06	1.18	15.45	2.76	-0.03	1.07
19:07	1.2	15.42	2.77	0.17	1.07
19:08	1.29	15.42	2.78	0.17	1.03
19:09	1.2	15.36	2.92	0.11	1.02
19:10	1.06	15.38	2.99	0.14	1.06
19:11	0.94	15.37	2.99	0.07	1.06
19:12	1.24	15.35	3.02	0.07	1.07
19:13	0.93	15.37	2.98	0.11	1.12
19:14	0.7	15.37	2.97	0.09	1.08
19:15	1.16	15.37	2.92	0.15	1.06
19:16	0.9	15.42	2.78	0.13	1.06
19:17	1.08	15.41	2.78	0.14	1.06
19:18	1.13	15.43	2.77	0.12	1.06
19:19	1.29	15.42	2.78	0.12	1.05
19:20	1.49	15.41	2.79	0.13	1.04
19:21	1.19	15.39	2.82	0.1	1.09
19:22	0.98	15.38	2.91	0.1	1.06
19:23	1.19	15.35	2.96	0.1	1.03
19:24	1.07	15.36	2.97	0.07	1.03
19:25	1.28	15.37	3	0.11	1.04
19:26	1.51	15.33	2.97	0.06	1.04
19:27	1.69	15.38	2.99	0.15	1.01
19:28	1.53	15.36	2.96	0.16	1.04
19:29	0.95	15.42	2.82	0.09	1.07
19:30	0.76	15.41	2.8	0.09	1.03
19:31	1.03	15.46	2.77	0.05	1.01
19:32	1.14	15.41	2.76	0.01	1.01
19:33	2.25	8.87	1.48	0.02	0.69

19:34	-0.08	0.17	-0.04	0	0.04
19:35	0.19	0.08	0.07	0.06	0.03
19:36	0.1	0.04	0.15	0.02	0.03
19:37	-0.04	0.19	0.2	0.03	0.02
19:38	0.03	11.61	0.63	-0.11	0.18
19:39	-0.09	11.95	0.16	0.11	0.01
19:40	0.11	10.06	1.72	0.05	0.44
19:41	0.01	0.06	3.1	0.11	0.02
19:42	-0.22	0.07	2.93	0.09	0.01
19:43	0.01	6.87	2.86	0.11	0.46
19:44	1.22	14.48	2.81	0.05	1.04
19:45	0.23	0.22	-0.01	0.07	9.25
19:46	0.13	0.1	-0.06	0.08	9.79
19:47	0.05	0.09	-0.02	0.06	9.9
19:48	3.2	2.63	0.67	0.07	5.1
19:49	27.6	0.06	0.14	0.03	0.07
19:50	29.58	0.06	0.14	0.08	0.04
19:51	29.06	0.02	0.14	0.06	0.03
19:52	29.86	0.04	0.15	0.05	0.02
19:53	25.19	7.23	1.51	2.19	0.5
19:54	2.51	15.3	2.96	-0.09	1.03
19:55	1.58	15.36	2.78	-0.1	1.03
19:56	1.31	15.38	2.82	-0.09	1.02
19:57	1.31	15.38	2.79	27.22	1.03
19:58	1.57	15.41	2.79	49.58	1.03
19:59	1.61	15.42	2.78	49.78	1.05
20:00	0.76	15.42	2.77	49.95	1.09
20:01	1.12	15.38	2.89	50.07	1.06
20:02	1.86	13.63	2.62	17.61	1.06
20:03	5.95	0.16	0.14	0.2	0.12
20:04	4.89	0.08	0.14	0.13	0.03
20:05	4.66	0.07	0.16	0.11	0.02
20:06	4.78	0.04	0.17	0.1	0.02
20:07	7.08	5.73	0.18	0.09	0.02
20:08	11.82	0.11	-0.04	0.11	0.02
20:09	9.79	0.1	-0.06	0.11	0.01
20:10	9.89	0.09	-0.03	0.15	0.01
20:11	9.53	1.41	-0.08	1.66	0.01
20:12	14.36	0.1	-0.08	1.29	0.01
20:13	15	0.11	-0.09	1.25	0.01
20:14	14.52	2.7	-0.01	1.16	0.01

Test Events Log Runs 7 - 12

Job No.	101494.1.004.02	Operator:	Daniel Neal
Client:	CCSI	Date:	19-Jul-00
		Date.	13-341-00
Plant:	Gianera Generating Station		
Location:	Gas Turbine Outlet		
4:21	Send N ₂ direct to all analyzers		
4:25	Set Zero on the CO analyzer		
4:25	Send High CO directly to all analyzers		
4:28	Set High CO Calibration		
4:28	Send Mid CO directly to all analyzers		
4:31	Record Mid CO reading		
4:31	Send Low CO directly to all analyzers		
4:35	Record Low CO reading		
4:35 4:41	Send N2 to the system Set Zero on O_2 , CO_2 , and NO_X analyzers, record CO_2	ero	
4:41	Send Mid O_2 to system	.010	
4:46	Set Mid O_2 on O_2 analyzer		
4:46	Send High O ₂ to system		
4:51	Record High O ₂ reading on the O ₂ analyzer		
4:51	Send Mid CO ₂ to system		
5:44	Set Mid CO ₂ on CO ₂ analyzer		
5:44	Send High CO ₂ to system		•
5:47	Record High CO ₂ reading on the CO ₂ analyzer		
5:47	Send Mid NO to the system		
5:53 5:53	Set Mid NO on NO _X analyzer	Modo	
5:53 5:56	Send High NO to system, change analyzer to Manual I Record High NO reading on the NO _x analyzer	vioue	
5:56	Send Low NO to the system		
6:00	Record Low NO reading on the NO _X analyzer		
6:00	Send Mid CO to system		
6:05	Record Mid CO reading on the CO analyzer		
6:08	Send Zero gas to THC system		
6:13	Set Zero on the THC analyzer		
6:13	Send High THC to THC system		
6:19	Set High on the THC analyzer		
6:19 6:22	Send Mid THC to THC system Record Mid THC reading on the THC analyzer		
6:22	Send Low THC to THC system		
6:25	Record Low THC reading on the THC analyzer		
0.20			
	Turn to "Sample" and set probe at 1 st sampling point		
6:40	Start Run 7		
7:12	End Run 7		
7.10	Cond N. thru the system to all analyzers		
7:12 7:47	Send N ₂ thru the system to all analyzers Record O2 zero		•
7:17 7:17	Record CO2 zero		
7:17 7:17	Record Nox zero		
7:17 7:17	Record CO zero		
7:17 7:17	Send Mid O2 to system		
7:20	Record Mid O2 reading on the O2 analyzer		
7:20	Send Mid CO2 to system		
7:23	Record Mid CO2 reading on the CO2 analyzer		

7:23 7:28 7:28 7:32 7:33 7:36 7:36 7:40	Send Mid NOx to system Record Mid NOx reading on the NOx analyzer Send Mid CO to system Record Mid CO reading on the CO analyzer Send zero to THC system Record zero THC reading on the THC analyzer Send Mid THC to system Record Mid THC reading on the THC analyzer
7:45 8:17	Start Run 8 End Run 8
8:17 18:21 18:21 18:21 18:21 18:25 18:25 18:25 18:28 18:28 8:33 8:33 8:37 8:37 8:40 8:40 8:44	Send N ₂ thru the system to all analyzers Record O2 zero Record CO2 zero Record Nox zero Record CO zero Send Mid O2 to system Record Mid O2 reading on the O2 analyzer Send Mid CO2 to system Record Mid CO2 reading on the CO2 analyzer Send Mid NOx to system Record Mid NOx to system Record Mid NOx reading on the NOx analyzer Send Mid CO to system Record Mid CO reading on the CO analyzer Send Zero to THC system Record Zero THC reading on the THC analyzer Send Mid THC to system Record Mid THC reading on the THC analyzer
8:50 9:22	Start Run 9 End Run 9
9:27 9:30 9:30 9:30 9:31 9:32 9:36 9:39 9:39 9:43 9:43 9:44 9:54 9:54	Send N ₂ thru the system to all analyzers Record O2 zero Record CO2 zero Record Nox zero Record CO zero Send Mid O2 to system Record Mid O2 reading on the O2 analyzer Send Mid CO2 to system Record Mid CO2 reading on the CO2 analyzer Send Mid NOx to system Record Mid NOx to system Record Mid NOx reading on the NOx analyzer Send Mid CO to system Record Mid CO reading on the CO analyzer Send Zero to THC system Record Zero THC reading on the THC analyzer Send Mid THC to system Record Mid THC reading on the THC analyzer
11:20 11:52	Start Run 10 End Run 10
11:53 11:58 11:58	Send N ₂ thru the system to all analyzers Record O2 zero

ETV RTI Runs 7 -12.xls 7/25/00 1:25 PM

11:58	Record CO zero
11:58	Send Mid O2 to system
12:01	Record Mid O2 reading on the O2 analyzer
12:01	Send Mid CO2 to system
12:04	Record Mid CO2 reading on the CO2 analyzer
12:04	Send Mid NOx to system
12:09	Record Mid NOx reading on the NOx analyzer
12:09	Send Mid CO to system
12:15	Record Mid CO reading on the CO analyzer
12:15	Send zero to THC system
12:19	Record zero THC reading on the THC analyzer
12:19	Send Mid THC to system
12:24	Record Mid THC reading on the THC analyzer
12:30	Start Run 11
13:02	End Run 11
•	
13:05	Send N ₂ thru the system to all analyzers
13:10	Record O2 zero
13:10	Record CO2 zero
13:10	Record Nox zero
13:10	Record CO zero
13:10	Send Mid O2 to system
13:13	Record Mid O2 reading on the O2 analyzer
13:13	Send Mid CO2 to system
13:16	Record Mid CO2 reading on the CO2 analyzer
13:16	Send Mid NOx to system
13:21	Record Mid NOx reading on the NOx analyzer
13:21	Send Mid CO to system
13:25	Record Mid CO reading on the CO analyzer
13:25	Send zero to THC system
13:28	Record zero THC reading on the THC analyzer
13:28	Send Mid THC to system
13:32	Record Mid THC reading on the THC analyzer
	•
13:36	Start Run 12
14:08	End Run 12
14:08	Send N ₂ thru the system to all analyzers
14:12	Record O2 zero
14:12	Record CO2 zero
14:12	Record Nox zero
14:12	Record CO zero
14:12	Send Mid O2 to system
14:16	Record Mid O2 reading on the O2 analyzer
14:16	Send Mid CO2 to system
14:19	Record Mid CO2 reading on the CO2 analyzer
14:19	Send Mid NOx to system
14:25	Record Mid NOx reading on the NOx analyzer
14:25	Send Mid CO to system
14:31	Record Mid CO reading on the CO analyzer
14:31	Send zero to THC system
14:34	Record zero THC reading on the THC analyzer
14:34	Send Mid THC to system
14:40	Record Mid THC reading on the THC analyzer

ETV/RTI Verification Test 2nd Day AM & PM Test Time is 04:21:30.73. Date is 7-19-2000.

Time	CO .	O2	CO2	TGOC	NOx
	ppm	%	%	ppm	ppm
4:21	-0.24	20.14	0.29	1.12	0
4:22	-0.29	20.07	0.23	1.34	0
4:23	-0.15	0.71	0.03	1.23	0.01
4:24		0.1	-0.09	1.22	0
4:25		0.05	-0.11	1.37	0
4:26		-0.02	-0.1	1.38	0.03
4:27		0.02	-0.11	1.44	0.02
4:28		0.07	-0.12	1.35	0
4:29		0.01	-0.09	1.21	0.01
4:30 4:31	30.38 30.12	-0. 04 -0. 05	0.13 0.17	1.03	-0.01
4:32		-0.05	0.17	1.05 1.08	-0.02 0.01
4:33		-0.03	0.15	0.97	-0.01
4:34		-0.07	0.15	0.97	-0.01
4:35		-0.05	0.16	1.01	-0.02
4:36	12.44	13.68	0.05	1.13	0.01
4:37	1.36	0.25	-0.11	1.01	0.01
4:38		0.04	-0.1	1	0.01
4:39	0.26	0.02	-0.11	1.07	0.01
4:40		0.03	-0.03	1.1	0
4:41	0.16	0.02	-0.05	1.11	0
4:42		5.51	-0.05	0.97	0.01
4:43 4.44	0.26 -0.04	11.83 11.87	0.15	0.99 0.95	0
4: 44 4:45	-0.04	11.07	0.17 0.18	1.03	0 -0.01
4:46		11.95	0.15	1.06	-0.01
4:47	0.05	15.26	0.16	1.11	-0.01
4:48	-0.07	20.84	0.15	1.16	-0.01
4:49	-0.2	20.89	0.1	1.11	-0.01
4:50	-0.09	20.92	-0.06	1.14	0
4:5 1	-0.08	20. 93	-0.05	1.18	0
4:52	-0.19	9.28	1.45	1.23	0.01
4:53	-0.19	0.12	2.9	1.25	0
4:54	-0.15	0.05	2.91	1.41	0.01
4:55 4:56	-0.17 -0.22	0.04 -0.04	2.91	1.4	0.01
4:56 4:57	-0.22	-0.04	3.13 3.14	1.46 1.4	0
4:58	-0.22	-0.08	3.14	1.34	0
4:59	-0.2	-0.06	3.06	1.37	0
5:00	-0.22	-0.07	3.06	1.09	Ö
5:01	-0.2	2.3	4.39	1.16	-0.01
5:02	-0.44	-0.14	9.57	1.15	0
5:03	-0.4	-0.12	9.45	1.07	0.01
5:04	-0.44	3.42	7.76	1.09	0.01
5:05	0.28	0.23	3	1.34	0
5:06	-0.07	-0.01	2.91	1.28	0
5:07 5:08	-0.17 -0.16	-0.02	2.9 2.91	1.17	0
5:09	-0.16	-0.02	3.1	1.35 1.21	0 -0.01
5:10	-0.2	-0.08	3.15	1.12	-0.01
5:10	-0.27	-0.07	3.16	1.28	-0.01
5:12	-0.27	-0.1	3.22	1.13	-0.01
5:13	-0.26	-0.08	3.27	1.38	0
5:14	0.1	-0.08	3.26	1.21	-0.01
5:15	-0.17	-0.07	3.19	1	-0.01
5:16	-0.17	-0.04	3.02	0.94	0
5:17	-0.22	-0.03	2.98	1.22	0
5:18	-0.22	-0.03	2.96	1.12	0

5:19	-0.11	0.96	1.77	1.16	0
5:20	-0.01	0.02	-0.06	1.12	0
5:21	0.04	0	0	0.94	0
5:22	0	-0.04	0.16	0.99	-0.01
5:23	-0.03	-0.05	0.24	1.03	-0.02
5:24	-0.07	-0.07	0.25	. 1	-0.02
5:25	-0.03	-0.05	0.26	0.98	-0.02
5:26	-0.13	-0.06	0.27	0.9	-0.01
5:27	-0.02	-0.08	0.23	0.95	-0.01
5:28	-0.02	-0.05	0.17	0.95	-0.01
5:29	-0.02	0.01	-0.07	0.93	0
5:30	-0.11	0.01	-0.05	0.91	0
5:31	0.06	-0.01	-0.07	0.94	0
5:32	-0.02	0.01	-0.06	1.04	0
5:33	0.07	0.02	-0.04	1.09	-0.01
5:34	0.04	-0.01	. 0	1.1	-0.01
5: 35	-0.05	-0.03	0.16	1.25	-0.01
5:36	-0.13	1.59	1.53	1.16	-0.01
5:37	-0.25	-0.09	3.31	1.04	-0.02
5:38	-0.41	-0.1	3.28	0.98	-0.01
5:39	-0.29	-0.09	3.26	0.89	-0.02
5:40	-0.27	-0.11	3.18	0.98	-0.01
5:41	-0.25	-0.1	3.12	0.9	-0.01
5:42	-0.21	-0.03	2.86	1	0
5:43	-0.28	-0.04	2.85	0.97	0.01
5:44	-0.12	-0.04	2.9	1	0
5:45	-0.18	7.6	3.18	0.96	0.01
5:46	-0.45	-0.1	9.17	0.91	0
5:47	-0.44	-0.12	9.21	0.93	0.01
5:48	-0.54	-0.14	9.31	0.81	0
5:49	-0.52	7.65	5.8	0.92	0.01
5:50	-0.18	2.43	0.4	0.92	5.57
5:51	-0.08	-0.03	0.27	0.87	9.89
5: 52	-0.09	-0.03	0.23	0.8	10.01
5:53	-0.06	-0.04	0.25	0.94	9.95
5:54	0.01	0.96	0.34	0.93	10.89
5: 55	0.11	0	0.08	0.86	16.84
5: 56	-0.01	-0.01	0.01	0.95	16.8
5: 57	-0.01	0.36	0.03	0.91	16.17
5:58	0.01	0.52	0.09	0.99	5.56
5:59	-0.04	-0.01	0	1.06	4.88
6:00	0.04	-0.02	0.01	1.08	4.87
6:01	-0.02	4.99	0.08	1	3.67
6:02	-0.03	-0.02	0.22	0.93	0.03
6:03	2.67	1.61	0.28	1.04	0.65
6:04	27.85	-0.03	0.23	1.05	0.05
6:05	29.83	-0.06	0.23	0.92	0.02
6:0 6	26.08	1.18	0.23	0.88	0.08
6:07	1.44	2.05	0.27	1	0.01
6:08	19.57	0.39	0.13	0.95	0.04
6:09	18.75	13.33	0.04	3.19	0.06
6:10	0.09	20.11	0.05	0	0.07
6:11	0.17	20.1	0.06	-0.04	0.06
6:12	0.25	20.12	0.06	-0.2	0.05
6:13	0.24	20.18	0.03	0.02	0.05
6:14	0.16	20.17	0.05	29.73	0.04
6:15	0.08	20.11	0.22	84.96	0.05
6:16	-0.05	20.12	0.24	85.25	0.05
6:17	-0.02	20.13	0.26	85.06	0.04
6:18	-0.09	20.12	0.27	85.24	0.04
6:19	-0.09	20.13	0.27	85.04	0.04
6:20	0	20.1	0.27	66.76	0.04
6:21	0.05	20.12	0.21	50.05	0.04
6:22	0.12	20.15	0.05	49.95	0.05

6:23	0.16	20.19	0.05	38.14	0.04
6:24	0.07	20.17	0.04	30	0.04
6:25	0.12	20.18	0.03	30	0.04
6:26	0.11	20.2	0.04	29.94	0.04
6:27	0.23	20.19	0.02	15.41	0.03
6:28	0.11	20.11	0.21	2.47	0.02
6:29	0.28	20.14	0.24	0.03	0.02
6:30	0.23	20.1	0.28	1.21	0.02
6:31	0.22	20.12	0.28	1.12	0.02
6:32	0.25	20.12	0.26	1.12	0.02
6:33	0.23	20.14	0.20		
6:34	0.21	20.03	0.27	1.25 0.34	0.02
6:35	-0.16	20.1	0.16		0.03
6:36	0.10	20.2		0.16	0.03
	0.23		0.03	0.23	0.03
6:37		15.68	2.59	0.23	1.03
6:38	1.29	15.41	2.69	0.19	1.08
6:39	0.95	15.39	2.69	0.19	1.2
6:40	0.79	15.4	2.71	0.21	1.19
6:41	0.9	15.33	2.88	0.16	1.15
6:42	0.73	15.34	2.97	0.17	1.14
6:43	1.04	15.33	2.97	0.15	1.13
6:44	1.11	15.3	3	0.21	1.12
6:45	1.03	15.32	2.97	0.21	1.12
6:46	1.17	15.31	2.97	0.11	1.12
6:47	1.16	15.33	2.91	0.18	1.17
6:48	0.75	15.38	2.71	0.13	1.19
6:49	1	15.38	2.75	0.24	1.15
6:50	0.99	15.39	2.72	0.19	1.14
6:51	1.05	15.37	2.73	0.17	1.13
6:52	0.98	15.36	2.71	0.16	1.13
6:53	1.02	15.39	2.77	0.14	1.11
6:54	0.98	15.32	2.88	0.16	1.1
6:55	1.09	15. 31	2.96	0.18	1.09
6:56	1.11	15.31	2.96	0.09	1.12
6:57	0.52	15.3	2.96	0.15	1.14
6:58	0.73	15.31	2.99	0.08	1.11
6:59	0.89	15.35	2.96	0.15	1.1
7:00	0.97	15.34	2.96	0.17	1.09
7:01	0.91	15.39	2.72	0.1	1.1
7:02	0.68	15.4	2.73	0.14	1.1
7:03	1.54	15.36	2.75	0.18	1.11
7:04	2.15	15.4	2.75	0.16	1.1
7:05	0.62	15.4	2.73	0.14	1.14
7:06	0.81	15.38	2.71	0.11	1.19
7:07	1.04	15.36	2.85	0.12	1.15
7:08	1.11	15.33	2.99	0.21	1.12
7:09	1.24	15.35	2.96	0.07	1.12
7:10	1.3	15.34	2.95	0.01	1.11
7:11	0.81	15.32	2.95	0.18	1.1
7:12	0.97	15.32	2.98	0.17	1.1
7:13	1.49	14.45	2.75	0.17	1.06
7:14	1.17	0.28	0.08	0.13	0.04
7:15	-0.02	0.12	0.04	0.04	0.03
7:16	0.04	0.09	0.04	0.12	0.03
7:17	0.01	0.07	0.07	0.2	0.02
7:18	0	4.09	0.3	-0.02	0.12
7:19	-0.15	11.98	0.04	-0.05	0.01
7:20	-0.21	11.98	0.07	0.06	0.01
7:21	0.11	8.7	1.67	0.14	0.32
7:22	-0.31	-0.02	3.07	0.12	0.01
7:23	-0.81	-0.01	3.06	0.2	0.01
7:24	-0.02	6.77	3.06	0.04	0.5
7:25	0.46	3.81	0.98	0.05	6.65
7:26	-0.06	-0.01	0.25	0.07	9.55
·			2.20	0.07	0.00

7:27 -0.01 0.04 0.11 0.1 9.74 7:28 0.03 0.05 0.03 0.15 9.74 7:30 26.88 0.05 0.01 0.12 0.09 7:31 29.54 0.05 0.04 0.03 0.05 7:32 29.85 0.08 0.02 0.14 0.03 7:33 29.76 0.04 0 0.08 0.03 7:35 1.38 15.24 2.92 -0.04 1.1 7:36 0.92 15.28 2.95 -0.07 1.1 7:37 0.98 15.32 2.95 0.48 1.1 7:37 0.98 15.32 2.95 0.48 1.1 7:39 1.2 15.3 2.95 0.48 1.1 7:40 0.83 15.38 2.89 49.63 1.17 7:41 0.74 15.38 2.73 0.16 1.1 7:42 0.89 15.41						
7:28 0.03 0.05 0.03 0.15 9.74 7:29 1.6 3.28 0.66 0.1 5.79 7:30 26.88 0.05 0.01 0.12 0.09 7:31 29.54 0.05 0.04 0.03 0.05 7:32 29.85 0.08 0.02 0.14 0.03 7:33 29.76 0.04 0 0.08 0.03 7:34 22.55 8.27 1.76 0.39 0.61 7:36 0.92 15.28 2.95 0.04 1.1 7:37 0.98 15.32 2.95 0.48 1.1 7:39 1.2 15.31 2.96 48.35 1.11 7:39 1.2 15.38 2.89 49.63 1.17 7:40 0.83 15.38 2.89 49.63 1.17 7:41 0.74 15.38 2.73 0.16 1.08 7:43 1 15.42	7.27	-0.01	0.04	0.11	0.1	0.7
7:29 1.6 3.28 0.66 0.1 5.79 7:30 26.88 0.05 0.01 0.12 0.09 7:32 29.85 0.08 0.02 0.14 0.03 7:32 29.85 0.08 0.02 0.14 0.03 7:34 22.55 8.27 1.76 0.39 0.61 7:35 1.38 15.24 2.92 -0.04 1.1 7:36 0.92 15.28 2.95 -0.07 1.1 7:37 0.98 15.32 2.95 0.48 1.1 7:39 1.2 15.3 2.95 49.58 1.12 7:40 0.83 15.38 2.99 49.63 1.17 7:41 0.74 15.38 2.73 16.4 1.14 7:42 0.89 15.41 2.73 0.12 1.1 7:42 0.89 15.41 2.75 0.25 1.08 7:44 1.06 15.41 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>						
7:30 26.88 0.05 0.01 0.12 0.09 7:31 29.84 0.05 0.04 0.03 0.05 7:32 29.85 0.08 0.02 0.14 0.03 7:33 29.76 0.04 0 0.08 0.03 7:35 1.38 15.24 2.92 -0.04 1.1 7:36 0.92 15.28 2.95 0.07 1.1 7:37 0.98 15.32 2.95 0.48 1.1 7:37 0.98 15.32 2.95 0.48 1.1 7:39 1.2 15.3 2.95 0.48 1.1 7:40 0.83 15.38 2.89 49.63 1.17 7:40 0.83 15.38 2.89 49.63 1.17 7:42 0.89 15.41 2.73 0.12 1.1 7:43 1 15.41 2.75 0.25 1.08 7:44 1.06 15.41						
7:31 29.54 0.05 0.04 0.03 0.06 7:32 29.85 0.08 0.02 0.14 0.03 7:33 29.76 0.04 0 0.08 0.03 7:34 22.55 8.27 1.76 0.39 0.61 7:36 0.92 15.28 2.95 -0.07 1.1 7:37 0.98 15.32 2.95 0.48 1.1 7:38 1.19 15.31 2.96 48.35 1.11 7:39 1.2 15.3 2.95 49.58 1.12 7:40 0.83 15.38 2.89 49.63 1.17 7:40 0.83 15.41 2.73 0.12 1.1 7:42 0.89 15.41 2.73 0.18 1.04 7:43 1 15.42 2.73 0.18 1.09 7:44 1.06 15.41 2.75 0.14 1.09 7:45 1 15.41	7:29	1.6	3.28	0.66	0.1	5.79
7:31 29.54 0.05 0.04 0.03 0.05 7:32 29.85 0.08 0.02 0.14 0.03 7:33 29.76 0.04 0 0.08 0.03 7:34 22.55 8.27 1.76 0.39 0.61 7:36 0.92 15.28 2.95 -0.07 1.1 7:37 0.98 15.32 2.95 0.48 1.1 7:37 0.98 15.31 2.96 48.35 1.11 7:39 1.2 15.3 2.95 0.48 1.1 7:40 0.83 15.38 2.89 49.63 1.17 7:41 0.74 15.38 2.73 16.4 1.4 7:42 0.89 15.41 2.73 0.18 1.09 7:43 1 15.42 2.73 0.18 1.09 7:44 1.06 15.41 2.77 0.14 1.09 7:45 1 15.41	7:30	26.88	0.05	0.01	0.12	0.09
7:32 29.85 0.08 0.02 0.14 0.08 7:33 29.76 0.04 0 0.08 0.03 7:34 22.55 8.27 1.76 0.39 0.61 7:35 1.38 15.24 2.92 -0.04 1.1 7:36 0.92 15.28 2.95 0.48 1.1 7:37 0.98 15.32 2.95 0.48 1.1 7:38 1.19 15.31 2.96 48.35 1.11 7:39 1.2 15.38 2.89 49.63 1.17 7:41 0.74 15.38 2.73 16.4 1.14 7:42 0.89 15.41 2.73 0.18 1.09 7:43 1 15.42 2.73 0.18 1.09 7:44 1.06 15.41 2.75 0.25 1.08 7:47 1.26 15.35 2.9 0.07 1.06 7:48 1.05 15.33	7:31	29.54	0.05	0.04	0.03	0.05
7:33 29.76 0.04 0 0.08 0.03 7:34 22.55 8.27 1.76 0.39 0.61 7:35 1.38 15.24 2.92 -0.04 1.1 7:36 0.92 15.28 2.95 -0.48 1.1 7:37 0.98 15.32 2.95 0.48 1.1 7:38 1.19 15.31 2.96 48.35 1.11 7:39 1.2 115.3 2.95 49.58 1.12 7:40 0.83 15.38 2.89 49.63 1.17 7:42 0.89 15.41 2.73 0.12 1.1 7:42 0.89 15.41 2.73 0.18 1.09 7:44 1.06 15.41 2.75 0.25 1.08 7:44 1.06 15.41 2.75 0.25 1.08 7:44 1.05 15.35 2.9 0.07 1.06 7:48 1.15 15.33 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>						
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7:37 0.98 15.32 2.95 0.48 1.1 7:38 1.19 15.31 2.96 48.35 1.11 7:39 1.2 15.3 2.95 49.58 1.12 7:40 0.83 15.38 2.89 49.63 1.17 7:41 0.74 15.38 2.73 16.4 1.14 7:42 0.89 15.41 2.73 0.12 1.1 7:43 1 15.42 2.73 0.18 1.09 7:44 1.06 15.41 2.77 0.14 1.09 7:45 1 15.31 2.97 0.07 1.06 7:46 1.1 15.38 2.93 0.01 1.08 7:47 1.26 15.35 2.99 0.07 1.06 7:48 1.15 15.33 2.96 0.1 1.1 1.1 7:50 0.81 15.33 2.96 0.11 1.1 1.1 7:51	7:35	1.38	15.24	2.92	-0.04	1.1
7:37 0.98 15.32 2.95 0.48 1.1 7:38 1.19 15.31 2.96 48.35 1.11 7:39 1.2 15.3 2.95 49.58 1.12 7:40 0.83 15.38 2.89 49.63 1.17 7:41 0.74 15.38 2.73 0.12 1.1 7:42 0.89 15.41 2.73 0.12 1.1 7:43 1 15.42 2.73 0.18 1.09 7:44 1.06 15.41 2.77 0.14 1.09 7:45 1 15.41 2.77 0.14 1.09 7:47 1.26 15.35 2.9 0.07 1.08 7:47 1.26 15.35 2.9 0.07 1.08 7:48 1.15 15.33 2.96 0.1 1.1 7:49 0.87 15.33 2.96 0.1 1.1 7:50 0.81 15.33	7:36	0.92	15.28	2.95	-0.07	1.1
7:38 1.19 15.31 2.96 48.35 1.11 7:39 1.2 15.3 2.95 49.58 1.12 7:40 0.83 15.38 2.89 49.63 1.17 7:41 0.74 15.38 2.73 16.4 1.14 7:42 0.89 15.41 2.73 0.12 1.1 7:43 1 15.42 2.73 0.18 1.09 7:44 1.06 15.41 2.75 0.25 1.08 7:45 1 15.36 2.97 0.07 1.06 7:46 1.1 15.38 2.93 0.07 1.06 7:48 1.15 15.36 2.97 0.07 1.06 7:48 0.87 15.33 2.96 0.1 1.13 7:50 0.81 15.33 2.96 0.11 1.1 7:51 0.86 15.35 2.95 0.11 1.08 7:52 0.89 15.35	7:37	0.98				
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8:02 0.94 15.35 2.97 0.09 1.04 8:03 1.03 15.36 2.97 0.09 1.03 8:04 1.09 15.34 2.97 0.12 1.03 8:05 1.15 15.34 2.99 0.08 1.04 8:06 0.68 15.35 2.95 0.07 1.09 8:07 0.75 15.4 2.74 0.13 1.08 8:08 0.89 15.42 2.73 0.11 1.07 8:09 0.96 15.43 2.71 0.09 1.06 8:10 0.95 15.43 2.74 0.1 1.07 8:11 0.98 15.42 2.69 0.13 1.07 8:12 1.05 15.42 2.69 0.13 1.07 8:13 1.3 15.41 2.75 0.12 1.07 8:14 1.16 15.35 2.95 0.11 1.07 8:15 0.57 15.36<		0.9	15.34			
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8:44 0.84 15.36 2.97 49.31 1.05 8:45 0.93 15.36 2.97 49.27 1.05 8:46 1.19 15.37 2.98 21.11 1.03 8:47 1.14 15.42 2.79 0.22 1.02 8:48 1.09 15.43 2.69 0.29 1.05 8:49 0.63 15.44 2.7 0.16 1.08 8:50 0.84 15.45 2.69 0.21 1.05 8:51 0.97 15.46 2.69 0.13 1.03 8:52 0.91 15.46 2.69 0.19 1.03 8:53 0.99 15.45 2.69 0.19 1.03 8:54 0.89 15.4 2.93 0.13 1.01 8:55 1.27 15.39 2.96 0.39 1.06 8:55 1.26 15.37 2.96 0.39 1.06 8:58 0.68 15	8:43	0.88	15.35	2.98	49.22	1.06
8:45 0.93 15.36 2.97 49.27 1.05 8:46 1.19 15.37 2.98 21.11 1.03 8:47 1.14 15.42 2.79 0.22 1.02 8:48 1.09 15.43 2.69 0.29 1.05 8:50 0.84 15.45 2.69 0.21 1.05 8:51 0.97 15.44 2.69 0.19 1.03 8:52 0.91 15.46 2.69 0.13 1.03 8:53 0.99 15.45 2.69 0.19 1.03 8:53 0.99 15.45 2.93 0.13 1.01 8:53 0.99 15.45 2.93 0.13 1.01 8:55 1.27 15.39 2.94 0.18 1.01 8:56 1.29 15.37 2.96 0.39 1.06 8:57 1.05 15.38 2.96 0.39 1.06 8:59 1.01 1						
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8:49 0.63 15.44 2.7 0.16 1.08 8:50 0.84 15.45 2.69 0.21 1.05 8:51 0.97 15.44 2.69 0.19 1.03 8:52 0.91 15.46 2.69 0.13 1.03 8:53 0.99 15.45 2.69 0.19 1.03 8:54 0.89 15.4 2.93 0.13 1.01 8:55 1.27 15.39 2.94 0.18 1.01 8:56 1.29 15.37 2.96 0.39 1.06 8:58 0.68 15.38 2.96 0.39 1.06 8:59 1.01 15.39 2.96 0.39 1.02 9:01 0.98 15.44 2.75 0.41 1.02 9:02 1.18 15.38 2.92 0.39 1.02 9:03 1.24 15.44 2.75 0.41 1.02 9:04 1.33 15.44	8:48	1.09	15.43	2 69		
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8:58 0.68 15.38 2.96 0.39 1.02 8:59 1.01 15.39 2.96 0.39 1.02 9:00 1.18 15.38 2.92 0.39 1.02 9:01 0.98 15.44 2.75 0.41 1.02 9:02 1.18 15.43 2.76 0.4 0.99 9:03 1.24 15.44 2.73 0.4 0.99 9:04 1.33 15.44 2.71 0.42 0.99 9:05 1.19 15.45 2.73 0.39 1.02 9:06 0.62 15.46 2.71 0.4 1.03 9:07 0.99 15.43 2.86 0.37 1 9:08 1 15.39 2.96 0.38 0.98 9:10 1.02 15.4 2.98 0.39 0.98 9:11 1.23 15.37 2.97 0.38 0.98 9:13 1.01 15.37	8:56	1.29	15.37	2.96	0.35	1.01
8:58 0.68 15.38 2.96 0.39 1.05 8:59 1.01 15.39 2.96 0.39 1.02 9:00 1.18 15.38 2.92 0.39 1.02 9:01 0.98 15.44 2.75 0.41 1.02 9:02 1.18 15.43 2.76 0.4 0.99 9:03 1.24 15.44 2.73 0.4 0.99 9:04 1.33 15.44 2.71 0.42 0.99 9:05 1.19 15.45 2.73 0.39 1.02 9:06 0.62 15.46 2.71 0.4 1.03 9:07 0.99 15.43 2.86 0.37 1 9:08 1 15.39 2.96 0.38 0.98 9:10 1.02 15.4 2.98 0.39 0.98 9:11 1.23 15.37 2.97 0.38 0.98 9:12 1.21 15.35	8:57	1.05	15.38	2.96	0.39	1.06
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9:04 1.33 15.44 2.71 0.42 0.99 9:05 1.19 15.45 2.73 0.39 1.02 9:06 0.62 15.46 2.71 0.4 1.03 9:07 0.99 15.43 2.86 0.37 1 9:08 1 15.39 2.96 0.38 0.98 9:09 1.02 15.39 2.96 0.38 0.98 9:10 1.02 15.4 2.98 0.39 0.98 9:11 1.23 15.37 2.97 0.38 0.98 9:12 1.21 15.35 2.99 0.39 1 9:13 1.01 15.37 2.97 0.38 1.04 9:14 1.11 15.44 2.79 0.4 1.05 9:15 1.21 15.44 2.73 0.41 1.03 9:16 1.05 15.46 2.73 0.43 1.03 9:17 1.23 15.43	9:03	1.24	15.44	2.73	0.4	0.99
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9:11 1.23 15.37 2.97 0.38 0.98 9:12 1.21 15.35 2.99 0.39 1 9:13 1.01 15.37 2.97 0.38 1.04 9:14 1.11 15.44 2.79 0.4 1.05 9:15 1.21 15.44 2.73 0.41 1.03 9:16 1.05 15.46 2.73 0.43 1.03 9:17 1.23 15.43 2.71 0.43 1.04 9:18 1.14 15.45 2.73 0.43 1.03 9:19 0.95 15.45 2.7 0.44 1.02 9:20 1.66 15.44 2.71 0.44 1.02 9:21 1.2 15.37 2.92 0.43 1.04 9:22 0.82 15.39 2.93 0.43 1.05 9:23 0.87 15.38 2.97 0.43 1.02 9:24 0.96 15.38 <td>9:09</td> <td>1.02</td> <td>15.39</td> <td>2.96</td> <td>0.38</td> <td>0.98</td>	9:09	1.02	15.39	2.96	0.38	0.98
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9:16 1.05 15.46 2.73 0.43 1.03 9:17 1.23 15.43 2.71 0.43 1.04 9:18 1.14 15.45 2.73 0.43 1.03 9:19 0.95 15.45 2.7 0.44 1.02 9:20 1.66 15.44 2.71 0.44 1.02 9:21 1.2 15.37 2.92 0.43 1.04 9:22 0.82 15.39 2.93 0.43 1.05 9:23 0.87 15.38 2.97 0.43 1.02 9:24 0.96 15.38 2.94 0.44 1 9:25 1.06 15.39 2.95 0.44 0.99 9:26 1.4 15.39 2.94 0.44 0.98 9:27 1.37 14.94 2.74 0.46 0.97 9:28 0.61 0.35 0.06 0.46 0.06 9:29 0.02 0.17	9:15	1.21	15.44	2.73	0.41	1.03
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9:23 0.87 15.38 2.97 0.43 1.02 9:24 0.96 15.38 2.94 0.44 1 9:25 1.06 15.39 2.95 0.44 0.99 9:26 1.4 15.39 2.94 0.44 0.98 9:27 1.37 14.94 2.74 0.46 0.97 9:28 0.61 0.35 0.06 0.46 0.06 9:29 0.02 0.17 0.01 0.47 0.04 9:30 -0.04 0.14 0.01 0.47 0.03 9:31 -0.02 0.13 0.01 0.48 0.03 9:32 -0.03 0.1 0 0.48 0.03 9:33 0.34 4.63 0.61 0.48 0.36	9:22	0.82	15.39	2.93	0.43	
9:24 0.96 15.38 2.94 0.44 1 9:25 1.06 15.39 2.95 0.44 0.99 9:26 1.4 15.39 2.94 0.44 0.98 9:27 1.37 14.94 2.74 0.46 0.97 9:28 0.61 0.35 0.06 0.46 0.06 9:29 0.02 0.17 0.01 0.47 0.04 9:30 -0.04 0.14 0.01 0.47 0.03 9:31 -0.02 0.13 0.01 0.48 0.03 9:32 -0.03 0.1 0 0.48 0.03 9:33 0.34 4.63 0.61 0.48 0.36						
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9:27 1.37 14.94 2.74 0.46 0.97 9:28 0.61 0.35 0.06 0.46 0.06 9:29 0.02 0.17 0.01 0.47 0.04 9:30 -0.04 0.14 0.01 0.47 0.03 9:31 -0.02 0.13 0.01 0.48 0.03 9:32 -0.03 0.1 0 0.48 0.03 9:33 0.34 4.63 0.61 0.48 0.36			15.39	2.95	0.44	
9:27 1.37 14.94 2.74 0.46 0.97 9:28 0.61 0.35 0.06 0.46 0.06 9:29 0.02 0.17 0.01 0.47 0.04 9:30 -0.04 0.14 0.01 0.47 0.03 9:31 -0.02 0.13 0.01 0.48 0.03 9:32 -0.03 0.1 0 0.48 0.03 9:33 0.34 4.63 0.61 0.48 0.36	9:26	1.4	15.39	2.94	0.44	0.98
9:28 0.61 0.35 0.06 0.46 0.06 9:29 0.02 0.17 0.01 0.47 0.04 9:30 -0.04 0.14 0.01 0.47 0.03 9:31 -0.02 0.13 0.01 0.48 0.03 9:32 -0.03 0.1 0 0.48 0.03 9:33 0.34 4.63 0.61 0.48 0.36	9:27	1.37	14.94	2.74	0.46	
9:29 0.02 0.17 0.01 0.47 0.04 9:30 -0.04 0.14 0.01 0.47 0.03 9:31 -0.02 0.13 0.01 0.48 0.03 9:32 -0.03 0.1 0 0.48 0.03 9:33 0.34 4.63 0.61 0.48 0.36						
9:30 -0.04 0.14 0.01 0.47 0.03 9:31 -0.02 0.13 0.01 0.48 0.03 9:32 -0.03 0.1 0 0.48 0.03 9:33 0.34 4.63 0.61 0.48 0.36						
9:31 -0.02 0.13 0.01 0.48 0.03 9:32 -0.03 0.1 0 0.48 0.03 9:33 0.34 4.63 0.61 0.48 0.36						
9:32 -0.03 0.1 0 0.48 0.03 9:33 0.34 4.63 0.61 0.48 0.36						
9:33 0.34 4.63 0.61 0.48 0.36						
	9:32	-0.03		0	0.48	0.03
	9:33	0.34	4.63	0.61	0.48	0.36
	9:34	0.01	10			

9:35	0	11.96	0.24	0.45	0.01
9:36	-0.25	11.96	0.24	0.46	0.01
9:37	0	10.3	1.52	0.46	0.26
9:38	-0.28	0.08	3.09	0.45	0.20
9:39	-0.35	0.03	3.07	0.46	0.01
9:40	0.08	7.68	3.03	0.40	0.5
9:41	0.35	0.74	0.18		8.39
9:42	0.02		0.16	0.48	
9:43	0.02	0.12		0.48	9.46
9:43 9:44	0.01	0.09	0	0.48	9.55
	21.05	5.54	1	0.48	6.42
9:45		0.16	-0.01	0.5	0.16
9:46	29.42	0.12	-0.03	0.49	0.06
9:47	29.57	0.08	0.04	0.48	0.04
9:48	29.38	0.02	0.25	0.47	0.02
9:49	29.48	0.04	0.26	0.44	0.02
9:50	23.21	7.9	1.65	23.52	0.51
9:51	1.83	15.26	2.92	33.54	0.98
9:52	1.07	15.31	2.96	0.4	1.05
9:53	0.68	15.34	3	0.32	1.08
9:54	1.12	15.38	2.8	0.33	1.06
9:55	1.08	15.41	2.69	0.34	1.06
9:56	0.98	15.44	2.68	45.02	1.05
9:57	1.2	15.46	2.7	49.06	1.05
9:58	1.38	15.46	2.71	49.07	1.05
9:59	1.48	15.45	2.66	25.35	1.05
10:00	1.41	15.44	2.67	0.63	1.07
10:01	0.75	15.39	2.93	0.53	1.08
10:02	1.04	15.39	2.94	0.5	1.04
10:03	1.1	15.38	3	0.48	1.03
10:04	1.21	15.38	2.96	0.48	1.03
10:05	1.35	15.37	2.95	0.49	1.03
10:06	1.28	15.38	2.97	0.49	1.03
10:07	1.44	15.42	2.89	0.48	1.03
10:08	1.27	15.42	2.73	0.5	1.09
10:09	0.87	15.47	2.71	0.49	1.08
10:10	1.18	15.43	2.69	0.52	1.06
10:11	1.24	15.46	2.68	0.5	1.04
10:12	1.24	15.47	2.7	0.49	1.04
10:13	1.48	15.45	2.68	0.5	1.01
10:14	2.19	15.41	2.84	0.49	0.98
10:15	1.93	15.38	2.92	0.49	0.99
10:16	0.93	15.4	2.92	0.49	1.02
10:17	1.09	15.39	2.99	0.45	0.99
10:18	1.42	15.36	2.97	0.48	0.97
10:19	1.31	15.38	2.95	0.49	0.97
10:20	1.42	15.37	2.92	0.49	0.96
10:21	1.53	15.44	2.72	0.5	0.97
10:22	1.73	15.45	2.76	0.49	0.97
10:23	1.45	15.44	2.69	0.49	1.02
10:24	1.05	15.43	2.68	0.51	1.02
10:25	1.35	15.46	2.69	0.5	0.99
10:26	1.57	15.46	2.67	0.5	0.99
10:27	1.51	15.43	2.83	0.49	0.99
10:28	1.72	15.38	2.92	0.49	0.98
10:29	1.72	15.37	2.91		
10:29	1.78	15.37	2.95	0.48 0.46	0.98 1.01
10:31	1.05	15.41			1.01
10.31	1.05		2.98	0.47	
		15.36	2.99	0.49	1.01
10:33	1.43	15.38	2.96	0.48	1 01
10:34	1.68	15.43	2.74	0.5	1.01
10:35	1.92	15.44	2.7	0.51	1
10:36	1.99	15.43	2.72	0.51	1
10:37	2.28	15.44	2.7	0.5	1 07
10:38	1.25	15.44	2.67	0.5	1.07

10:39	1.37	15.45	2.67	0.51	1.04
10:40	1.7	15.44	2.72	0.5	1.01
10:41	1.63	15.38	2.93	0.53	0.99
10:42	1.94	15.38	2.93	0.53	0.99
10:43	1.93	15.37	2.93	0.51	0.99
10:44	2.21	15.37	2.94	0.5	0.99
10:45	1.36	15.36	2.97	0.49	1.05
10:46	1	15.36	2.99	0.49	1.04
10:47	1.46	15.42	2.77	0.51	1.04
10:48	1.59	15.47	2.71	0.5	1.03
10:49	1.86	15.45	2.69	0.52	1.04
10:50	1.9	15.43	2.68	0.51	1.04
10:51	2.07	15.4 5	2.68	0.51	1.05
10:52	1.62	15.47	2.67	0.51	1.1
10:53	1.13	15.47	2.69	0.5	1.1
10:54	1.44	15.38	2.92	0.49	1.06
10:55	1.57	15. 37	2.95	0.49	1.04
10:56	1.59	15.39	2.95	0.48	1.04
10:57	1.8	15.38	2.94	0.48	1.04
10:58	2.07	15.37	2.96	0.51	1.05
10:59	, 1.66	15.38	2.97	0.52	1.09
11:00	0.98	15.42	2.85	0.5	1.1
11:01	1.41	15.44	2.68	0.52	1.07
11:02	1.46	15.46	2.68	0.51	1.05
11:03	1.53	15.47	2.67	0.51	1.04
11:04	1.6	15.45	2.67	0.51	1.05
11:05	1.92	15.44	2.68	0.5	1.02
11:06	2.13	15.46	2.68	0.52	1.03
11:07	1.23	15.4	2.9	0.49	1.06
11:08	1.34	15.38	2.95	0.48	1.03
11:09	1.55	15.38	2.97	0.48	1
11:10	1.66	15.36	2.96	0.49	1
11:11	1.94	15.37	2.96	0.48	0.99
11:12	2.03	15.4	2.95	0.49	1
11:13	2.28	15.41	2.85	0.49	1.02
11:14	1.45	15.42	2.72	0.52	1.06
11:15	1.36	15.44	2.67	0.51	1.05
11:16	1.84	15.48	2.67	0.5	1.02
11:17	1.93	15.44	2.66	0.51	1.01
11:18 11:19	1.99	15.45	2.68	0.51	1
11:20	2.09 2.51	15.45	2.71	0.51	1
11:21	1.76	15.39 15.38	2.86	0.49	1
11:22	1.70	15.36	2.94	0.49	1.05
11:23	1.73	15.38	2.95 2.98	0.48 0.49	1.02 1
11:24	1.85	15.39	2.96		
11:25	2.01	15.38	2.91	0.48 0.49	0.99
11:26	2.14	15.42	2.87	0.48	0.99 0.99
11:27	2.39	15.44	2.68	0.52	1.02
11:28	1.4	15.46	2.7	0.49	1.07
11:29	1.46	15.45	2.66	0.53	1.06
11:30	1.74	15.43	2.68	0.46	1.03
11:31	1.92	15.45	2.69	0.28	1.03
11:32	1.92	15.46	2.71	0.3	1
11:33	2.12	15.39	2.84	0.24	1
11:34	2.21	15.39	2.93	0.25	1
11:35	1.61	15.38	2.93	0.24	1.04
11:36	1.22	15.39	2.94	0.26	1.03
11:37	1.56	15.42	2.95	0.25	1.01
11:38	1.72	15.4	2.9	0.26	0.99
11:39	1.92	15.38	2.91	0.26	0.98
11:40	2.21	15.46	2.68	0.28	0.99
11:41	2.2	15.45	2.68	0.24	1.01
11:42	1.27	15.44	2.72	0.23	1.08

11:43	1.22	15.48	2.7	0.28	1.06
11:44	1.51	15.44	2.68	0.24	1.05
11:45	1.69	15.46	2.7	0.23	1.04
11:46	1.62	15.41	2.8	0.25	1.05
11:47	1.62	15.39	2.94	0.19	1.05
11:48	2	15.4	2.92	0.25	1.04
11:49	1.73	15.37	2.92	0.26	1.07
11:50	0.92	15.41	2.92	0.08	1.09
11:51	1.35	15.37	2.96	0.24	1.04
11:52	1.37	15.39	2.91	0.24	1.04
11:53	1.78	15.45	2.73	0.21	1.04
	2.44	10.61			
11:54			1.8	0.09	0.74
11:55	0.61 -0.04	0.21	0.05	0.17	0.03
11:56		0.14	0.06	0.23	0.03
11:57	0.05	0.12	0.02	0.25	0.03
11:58	-0.03	0.12	0.01	0.26	0.02
11:59	0.14	5.61	0.48	0.3	0.19
12:00	-0.15	11.91	0.24	0.11	0.01
12:01	-0.07	11.97	0.23	0.21	0
12:02	0.16	10.87	1.05	0.15	0.29
12:03	0.05	0.09	3.03	0.14	0.02
12:04	-0.27	0.03	3.06	0.31	0.01
12:05	0.25	7.57	3.09	0.2	0.49
12:06	0.83	3.19	0.75	0.18	7.13
12:07	0.09	0.13	0.03	0.24	9.66
12:08	-0.05	0.11	0.02	0.25	9.77
12:09	0.04	0.1	0.05	0.2	9.78
12:10	1.68	2.98	0.52	0.31	6.24
12:11	26. 96	0.13	0	0.23	0.1
12:12	29.72	0.09	0	0.26	0.06
12:13	29.56	0.06	0.21	0.19	0.04
12:14	29.73	0.04	0.24	0.3	0.02
12:15	29.68	0.04	0.23	0.33	0.02
12:16	21.61	8.66	1.82	2.65	0.58
12:17	1.46	15.28	2.9	0.07	1.02
12:18	1.55	15.31	2.94	0.05	1.02
12:19	1.9	15.37	2.86	0.07	1.01
12:20	1.96	15.43	2.69	27.75	1.01
12:21	1.95	15.4	2.68	48.86	1
12:22	2.34	15.44	2.67	48.95	0.99
12:23	2.59	15.44	2.68	49.06	1.01
12:24	1.43	15.45	2.68	48.91	1.05
12:25	1.76	15.47	2.67	49	1.01
12:26	1.81	15.39	2.87	18.8	0.99
12:27	2	15.38	2.91	0.37	0.98
12:28	2.14	15.39	2.97	0.34	0.97
12:29	2.27	15.4	2.94	0.26	0.97
12:30	2.42	15.36	2.94	0.23	0.99
12:31	1.22	15.39	2.94	0.25	1.05
12:32	1.4	15.41	2.85	0.23	1.03
12:33	1.82	15.43	2.69	0.29	1.01
12:34	1.88	15.46	2.67	0.25	1
12:35	2.03	15.46	2.67	0.24	0.99
12:36	2.08	15.44	2.66	0.24	1
12:37	2.19	15.46	2.69	0.25	1.03
12:38	1.24	15.45	2.03	0.24	1.06
	1.42	15.4			
12:39 12:40	1.73	15.41	2.86 2.94	0.26 0.2	1.03 1.01
	1.73	15.41		0.21	1.01
12:41	1.84		2.96		
12:42		15.37	2.98	0.22	0.99
12:43	2.07	15.39	2.92	0.23	0.99
12:44	2.15	15.38	2.92	0.2	1 06
12:45	1.34	15.43	2.84	0.22	1.06
12:46	1.38	15.46	2.7	0.23	1.04

12:47	1.53	15.46	2.67	0.21	1.02
12:48	1.52	15.48	2.68	0.27	1.02
12:49	1.55	15.46	2.68	0.22	1.02
12:50	1.68	15.47	2.69	0.29	1
12:51	1.82	15.45	2.72	0.26	1.01
12:52	1.57	15.38	2.84	0.25	1.04
12:53	0.95	15.39	2.92	0.22	1.07
12:54	1.25	15.38	2.91	0.26	1.02
12:55	1.5	15.4	2.91	0.24	- 1
12:56	1.72	15.38	2.91	0.19	1
12:57	1.96	15.37	2.9	0.2	1
12:58	2.3	15.4	2.88	0.21	1.
12:59	2.31	15.47	2.68	0.21	1.03
13:00	1.33	15.44	2.72	0.3	1.06
13:01	1.76	15.47	2.7	0.1	1.02
13:02	1.97	15.46	2.69	0.28	1
13:03	2.64	11.55	1.95	0.23	0.79
13:04 13:05	1.11 -0.02	0.19 0.13	0.05	0.19	0.04
13:06	0.02	1.05	0.16	0.21	0.03
13:07	0.37	7.42	0.38 0.83	0.24 0.2	0.09
13:08	0.03	0.06	0.83	0.23	0.24 0.01
13:09	-0.04	0.07	0.25	0.23	0.01
13:10	-0.03	0.05	0.25	0.18	0
13:11	0.26	6.65	0.65	0.25	0.15
13:12	0.07	11.99	0.05	0.25	0.01
13:13	-0.02	12	0.04	0.19	0.01
13:14	0.22	9.38	1.44	0.2	0.35
13:15	-0.05	0.13	2.82	0.23	0.02
13:16	-0.2	0.11	2.82	0.21	0.02
13:17	0.26	6.43	2.82	0.27	0.42
13:18	0.79	2.81	0.7	0.2	7.69
13:19	0	0.06	0.22	0.2	9.72
13:20	0.02	0.05	0.23	0.17	9.78
13:21	0.04	0.02	. 0.24	0.21	9.78
13:22	0.83	2.94	0.78	0.17	6.85
13:23	25.68	0.07	0.28	0.21	0.1
13:24	29.65	0.04	0.24	0.2	0.05
13:25	29.67	0.12	0.06	0.19	0.04
13:26	24.25	7.27	1.34	2.73	0.51
13:27	2.34	15.37	2.67	0.05	1.02
13:28 13:29	1.04 1.25	15.39 15.43	2.68	0.05	1.06
13:29	1.48		2.66	29.34	1.04
13:31	1.57	15.44 15.4	2.67 2.73	48.51	1.04
13:32	1.6	15.39	2.73	48.6 48.58	1.03 1.01
13:33	1.46	15.37	2.92	48.61	1.02
13:34	1.79	15.38	2.92	41.66	1.02
13:35	1.03	15.4	2.95	0.45	1.06
13:36	1.18	15.35	2.93	0.32	1.03
13:37	1.46	15.42	2.94	0.23	1.01
13:38	1.42	15.41	2.71	0.29	1.03
13:39	1.73	15.48	2.67	0.27	1
13:40	1.62	15.46	2.66	0.27	1.01
13:41	1.88	15.45	2.7	0.23	1.02
13:42	1.31	15.47	2.69	0.23	1.08
13:43	0.89	15.44	2.68	0.25	1.09
13:44	1.05	15.45	2.73	0.22	1.07
13:45	0.99	15.39	2.92	0.2	1.05
13:46	0.95	15.37	2.94	0.22	1.04
13:47	1.06	15.4	2.91	0.21	1.04
13:48	1.2	15.4	2.9	0.21	1.03
13:49	1.18	15.39	2.9	0.19	1.04
13:50	1.2	15.41	2.92	0.17	1.05

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13:51
            0.75
                      15.43
                                  2.78
                                             0.19
                                                         1.08
13:52
             0.8
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13:53
            1.01
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                                                         1.03
13:54
            1.01
                      15.47
                                  2.69
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                                                         1.02
13:55
            1.26
                      15.47
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                                              0.2
                                                        0.99
13:56
            1.43
                      15.47
                                  2.68
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             1.9
13:57
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13:58
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                      15.41
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13:59
            0.94
                      15.39
                                  2.92
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                                                         1.04
14:00
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                       15.4
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14:01
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                                                         0.98
14:02
             1.4
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                                  2.91
                                             0.21
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14:03
            1.51
                       15.4
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                                             0.21
                                                        0.98
14:04
            1.67
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                                  2.85
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14:05
            1.93
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                                  2.69
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14:06
            1.27
                      15.48
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                                             0.23
                                                        1.02
14:07
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                      15.47
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14:08
            1.34
                      15.45
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                                             0.23
                                                        0.99
14:09
            1.31
                      15.47
                                  2.68
                                             0.24
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14:10
            1.71
                       1.28
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14:11
            -0.01
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                       0.11
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14:14
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14:15
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                       11.9
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                                             0.09
                                                        0.01
14:16
           -0.06
                      11.93
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                                             0.24
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14:17
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                       12.3
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                                                          0.1
                                   2.6
14:18
            0.02
                       2.03
                                             0.24
                                                        0.22
14:19
           -0.14
                       0.12
                                  2.83
                                              0.2
                                                        0.01
14:20
            0.14
                       6.57
                                  2.75
                                             0.22
                                                        0.55
14:21
            0.26
                       0.27
                                  0.04
                                             0.21
                                                        9.36
14:22 Data acquisition system inadvertently shut down, then restarted. 14:22 data lost.
14:23
               0
                       0.37
                                  -0.1
                                             0.15
                                                        9.77
14:24
                                  0.01
            0.06
                       0.12
                                              0.2
                                                        9.77
14:25
            0.06
                        0.1
                                  0.02
                                             0.24
                                                        9.77
14:26
            2.45
                       2.37
                                  0.67
                                              0.2
                                                         5.4
14:27
            27.6
                       0.07
                                  0.22
                                             0.19
                                                        0.07
14:28
           29.64
                       0.03
                                  0.23
                                             0.19
                                                        0.03
14:29
           29.72
                       0.06
                                  0.22
                                              0.2
                                                        0.02
14:30
           29.69
                       0.06
                                  0.25
                                             0.19
                                                        0.02
14:31
           29.73
                       0.06
                                  0.24
                                             0.19
                                                        0.01
14:32
           19.44
                       9.73
                                     2
                                             2.25
                                                        0.69
14:33
            0.91
                      15.36
                                  2.69
                                             0.06
                                                        1.04
14:34
            0.85
                       15.4
                                   2.7
                                             0.02
                                                        1.05
14:35
            0.96
                       15.4
                                  2.71
                                              5.8
                                                        1.04
14:36
            1.13
                      15.44
                                  2.67
                                            47.91
                                                         1.03
14:37
            1.28
                      15.44
                                  2.67
                                           . 48.2
                                                         1.01
14:38
            1.34
                      15.42
                                  2.66
                                            48.38
                                                           1
14:39
             1.4
                      15.43
                                  2.77
                                            48.63
                                                         1.02
14:40
            0.85
                      15.38
                                  2.87
                                            48.78
                                                         1.05
14:41
                      15.38
            0.89
                                  2.89
                                            48.79
                                                         1.02
14:42
            0.98
                       15.4
                                   2.9
                                            23.05
                                                           1
14:43
            0.94
                      15.37
                                   2.9
                                             0.37
                                                         0.99
14:44
             1.1
                      15.38
                                  2.94
                                             0.31
                                                        0.98
```

B.2 Raw Data – Ambient Conditions

Ambient Conditions Data Summary

Date: July 18, 2000

			,	
	Time	Temp. deg F	Pressure, in. Hg	Relative humidity, %
Run 1	7:05	14.8°C 53.7°C	30. <i>0</i> 9	80.6
	7:20	14.8 592°F	30.16	79.9
	7: 30	59.2°F	30.10	79. 1
Run 1 Avg.	7:00-7:32		30. Win Ha	79.9%
Run 2	8:15	59.7	30.11+	74.5
	8:25	15.9 60.4 60.4	30.12	76.4
-	8:35 CC	16.4 61.2 61.5	30.12	75.0
Run 2 Avg.	8:10-8:42	60.5°F	30.12 m Hg	75.3%
Run 3	9:27	61.5	30.12	73.4
	9:37	17.3 225 63.1	30.12	69.1
	9:47	17.9 44.0 64.0	30.10	68.0
Run 3 Avg.	9:20-9:52	62.9°F	30.11inHg	70.2%

used thermocouple on thermohygrometer which reads in °C.

The °C was converted to °F by × 1/5 + 32. The °F values Mare from another thermocouple for checking purposes.

Crosg

Ambient Conditions Data Summary

Date: July 18, 2000

Craig Clopsedolk

	Time	Temp. deg F	Pressure, in. Hg	Relative humidity, %
Run ∜ 4	16:45	25.3° 79.1° 77.5	30.03	51.4
	16:55	25.29 77.95 77. 4	30.02	50.4
·	17:05	76.6	30.02	51.9
Run 4 Avg.	16:40-17:12	77.2°F	30.02 in the	51.2%
Run 25	17:58	75.7	30.01	49.8
.*	18:14	74.7	30.01	52.5
	18:21	73.0	30.01	53.6
Run 2 Avg.	17:50-18:22	74.5°F	30.01 m Hg	52.0%
Run 56	18:05	21.1 689 70.0	30.01	56.6
	19:20	70.9	30.01	58.6
	19:29	20.8 A.7 69.4	30.01	58./
Run Avg.	18:58-19:30	70.1°F	30,01 in Hg	57.8%

used Taglor barometer # MRI Y-2101

Ambient Conditions Data Summary

Log Classaddle Date: 7/19/00

ı	Time	Temp. deg F	Pressure, in. Hg	Relative humidity, %
Run ₹7	6:44	13.9°< 57.25 57.0	30.02	87.5
	6:53	142C 57.71 58.3	30.02	86.6
	7:07	14.7° 58.2 58.5	30.02	85./
Run Avg.	6:40-7:12	57.9°F	30.02 inHg	86.4%
Run 28	7:52	16.0 60.5 60.8	30.03	80.0
	8:07	16.0 60.5	30.03	79.0
	8:15	60.8	30.03	78.5
Run 🎖 Avg.	7:45-8:17	60.8°F	30.03 inth	79.2%
Run 39	8:57	16.4 61.8 61.5	30.03	75.5
	9:09	62.6	30.03	73.2
	9:20	17.5 63.5	30.03	70.6
Run & Avg.	8:50-9:22	62.5	30.03 mHg	73.1

Ambient Conditions Data Summary

Date: July 19, 2000 Craig Classadolle

			<u>_</u>	······
	Time	Temp. deg F	Pressure, in. Hg	Relative humidity, %
Run 10	11:28	20.8 69.4°	30.02	60.7
	11-36	69.3	30.02	628
	11:44	21-0 69-6 69.8	30.02	60.6
Run 10Avg.	11:20-11:52	69.5°F	30.02 mHg	61.4%
Run ≇ ∐	12:38	21.6 20.8 70.9	30.01	61.8
	12:46	21.4 70.6 70.5	30.01	62.1
	12:55	22.4 21.9 72.3	30.01	60.8
Run Avg.	12:30-13:02	71.2°F	30.01 in Hg	61.6%
Run \$12	13:44	73.9	30.00	54.5
	13:53	23.4 74.3 74.1	35.00	52.9
	14:04	75.D	36.00	51.6
Run Avg.	13:36-14:08	74.3	30.00 in Hg	53.0

B.3 Emission Concentration Summaries

				Emissi	ion Conc	Emission Concentration Data)ata				1	COL	corrected for O ₂	02
Job No.	101494.1.004.02	02								1600	X N		1600	Š
Client:	ccsı						8	o'	ç O	as ppmv	as ppmv	ខ	as ppmv	as ppmv
Plant:	Gianera General	erating Station	tion				ppmv	percent	percent	r, C,	NO,	ppmv	C,H,	NO,
Location:	Gas Turbine Ou	Outlet				Raw Avg.:	1.11	15.46	3.05	0.13	1.07			
Operator:	Daniel Neal					Avg. Zero:	0.05	0.08	-0.04	40.04	0.01			
Date:	18-Jul-00				U	Corr. Factor:	1.00792	1.00335	0.96940	0.99830	1.00050			
Run No.	-					Corr. Avg.:	1.10	15.43	2.99	0.17	1.07	1.19		1.15
Condition:	100					Minimum:	0.58	15.37	2.86	-0.07	1.03			
						Maximum:	1.54	15.48	3.13	0.33	1.12			
			_	RAW DATA	. ◀			COR	CORRECTED DATA	ATA				
	1				TGOC	NOX				760C	Ň			
	Time	8	o'	ပ္ပိ	as ppmv	as ppmv	8	ò	S	as ppmv	as ppmv			
	24-Hr	VMQq	percent	percent	ι. Υ	NO,	ppmv	percent	percent	τ υ	NO ₂			
	7:01	0.59	15.44	3.16	0.29		0.58	15.42	3.10	0.33	1.10	0.62		1.18
	7:02	0.92	15.42	3.17	0.24	1.07	0.91	15.40	3.11	0.28	1.07	0.98		1.14
	7:03	96.0	15.46	33	0.22	1.07	0.95	15.44	2.94	0.26	1.07	1.03		1.15
	7:04	0.93	15.49	2.94	0.21	1.05	0.92	15.47	2.88	0.25	1.05	1.00		1.14
	7:05	1.16	15.49	2.94	0.19	1.05	1.15	15.47	2.88	0.23	1.05	1.25		1.14
	7:06	1.2	15.48	2.92	0.2	1.06	1.19	15.46	2.86	0.24	1.06	1.29		1.14
	7:07	1.18	15.47	2.93	0.2	1.06	1.17	15.45	2.87	0.24	1.06	1.27		1.14
	7:08	1.38	15.49	2.94	0.18	1.07	1.38	15.47	2.88	0.22	1.07	1.49		1.16
	7:09	1.16	15.49	2.94	0.18	1.11	1.15	15.47	2.88	0.22	1.1	1.25		1.20
	7:10	0.68	15.45	3.14	0.13	1.11	0.67	15.43	3.08	0.17	1.1	0.72		1.19
	7:11	0.94	15.39	3.16	0.14	1.1	0.93	15.37	3.10	0.18	1.10	0.99		1.17
	7:12	0.95	15.43	3.19	0.12	1.09	0.94	15.41	3.13	0.16	1.09	1.01		1.17
	7:13	0.98	15.41	3.19	0.14	1.09	0.97	15.39	3.13	0.18	1.09	1.		1.16
	7:14	1.02	15.44	3.17	0.1	1.06	1.01	15.42	3.11	0.14	1.06	1.09		1.14
	7:15	1.17	15.43	3.17	0.09	1.05	1.16	15.41	3.11	0.13	1.05	1.25		1.12
	7.16	1.13	15.43	3.11	0.12	1.03	1.12	15.41	3.05	0.16	1.03	1.21		1.10
	7.17	1.43	15.48	2.99	0.13	1.04	1.43	15.46	2.93	0.17	<u>1</u> .	1.55		1.12
	7.18	1 25	15.47	2.97	0.13	1.08	1.24	15.45	2.91	0.17	1.08	1.35		1.16
	7.19	2.7	15.49	2.96	0.12	1.09	0.70	15.47	2.90	0.16	1.09	0.76		1.18
	7.20	-	15 48	2.96	0.12	1.06	1.00	15.46	2.90	0.16	1.06	1.09		1.4
	7.77	5 2	15.5	295	0.13	1.05	1.08	15.48	2.89	0.17	1.05	1.18		7.7
	12.7		15.48	2.95	0.12	1.05	1.14	15.46	2.89	0.16	1.05	1.24		1.13
	77.7	. +	15.45	3.07	0.11	1.05	1.17	15.43	3.01	0.15	1.05	1.27		1.13
	57.7	- -	15.41	3.15	0.0	1.06	1.54	15.39	3.09	0.13	1.06	1.64		1.13
	#7: / #C: /	 	15.41	3.15	0.0	1.05	1.43	15.39	3.09	0.13	1.05	1.53		1.12
	C7.7		15.47	3.15	0.11	1.07	1.52	15.40	3.09	-0.07	1.07	1.63		1.14
	7:77	- C	15.44	3.14	0.0	1.12	0.90	15.42	3.08	0.13	1.12	0.97		1.20
	17:1	800	15 44	3.17	0.0	1.1	0.88	15.42	3.11	0.13	1.1	0.95		1.19
	07:7	8 6	15.41	3.15	0.1	1.11	0.97	15.39	3.09	0.14	÷.	<u>.</u> 8		1.18
	67:7	1 2 7	15.49	2.98	0.11	1.09	1.26	15.47	2.92	0.15	1.09	1.37		1.18
	7.30	35. 1	15.49	2.95	0	1.09	1.36	15.47	2.89	0.14	1.09	1.47		1.18
	r::/ 7:37	5.1 4 L	15.49	2.93	0.11	1.07	1.40	15.47	2.87	0.15	1.07	1.52		1.16
	1	:		İ										

	NOx	as ppmv	NO ₂				1.14				٠.		;	1.13	<u> </u>	1.18	1.14	1.13	1.12	1.12	. .	1.12	E	1.16	1.16	1.12	1.12	1.12	1.17	1.18	1.12	1.	9.9	01.L	01.T	: ?	<u>.</u> :	3.5	5.10	. +	1.13
r 02	Z		Z																																						
corrected for O ₂	TGOC	as ppmv	τ°																																						
CO		8	ppmv				1.71						,	1.96 7.43	2.07	1.10	1.22	1.54	1.55	1.59	1.72	2.05	2.08	1.28	1.67	1.81	1.97	1.90	2.10	1.19	1.49	1.59	1.74	1.70	2.01	21.2	2.00	2.7	1.61	6.1	163
	NO.	as ppmv	NO,	1.07	0.04	1.00956	<u>-</u> 3	1.01	- 1.1		NOx	as ppmv	NO,	20.1	10.	1.07	1.03	1.02	1.03	1.03	1.02	1.03	90.1	1.06	1.05	1.01	1.01	1.02	1.06	1.07	1.03	1.02	1.01	1.01	1.0	7.07	80.	F !	1.07	8 5	10.
	TGOC	as ppmv	r,	0.09	-0.07	1.00281	0.16	0.12	0.20	ATA	1 60C	-	τ Έ	0.18	0.19	0.19	0.18	0.16	0.16	0.17	0.17	0.14	0.10	0.13	0.18	0.16	0.16	0.17	0.17	0.15	0.14	0.14	0.14	0.14	0.12	0.13	ct.o	0.16	0.16	0.17	0.10
		°	percent	3.03	0.05	0.99834	2.98	2.85	3.14	CORRECTED DATA		8	percent	2 85	2.86	2.86	2.87	5.83	3.06	3.09	3.09	3.11	3.10	3.09	2.86	2.90	2.90	2.88	2.87	2.96	3.14	3.12	3.12	3.12	3.12	3.13	3.02	2.83	2.89	2.90	2.30
		o'	percent	15.48	0.11	1.00968	15.52	15.47	15.58	CORR		°	percent	15.54	15.53	15.53	15.55	15.57	15.48	15.49	15.48	15.47	13.48	15.50	15.55	15.56	15.58	15.55	15.55	15.55	15.48	15.50	15.49	15.51	15.51	15.47	15.51	15.56	15.56	15.57	15.57
ata		8	ppmv	1.54	0.00	1.01150	1.56	0.99	1.96			8	ppmv	1 4 9 2	1.88	1.00	1.10	1.40	1.43	1.46	1.58	1.89	1.8.1	1.4	1.52	1.6	1.78	1.72	6. F	1.08	1.37	1.46	1.60	1.56	2 . 5	1.95	1.83	0.99	1.46	1.49	9. 4
Emission Concentration Data				Raw Avg.:	Avg. Zero:	Corr. Factor:	Corr. Avg.:	Minimum:	Maximum:		NOx	as ppmv	V O X	0.1	1.04	1.1	1.06	1.05	1.06	1.06	1.05	9. 6		1.09	1.08	1.04	1.04	1.05	G G	<u> </u>	1.06	1.05	1.04	1.04	1.04	1.05	= :	1.14	- :	1.09) O
ion Conc						O				A	TGOC	as ppmv	֓֞֞֞֞֞֞֞֝֞֝֓֞֝֞֝֓֞֝֓֞֝֞֝֓֞֝֞֝֓֞֝֞֝֓֞֝֓֞֝		0.12	0.12	0.11	0.09	0.09	0.1	0.1	70.0	60.0	0.00	0.11	0.09	0.09	6	- c	0.08	0.0	0.07	0.07	0.07	0.05	90'0	0.08	0.09	0.0	0.1	0.03
Emissi										RAW DATA		င္ပိ	percent	2.0	2.91	2.91	2.92	2.94	3.11	3.14	3.14	3.16	 	. 6.	2.91	2.95	2.95	2.93	2.92	3.01	3.19	3.17	3.17	3.17	3.17	3.18	3.07	2.94	2.94	2.95	2.95
			tion		٠							o	percent	15.5	15.49	15.49	15.51	15.53	15.44	15.45	15.44	15.43	13.44	15.46	15.51	15.52	15.54	15.51	15.49	5.51	15.44	15.46	15.45	15.47	15.47	15.43	15.47	15.52	15.52	15.53	15.53
	.02		erating Station	Outlet								8	1 75	5 6	1.86	0.99	1.09	1.38	4.	1.44	1.56	1.87	8.	5.5	5.	1.62	1.76	1.7	1.94	100	135	1.44	1.58	1.54	1.82	1.93	1.81	0.98	1.44	1.47	1.58
	101494.1.004.02	ccsi	Gianera Generat	Gas Turbine Outlet	Daniel Neal	18~Jul-00	2	100		,		Time	24-Hr 8-11	8.12	8:13	8:14	8:15	8:16	8:17	8:18	8:19	8:20	12:8	0.22 8.23	8:24	8:25	8:26	8:27	8:28	67.0 6.30	8:31	8:32	8:33	8:34	8:35	8:36	8:37	8:38	8:39	8:40	8:41
	Job No.	Client:	Plant:	Location:	Operator:	Date:	Run No.	Condition:																																	

				Emiss	ion Conc	Emission Concentration Data	Jata				1	cor	corrected for O ₂	02
Job No.	101494.1.004.02	.02								TGOC	Ň		T GOC	NO.
Client:	ccsi						ខ	ò	6	as ppmv	as ppmv	8	as ppmv	as ppmv
Plant:	Gianera Generating Station	erating St.	ation				ppmv	percent	percent	ς Έ	Š,	ppmv	ι. Υ.	NO.
Location:	Gas Turbine Ou	Outlet				Raw Avg.:	1.32	15.50	3.03	0.14	1.01			
Operator:	Daniel Neal					Avg. Zero:	9.0	0.13	0.14	-0.03	0.04			
Date:	18~Jul-00				_	Corr. Factor:	1.01339	1.00799	1.02906	1.00788	1.01827			
Run No.	8					Corr. Avg.:	1.37	15.50	2.97	0.17	0.99	1.50		1.08
Condition:	100					Minimum:	0.63	15.45	2.83	0.12	96.0			
						Maximum:	1.92	15.56	3.14	0.21	1.06			
				RAW DATA	Ι			COR	CORRECTED DATA	ATA				
	I				TG0C	, VON				TGOC	Ň			
	Time	ខ	o'	S S	as ppmv	as ppmv	8	o'	8	as ppmv	as ppmv			
	24-Hr	ррту	percent	percent	ι υ	NO,	ppmv	percent	percent	τ. C	Š V			
	9:21	1.64	15.54	2.93	0.14	-	1.70	15.54	2.87	0.17	0.98	1.87		1.08
	9:22	1.57	15.52	2.89	0.15	-	1.63	15.52	2.83	0.18	0.98	1.78		1.07
	9:23	1.78	15.54	2.92	0.13	0.99	1.84	15.54	2.86	0.16	0.97	2.02		1.06
	9:24	1.51	15.54	2.95	0.1	1.03	1.57	15.54	2.89	0.13	1.01	1.72		1.1
	9:25	0.83	15.48	3.14	0.09	1.03	0.88	15.48	3.09	0.12	1.01	0.95		1.10
	9:56	1.39	15.47	3.15	0.09	1.01	1.44	15.47	3.10	0.12	0.99	1.57		1.07
	9:27	1.4	15.45	3.17	0.12	0.99	1.45	15.45	3.12	0.15	0.97	1.57		1.05
	9:58	1.37	15.46	3.15	0.12	0.98	1.42	15.46	3.10	0.15	96.0	1.5		1.0
	9:59	1.54	15.47	3.16	0.13	-	1.60	15.47	3.11	0.16	0.98	1.73		1.06
	9:30	1.62	15.45	3.15	0.13	-	1.68	15.45	3.10	0.16	0.98	1.81		1.06
	9:31	1.86	15.49	3.09	0.14	1.03	1.92	15.49	3.04	0.17	1.01	5.09		1.10
	9:32	1.65	15.49	2.93	0.17	1.07	1.71	15.49	2.87	0.20	1.05	1.86		1.14
	9:33	0.79		2.95		1.08	0.84	15.55	2.89	0.18	1.06	0.92		1.17
	9:34	1.41	15.52	2.9		•	1.46	15.52	2.84	0.20	1.02	1.61		1.12
	9:35	1.52		2.92		1.01	1.58	15.56	2.86	0.18	0.99	1.74		1.09
	9:36	1.54	15.52	2.9		-	1.60	15.52	2.84	0.21	0.98	1.75		1.07
	9:37	1.44					1.49	15.55	2.83	0.21	0.98	1.65		1.08
	9:38	1.34	15.51				1.39	15.51	2.98	0.19	96.0	1.52		1.05
	6:36	1.56	15.48	3.16	0.12		1.62	15.48	3.11	0.15	96.0	1.76		7.0
	9.40	1.45			0.11	0.99	1.50	15.49	3.11	0.14	0.97	.		1.05
	9:41	0.59				1.04	0.63	15.46	3.11	0.15	1.02	0.69		1.10
	0.42	1.28	·		0.11	1.01	1.33	15.49	3.11	0.14	0.99	1.45		1.08
	9.43	0.98				1.01	1.03	15.45	3.11	0.17	0.99	. =		1.07
	0.44	109	Ţ			1.01	1.14	15.45	3.14	0.17	0.99	1.23		1.07
	9.45	1 17				•	1.22	15.52	2.98	0.18	1.00	<u>ਨ</u>		1.09
	0.0 0.0	7	•		0.16		1.38	15.52	2.88	0.19	1.00	1.52		1.09
	0.4.0	. t			0.16	_	1.30	15.54	2.87	0.19	1.00	1.43		1.10
٠	3.0	3. 4				_	1.66	15.54	2.88	0.17	1.00	1.82		1.10
	0. C	5 6	15.54			•	96.0	15.54	2.87	0.18	1.04	1.05		1.14
		9 6	•		0.15	1.03	0.87	15.53	2.90	0.18	1.01	0.95		1.1
	9.30	20.0		29.2	0.15	101	0.95	15.54	2.86	0.18	0.99	1.02		1.09
	9.51	2. C	- ,-	3.11	0.14	-	1.14	15.47	3.06	0.17	0.98	1.24		1.06
	7C'R	5.		;	;									

				Emissi	on Conc	Emission Concentration Data	Jata				1	COL	corrected for O ₂	27
Job No.	101494.1.004.02	03								1000	Š		1600	Š
Client:	ccsi						8	o'	8	as ppmv	as ppmv	8	as ppmv	as ppmv
Plant:	Gianera Generating Station	rating Sta	tion			!	ppmv	percent	percent	CJH,	¥O,	ppmv	ς Ή	NO ₂
Location:	Gas Turbine Outlet	Juffet				Raw Avg.:	1.07	15.40	2.86	0.15	1.00			
Operator:	Daniel Neal					Avg. Zero:	0.05	0.09	0.10	0.01	0.03			
Date:	18~Jul-00				-	Corr, Factor:	1.00100	18500.1	1.01518	0.88800	1.01313	;		;
Run No.	7					Corr. Avg.:	1.03	15.40	2.81	0.13 6.13	0.98	1.10		1.06
Condition:	8					Minimum: Maximum:	1.38	15.46	2.70	0.02	1.04			
٠				RAW DATA	⋖			COR	CORRECTED DATA	ATA				
	ı				1 000	Š				7000	ğ			
	Time	8	ó	ŝ	as ppmv	as ppmv	8	õ	ŝ	as ppmv	as ppmv			
	24-Hr	ppmv	percent	percent	C,H	Š,	DDmv	percent	percent	±°.	Š			
	16:41	0.71	15.45	2.76	0.22	1.04	0.67	15.46	2.71	0.21	1.03	0.72		1.11
	16:42	0.93	15.42	2.77	0.11	1.04	0.89	15.43	2.72	0.10	1.03	0.95		1,11
	16:43	0.98	15.42	2.75	0.12	1.02	0.94	15.43	2.70	0.11	1.01	1.01		1.09
	16:44	0.93	15.44	2.77	0.11	-	0.89	15.45	2.72	0.10	0.99	96.0		1.07
	16:45	1.17	15.43	2.81	0.19	0.98	1,13	15.44	2.78	0.18	0.97	1.22		1.04
	16:46	1.16	15.37	2.99	0.03	0.99	1.12	15.37	2.94	0.03	96.0	1.19		1.04
	16:47	0.98	15.36	3.01	0.23	0.99	96.0	15.38	2.98	0.22	0.98	1.00		1.04
	16:48	1.39	15.35	2.97	0.23	-	1.35	15.35	2.82	0.22	0.99	1.43		1.05
	16:49	1.09	15.35	2.97	0.16	1.05	1.05	15.35	2.82	0.15	1.04	1.1		1.10
	16:50	0.77	15.37	2.96	0.1	1.03	0.73	16.37	2.91	0.09	1.02	0.77		1.09
	16:51	0.9	15.38	2.99	0.13	1.02	0.86	15.36	7.84	0.12	1.01	0.91		1.07
	16:52	1.05	15.41	2.85	0.14	1.01	1.01	15.41	2.80	0.13	9.5	1.08		1.07
	16:53	0.98	15.44	2.77	0.09	1.01	0.94	15.45	2.72	0.08	1 .8	1.01		1.08
	16:54	1.1	15.4	2.77	0.23	1.01	1.06	15.40	2.72	0.22	1.00	1.13		1.07
	16:55	1.2	15.42	2.8	0.11	-	1.16	15.43	2.76	0.10	0.99	1.25		1.06
	16:56	1.42	15.43	2.81	0.17	66.0	1.38	15.44	2.76	0.16	96.0	1.49		1.06
	16:57	1.24	15.42	2.77	0.18	1.02	1.20	15.43	2.72	0.17	1.01	1.29		1.09
	16:58	0.79	15,41	2.8	0.08	1.05	0.75	15.41	2.76	0.07	1.04	0.80		1.12
	16:59	0.7	15.37	2.96	0.19	-	99'0	15.37	2.91	0.18	0.99	0.70		1.05
	17:00	96.0	15.37	2.98	0.14	96.0	0.92	15.37	2.83	0.13	0.95	0.98		1.01
	17:01	0.97	15.38	2.96	0.11	0.94	0.93	15.38	2.91	0.10	0.93	0.99		0.99
	17:02	1.26	15.35	2.96	0.14	0.94	1.22	15.35	2.91	0.13	0.93	2.3		0.99
	17:03	1.17	15.36	2.97	0.24	0.94	1.13	15.36	2.92	0.23	0.93	2.5		86.0
	17:04	1.35	15.33	က	0.15	0.94	1.31	15.33	2.95	0.1	0.93	8		88.0
	17:05	1.37	15.4	2.89	0.17	96.0	1.33	15.40	7.84	0.18	0.95	1.42		1.02
	17:06	1.08	15.41	2.78	0.13	1.02	1.04	15.41	2.73	0.12	1.01	Ξ		1.08
	17.07	96	15.4	2.77	0.16	-	0.82	15.40	2.72	0.15	0.99	0.98		8. 3
	17.08	0.99	15.41	2.77	0.16	0.98	0.95	15.41	2.72	0.15	0.97	1.02		1.04
	17:09	1.16	15.43	2.79	0.19	0.99	1.12	15.44	2.74	0.18	0.98	1.20		1.06
	17:10	1.1	15.44	2.76	0.12	0.99	1.07	15.46	2.71	T	96.0	1.15		9.7
	17.11	1.19	15.43	2.76	0.17	0.99	1.15	15.44	2.71	0.16	0.98	1.24		3
	17:12	1.24	15.38	2.97	0.19	0.98	1.20	15.38	2.92	0.18	0.97	1.28		20.
									•					

0,	ΝOχ	as ppmv	NO,				1,11							1,1	1.08	1.06	1.06	1.06	1.07	1.11	1.13	1.17	1.17	1.15	1.18	1.13	1.1	1.1	1.09	1.11	1.14	1.10	.08 .08	1.10	1.12	1.1	1.10	1.1	1.17	1.15	1.13	1.12	1.1	1.1
corrected for O ₂	TGOC	as ppmv	H.C																																									
COI		8	bpmv				1.03							0.51	0.78	0.74	0.79	0.82	0.96	0.97	1.04	0.92	0.73	0.85	0.89	1.18	1.07	1.27	1.48	1.56	0.71	0.83	1.1	1.15	1.29	1.26	1.39	1.41	0.98	0.78	0.93	1.03	1.12	,,,
•	Š	as ppmv	Š,	1.05	0.03	1.01416	1.03	96.0	1.09		Š	as ppmv	ð	1.03	7.0	0.98	0.98	0.98	0.99	1.02	1.03	1.08	1.08	1.06	1.09	1.03	1.03	1.02	1.01	1.03	1.06	1.02	1.01	1.01	1.02	1.01	1.00	1.02	1.08	1.06	1.04	1.04	1.03	•
	1000	as ppmv	ς Έ	0.15	-0.03	0.99810	0.17	90.0	0.27	ATA	100 200	as ppmv	£ 5	0.16	0.17	0.14	0.16	0.25	0.16	0.17	0.16	0.16	0,21	0.16	0.18	0.18	0.14	0.21	0.15	0.18	0.20	0.12	0.11	0.26	0.21	0.27	0.19	0.24	0.18	0.17	0.12	0.19	0.13	
		6	percent	2.90	0.03	0.98689	2.84	2.70	2.96	CORRECTED DATA		8	percent	2.90	2.93	2.95	2.91	2.91	2.91	2.85	2.74	2.73	2.72	2.72	2.74	2.70	2.88	2.90	2.93	2.93	2.93	2.93	2.87	2.75	2.70	2.70	2.70	2.72	2.72	2.87	2.92	2.95	2.94	
		ó	percent	15.39	0.12	1.01139	15.44	15.39	15.50	CORF		o'	percent	15.41	15.42	15.41	15.42	15.44	15.43	15.43	15.50	15.47	15.47	15.47	15.46	15.48	15.42	15.43	15.42	15.40	15.40	15.42	15.41	15.45	15.49	15.49	15.50	15.47	15.47	15.4	15.42	15.40	15.39	
ata		8	hpmv	0.96	0.01	1.00218	0.95	0.47	1.45			8	ppmv	0.47	0.72	0.69	0.73	0.78	0.89	0.90	0.95	0.84	0.67	0.78	0.82	1.08	0.99	1.17	1.37	1.45	99'0	0.77	1.06	1.06	1.18	1.15	1.27	1.29	0.90	0.72	98.0	96.0	70.7	
Emission Concentration Data				Raw Avg.:	Avg. Zero:	Corr. Factor:	Corr. Avg.:	Minimum:	Maximum:		ğ	as ppmv	Š,	1.05	1.02	-	-	-	1.01	104	1.05	1.09	1.09	1.07		1.05	1.05	1.04	1.03	1.05	1.08	1.04	1.03	1.03	1.04	1.03	1.02	1.04	1.09	1.08	1.06	90.	1.05	
on Conce						ŏ					100 C	as pomv	Ή. Ό	0.14	0.15	0.12	0.14	0.23	0.14	0.15	0.14	0.14	0.19	0.14	0.14	0.16	0.12	0.19	0.13	0.16	0.18	0.1	0.09	0.24	0.19	0.25	0.17	0.22	0.14	0.15	0.1	0.17	0.11	
Emissic										RAW DATA		ŝ	percent	2.96	2.99	3.01	2.97	2.97	2.97	2.91	2.8	2.79	2.78	2.78	2.8	2.76	2.94	2.96	2.99	2.99	2.99	2.99	2.93	2.81	2.76	2.76	2.76	2.78	2.78	2.93	2.98	3.01	က	
			ion									ሪ			•	•	•	•		•	•	-	•	15.42	15.41	15.43	15.37	15.38	15.37	15.35	15.35	15.37	15.36	15.4	15.44	15.44	15.45	15.42	15.42	15.39	15.37	15.35	15.34	
	05		rating Station	Outlet								8	DDMV	0.48	0.73	0.7	0.74	0.77	0.0	0.91	96.0	0.85	0.68	0.79	0.83	1.09	-	1.18	1.38	1.46	0.67	0.78	1.07	1.07	1.19	1.16	1.28	1.3	0.91	0.73	0.87	0.97	1.05	
	101494.1.004.02	ccsı	Gianera Generating	Gas Turbine Outlet	Daniel Neal	18-Jul-00	9	100		1		Time	24 Hr	17:51	17:52	17:53	17.54	17:55	17:56	17:57	17:58	17:59	18:00	18:01	18:02	18:03	18:04	18:05	18:06	18:07	18:08	18:09	18:10	18:11	18:12	18:13	18:14	18:15	18:16	18:17	18:18	18:19	18:20	
	Job No.	Client:	Plant:	Location:	Operator:	Date:	Run No.	Condition:																																				

Job No. 10	101494,1,004.02	~								1900	Š		1600	Š
	ccsi						ខ	°	6	as ppmv	as ppmv	8	Amdd se	as ppmv
Plant: Gi	Gianera Generating Station	ating Stat	ion			•	ppmv	percent	percent	C,H	Š	ppmv	Ϋ́,	Š
	Gas Turbine Outlet	ıtlet				Raw Avg.:	1.18	15.39	2.89	0.11	1.05			
<u>ت</u>	Daniel Neaf					Avg. Zero:	90.0	0.10	0.03	0.04	0.03			
	18-Jul-00					Corr. Factor:	1.00420	1.01181	1.02730	0.99621	1.01467			
MUN NO.	٥					Corr. Avg.:	1.13	15.47	2.94	0.15	1.04	1.22		1.13
Condition:	ş					Minimum:	0.64	15.41	2.81	0.01	0.99			
						Maximum:	1.84	15.53	3.08	0.21	1.1			
				RAW DATA	4			COR	CORRECTED DATA	ATA				
					TGOC	Š				2002	Š			
	Tine	ဗ	ó	င္ပိ	as ppmv	as ppmv	8	o'	8	as ppmv	as ppmv			
		∆mdd	percent	percent	τ'ς Σ	Š,	∧mdd	percent	percent	C,H	ş			
	18:59	1,12	15.34	2.99	0.1	1.03	1.06	15.42	3.05	0.14	101	1.15		1.09
	19:00	1.32	15.37	2.98	0.12	1.02	1.27	15.45	3.04	0.16	9.1	1.37		1.09
	19:01	1.09	15.37	2.98	0.13	1.02	1.03	15.45	3.05	0.17	100	1.12		5
	19:02	1.57	15.36	2.94	0.08	1.02	1.52	15.44	2.99	0.12	8	1.64		60
	19:03	1.52	15.42	2.82	0.12	1.04	1.47	15.50	2.87	0.16	1.02	1.80		1.15
	19:04	96.0	15.42	2.8	0.1	1.09	0.90	15.50	2.85	0.14	1.08	0.99		1 4
	19:05	1.28	15.41	2.76	0.17	1.1	1.23	15.49	2.81	0.21	1.09	1.34		1.18
	19:06	1.18	15.45	2.78	-0.03	1.07	1.12	15.53	2.81	0.01	1.06	1.24		1.16
	19:07	1.2	15.42	2.77	0.17	1.05	1.14	15.50	2.82	0.21	1.03	1.25		1.13
	19:08	1.29	15.42	2.78	0.11	1.02	1.24	15.50	2.83	0.15	1.00	1.35		1.10
	19:09	1.2	15.36	2.92	0.14	1.03	7.7	15,44	2.97	0.18	1.01	1.24		1.10
	19:10	1.06	15.38	2.99	0.11	1.06	1.00	15.48	3.05	0.15	1.05	1.09		1.13
	19:11	0.94	15.37	2.99	0.07	- - - - - - - -	0.88	15.45	3.05	0.11	1.05	96.0		1.13
	19:12	1.24	15.35	3.02	0.1	1.07	1.18	15.43	3.08	0.14	1 .08	1.28		1.14
	19:13	0.93	15.37	2.98	0.11	1.12	0.87	16.45	3.04	0.15	1.1	0.95		1.20
	19:14	0.7	15.37	2.97	0.09	1.08	0.64	15.45	3.03	0.13	1.07	0.70		1.15
	19:15	1.16	15.37	2.92	0.15	1.06	1.10	15.45	2.97	0.19	1.05	1.20		1.13
	19:16	0.0	15.42	2.78	0.13	1.06	0.84	15.50	2.83	0.17	1.05	0.92		1.14
	19:17	1.08	15.41	2.78	0.14	1.06	1.02	15.49	2.83	0.18	1.05	1.12		1.1
	19:18	1.13	15.43	2.77	0.12	1.06	1.07	15.51	2.82	0.16	1.05	1.18		1.1
	19:19	1.29	15.42	2.78	0.12	1.05	1.24	15.50	2.83	0.16	1.03	1.36		1.13
	19:20	1.49	15.41	2.79	0.13	10.	7.	15.49	2.84	0.17	1.02	1.57		1.12
	19:21	1.19	15.39	2.82	0.1	1.09	1.13	15.47	2.87	0.14	1.08	1.23		1.17
	19:22	0.98	15.38	2.91	0.1	1.06	0.92	15.48	2.96	0.14	1.06	1.0		1.13
	19:23	1.19	15.35	2.96	0.1	1.03	1,13	15,43	3.02	0.14	101	1.22		1.09
	19:24	1.07	15.36	2.97	0.07	1.03	1.01	15.44	3.03	0.11	1.01	1.10		1.
	19:25	1.28	15.37	က	0.11	1 04	1.23	15.45	3.08	0.15	1.02	1.33		1.1
	19:26	1.51	15.33	2.97	0.08	1.04	1.46	15.41	3.03	0.10	1.02	35.		1.1
	19:27	1.69	15.38	2.99	0.15	1.01	1.64	15.46	3.05	0.19	0.99	1.78		1.08
	19:28	1.53	15.36	2.96	0.16	1.04	1.48	15.44	3.02	0.20	1.02	9.		1.1
		900	15.42	. 2 R2	000	1 07	68 0	45.50	2 87	0	ž	8		- 15
	67.61	2	77.0	70.7	9	5	3	1	•	:	3	;		:

	NOX	6	NO ₂				1.22							1.24	1.23	1.22	1.20	1.21	1.20	1.26	1.30	1.25	1.24	1.23	1.23	1.21	1.18	1.17	1.20	1.22	1.19	1.19	1.18	1.20	0.20	1.20	1.20	1.25	1.30	1.25	1.21	1.21	1.20	1.18	1.18
	TG0C	CO as ppmv	ppmv C ₃ H ₆				1.10							0.97	0.79	1.12	1.19	1.11	1.26	1.25	0.82	1.09	1.08	1.14	1.06	1.06	1.17	1.19	95.0	0.79	76.0	1.05	0.99	0.73	1.6/	2.34	89.0	0.89	1.13	1.20	1.34	1.40	0.88	1.05
i	ŏ N	as ppmv	NO ₂	1.12	0.01	1.01983	1.14	1.10	1.20		Š	as ppmv	NO.	1.16	1.15	1.14	1.13	1.13	1.13	1.18	1.20	1.16	1.15	1.14	1.14	1.12	1.1	1.10	1.13	1.15	1.12	Ξ:	1.10	F.;	E :	1.12	1.11	1.15	1.20	1.16	1.13	1.13	1.12	1.1	. 1.
	1600	as ppmv	r, C,	0.15	-0.03	-0.		0.04	0.27	DATA	TGOC	as ppmv	τ Σ	0.19	0.20	0.18	0.24	0.24	0.14	0.21	0.16	0.27	0.22	0.20	0.19	0.17										0.21			0.14			0.10	0.04	0.21	0.20
		င္ပ	percent	2.87		<u>.</u>			3.03	CORRECTED DATA		ç S	percent	2.90	3.00				3.00	2.94	2.73	2.77	2.74	2.75	2.73																3.02	2.99	2.98	2.98	3.01
		oʻ	percent	15.35	0.05	7			15.45	COR		°	percent	15.37	15.38	15.37	15.34	15.36	15.35	15.37	15.43	15.43		•		•							-									15.39	15.38	15.36	15.36
		ខ	ppmv	1.01	-0.01	1.00168	1.02	0.53	2.16			ខ	ppmv	0.91	0.74	1.05	1.12	1.04	1.18	1.17	0.76	1.01	1.00	1.06	0.99	1.03	0.99	1.10	1.12	0.53	0.74	0.90	0.98	0.92	0.69	1.55	2.16	0.63	0.82	1.05	1.12	1.25	1.31	0.82	0.98
				Raw Avg.:	Avg. Zero:	Corr. Factor:	Corr. Avg.:	Minimum:	Maximum:		NOx	as ppmv	NO,	1.15	1.14	1.13	1.12	1.12	1.12	1.17	1.19	1.15	1.14	1.13	1.13	1.1	Ξ:	1.09	1.12	1.14	1.1	Ξ.	1.09	- ;	- :	111	- .	1.14	1.19	1.15	1.12	1.12	1.11	1.1	7
Emission Concentration Data						O					TGOC	as ppmv	τ υ	0.16	0.17	0.15	0.21	0.21	0.11	0.18	0.13	0.24	0.19	0.17	0.16	0.14	0.16	0.18	0.09	0.15	0.08	0.15	0.17	0.1	0.14	0.18	0.16	0.14	0.11	0.12	0.21	0.07	0.01	0.18	0.17
SEL					•					RAW DATA		8	percent			2.97																2.96						2.73							2.98
			tation									ő				_			_		•		•	_	•				_			15.35				_			_			•	·		_
	04.02		Glanera Generating Station	ne Outlet				_				8	bbmv p							1.16	_		0.99		0.98																				0.97
	101494.1.004.02	CCSI	Glanera Ge	Gas Turbine Outle	Daniel Neal	19-Jul-00	7	100				Time	24-Hr	6:41	6:42	6:43	6:44	6:45	6:46	6:47	6:48	6:49	6:50	6:51	6:52	6:53	6:54	6:55	6:56	6:57	6:58	6:29	7:00	7:01	7:02	7:03	7:04	7:05	7:06	7.07	7.08	7:09	7:10	7.11	7:12
	Job No.	Client:	Plant:	Location:	Operator:	Date:	Run No.	Condition:																																					

Park		ş		Emiss	ion Conc	Emission Concentration Data)ata				٩	COL	corrected for O2	50	
Part		70.					. 6		ç		Š	ć	000	ž	
Part		;					8	o'	S S		as ppmv	8	as ppmv	as ppmv	
Name	ĕ	erating St	ation			,	ppmv	percent	percent	H.S	NO ₂	ppmv	H.	NO ₂	
CONT. Avg. 2	₾.	Outlet				Raw Avg.:	0.96	15.38	2.86	0.10	1.08				
Corr. About Abou	=				•	Avg. Zero:	1 00524	0.10	0.06	-0.03	0.03				
National Column					,	Corr. Ava.:	0.95	15.40	2.81	0.13	1.09	1.02		1 17	
COMPACTAL LANDATA TOTAL LANDATA CORRECTED DATA CORRE	le					Minimum:	0.56	15.35	2.64	0.01	1.05	2		•	
CO O, O CO C						Maximum:	1.29	15.45	2.95	0.19	1.15				
CO O ₁ CO ₁ Sppmv CO ₁ TGOC NO ₂ Ppmv percent Col. seppmv seppmv seppmv seppmv Ppmv percent Col. Col. Col. Col. 100 1.71 1.1 1538 2.73 0.16 1.08 1.09 1.40 2.68 0.19 1.10 1.17 1.26 1536 2.96 0.1 1.13 0.88 15.33 2.96 0.11 1.13 0.88 15.35 2.91 0.10 1.17 0.10 1.17 0.10 1.17 0.10 1.17 0.10 1.17 0.10 1.17 0.10 1.17 0.10 1.17 0.10 1.17 0.10 1.17 0.10 1.17 1.10 0.11 1.10 0.10 1.11 1.00 0.12 1.10 0.12 1.10 0.10 1.11 1.10 0.11 1.10 0.12 1.10 0.12 1.10 0.12				RAW DAT	Ā			COR	RECTED D	ATA					
CO O ₁ CO ₁ as ppmw CO O ₂ CO ₁ as ppmw sep pmw Pum percent percent C ₁ NO ppmv percent C ₁ NO 1.17 NO ppmv percent C ₁ NO 1.17 NO 1.18 1.23 1.26 1.23 0.70 1.08 1.23 2.85 0.10 1.17	•				TGOC	NO.				TGOC	Š				
ppm/m ppm/m <th< td=""><td></td><td>8</td><td>o</td><td>o O</td><td>as ppmv</td><td></td><td>8</td><td>o'</td><td>co co</td><td>as ppmv</td><td>as ppmv</td><td></td><td></td><td></td><td></td></th<>		8	o	o O	as ppmv		8	o'	co co	as ppmv	as ppmv				
1, 1, 15, 38 2, 73 0.15 1.08 1.08 15, 40 2.68 0.19 1.10 1.17 1, 15, 38 2, 24 0.15 1.08 1.08 1.54 2.88 0.10 1.10 1.13 1, 15, 38 2.99 0.07 1.08 1.14 15, 38 2.91 0.14 1.12 0.13 1, 15, 38 2.96 0.11 1.13 0.08 15, 37 2.90 0.14 1.12 0.13 1, 15, 38 2.96 0.11 1.08 0.08 15, 37 2.90 0.14 1.10 0.91 1, 15, 38 2.95 0.11 1.08 0.08 15, 37 2.90 0.14 1.10 0.91 1, 15, 38 2.96 0.11 1.08 0.08 15, 37 2.90 0.14 1.10 0.91 1, 15, 41 2.72 0.12 1.09 1.04 15, 42 2.67 0.15 1.10 0.91 1, 15, 42 2.74 0.13 1.11 1.26 15, 42 2.69 0.18 1.11 1.14 1, 17 15, 42 2.74 0.13 1.11 1.26 15, 42 2.69 0.16 1.11 1.14 1, 17 15, 42 2.77 0.13 0.19 1.13 1.14 2.82 0.15 1.10 0.95 1, 10 15, 34 2.97 0.09 1.03 15, 41 2.82 0.07 1.07 0.95 1, 10 15, 34 2.97 0.09 1.03 1.08 15, 38 2.92 0.15 1.15 1, 10 15, 34 2.97 0.09 1.03 1.08 15, 38 2.92 0.12 1.05 1.05 1, 15 15, 34 2.97 0.09 1.00 1.07 1.00 0.95 1.34 1.00 0.10 1.11 1.00 1, 15 15, 34 2.97 0.09 1.00 1.07 1.04 1.54 2.80 0.14 1.10 0.95 1, 15 15, 34 2.97 0.09 1.00 0.05 1.54 2.80 0.15 1.10 0.95 1.10 1, 15 15, 34 2.95 0.07 1.09 0.95 1.54 2.80 0.14 1.10 0.95 1.10 1, 16 15, 35 2.95 0.11 1.07 0.94 15, 42 2.80 0.14 1.09 1.02 1.05	,	vmdd	percent	percent	χ. S	ž	hpmv	percent	percent	Ή. Ú	NO,				
126 1535 2.9 0.07 1,06 1,25 15.37 2.86 0.10 1,08 1,34 1.34 1.34 1.34 1.34 1.34 1.34 1.34 1.34 1.34 1.34 1.34 1.34 0.07 1.08 1.14 1.13 0.08 1.535 2.94 0.14 1.12 0.08 1.33 2.96 0.11 1.13 0.08 1.535 2.94 0.14 1.12 0.89 1.08 0.08 1.537 2.90 0.14 1.10 0.09 1.08 1.08 1.08 1.09 1.08 1.08 1.09 1.09 1.08 1.09 1.09 1.01 1.09 1.09 1.04 1.11 1.10 0.09 1.08 1.09 1.04 1.14 1.10 0.09 1.08 1.04 1.14 1.10 1.04 1.12 1.09 0.09 1.08 1.23 2.81 0.04 1.09 0.09 1.03 1.04 1.14 1.10 <	ي	- :	15.38	2.73	0.16		1.09	15.40	2.68	0.19	1.10	1.17		1.18	
1,15 15,36 2.97 0.07 1,08 1,14 15,38 2.97 0.10 1,12 0.88 15,35 2.94 0.11 1,13 0.88 15,35 2.94 0.11 1,13 0.88 15,37 2.99 0.14 1,12 0.89 1.83 2.99 0.14 1,10 0.89 1.83 2.89 0.14 1,10 0.89 1.13 0.89 1.83 2.89 0.14 1,10 0.89 1.00 1.83 2.89 0.14 1,10 0.89 1.00 1.83 2.89 0.14 1,10 0.89 1.00 1.00 1.00 0.14 1,10 0.89 1.00 0.14 1,10 0.89 1.10 0.14 1,10 0.89 1.10 0.14 1,10 0.99 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	4	1.26	15.35	2.9	0.07	_	1.25	15.37	2.85	0.10	1.08	1.34		1.15	
0.87 15.33 2.96 0.1 1.13 0.86 15.35 2.96 0.11 1.13 0.86 15.35 2.96 0.11 1.13 0.88 15.35 2.99 0.14 1.10 0.88 1.93 0.14 1.10 0.98 1.12 0.99 1.14 1.10 0.91 1.00 0.98 1.53 2.99 0.14 1.00 0.98 1.53 2.99 0.14 1.10 0.99 1.00 1.53 2.99 0.14 1.10 0.94 1.00 1.00 1.00 0.14 1.10 0.94 1.00 1.00 1.00 0.14 1.10 0.04 1.10 0.04 1.10 0.04 1.10 0.04 1.10	7:48	1.15	15.36	2.97	0.07	_	1.14	15.38	2.92	0.10	1.10	1.22		1.17	
081 1533 2.96 0.11 1.1 0.80 15.37 2.91 0.14 1.10 0.89 0.89 1.535 2.95 0.01 1.08 0.85 15.37 2.90 0.14 1.10 0.94 1.01 15.36 2.93 0.01 1.08 0.08 15.37 2.90 0.014 1.10 0.03 1.02 15.41 2.72 0.11 1.08 1.00 1.53 2.88 0.14 1.10 0.03 1.02 15.41 2.72 0.13 1.09 1.04 15.42 2.87 0.14 1.10 0.03 1.22 15.42 2.74 0.13 1.13 0.58 1.54 2.89 0.14 1.11 1.14 1.22 15.42 2.74 0.13 1.13 0.58 15.41 2.79 0.14 1.10 0.13 1.11 1.14 1.24 1.54 2.72 0.13 1.13 0.58 15.42	7:49	0.87	15.33	2.96	0.1	1.13	0.86	15.35	2.91	0.13	1.15	0.91		1.22	
0.86 15.35 2.95 0.11 1.08 0.85 15.37 2.90 0.14 1.10 0.94 0.89 15.35 2.95 0.01 1.08 1.08 1.03 2.89 0.14 1.10 0.94 1.05 15.41 2.72 0.12 1.09 1.04 15.43 2.87 0.14 1.11 1.17 1.17 1.17 1.17 1.17 1.17 1.12 1.14 1.12 1.14	7:50	0.81	15.33	2.96	0.11	1.	08'0	15.35	2.91	0.14	1.12	0.85		1.19	
0.89 15.35 2.95 0.09 1.08 15.37 2.90 0.12 1.10 0.94 1.01 15.38 2.88 0.14 1.10 1.08 1.08 1.09 1.04 1.09 1.04 1.09 1.04 1.09 1.04 1.09 1.04 1.09 1.04 1.09 1.04 1.09 1.04 1.09 1.04 1.09 1.04 1.09 1.04 1.09 1.04 1.11 1.10 1.07 1.07 1.07 1.00 1.07 1.00 1.07 1.01 1.09 1.04 1.04 1.07 1.07 1.07 1.07 1.07 1.07 1.07 1.07 1.07 1.07 1.07 1.07 1.07 1.08 1.08 1.08 1.08 1.08 1.08 1.04 1.11 1.11 1.11 1.11 1.11 1.11 1.11 1.11 1.11 1.11 1.11 1.11 1.11 1.11 1.11 1.11 1.11 <td< td=""><td>7:51</td><td>0.86</td><td>15.35</td><td>2.95</td><td>0.11</td><td>1.08</td><td>0.85</td><td>15.37</td><td>2.90</td><td>0.14</td><td>1.10</td><td>0.91</td><td></td><td>1.17</td><td></td></td<>	7:51	0.86	15.35	2.95	0.11	1.08	0.85	15.37	2.90	0.14	1.10	0.91		1.17	
101 15.36 2.93 0.11 1.08 1.00 15.38 2.88 0.14 1.10 1.07 1.05 15.41 2.72 0.12 1.09 1.04 15.42 2.67 0.15 1.11 1.12 1.07 15.4 2.76 0.15 1.09 1.21 15.42 2.69 0.18 1.11 1.14 1.27 15.4 2.74 0.15 1.09 1.21 1.26 1.54 2.69 0.18 1.11 1.14 1.27 15.4 2.74 0.13 1.11 1.26 15.42 2.69 0.16 1.12 1.14 0.59 15.39 2.77 0.01 1.03 0.58 15.44 2.69 0.16 1.11 1.09 0.94 15.39 2.97 0.04 1.05 0.89 15.36 2.92 0.15 1.09 0.94 15.34 2.98 0.07 1.05 0.89 15.36 2.92 0.15	7:52	0.89	15.35	2.95	0.09	1.08	0.88	15.37	2.90	0.12	1.10	0.94		1.17	
1.05 15.41 2.72 0.12 1.09 1.04 15.43 2.67 0.15 1.11 1.12 1.07 15.4 2.75 0.11 1.09 1.06 15.42 2.70 0.13 1.11 1.14 1.27 15.4 2.74 0.15 1.09 1.06 15.42 2.79 0.13 1.11 1.30 1.29 15.39 2.73 0.11 1.13 0.58 15.41 2.69 0.13 1.15 0.58 1.54 2.69 0.16 1.11 0.92 0.86 15.32 2.77 0.13 1.09 0.85 15.41 2.87 0.07 1.01 0.93 15.41 2.87 0.07 1.00 0.93 15.34 2.87 0.07 1.00 0.93 15.34 2.87 0.07 1.00 0.93 15.34 2.82 0.07 1.00 0.93 15.34 2.82 0.07 1.00 0.93 15.34 2.82 0.07 <	7:53	1.01	15.36	2.93	0.1	1.08	1.00	15.38	2.88	0.14	1.10	1.07		1.17	
1,07 15.4 2.75 0.1 1,09 1,06 15.42 2.70 0,13 1,14 1,14 1,22 15.4 2.74 0,15 1,09 1,21 15.42 2.69 0,18 1,11 1,30 1,27 15.4 2.74 0,15 1,09 1,21 15.42 2.69 0,18 1,11 1,30 0.59 15.39 2.73 0,13 1,09 0.85 15.44 2.69 0,16 1,11 0,92 0.94 15.39 2.87 0.04 1.05 0.93 15.41 2.87 0,07 1,07 1,00 0.94 15.36 2.97 0.04 1.05 0.93 15.42 2.92 0,17 1,00 0.94 15.36 2.97 0.09 1.03 1.02 15.36 2.92 0,17 1,00 1.03 15.34 2.97 0.12 1.03 1.03 1.14 1,19 0.92 1.03	7:54	1.05	15.41	2.72	0.12	1.09	1.04	15,43	2.67	0.15	1.1	1.12		1.20	
1.22 15.4 2.74 0.15 1.09 1.21 15.42 2.69 0.18 1.11 1.30 1.27 15.4 2.74 0.13 1.1 1.26 15.42 2.69 0.16 1.11 1.30 0.59 15.39 2.73 0.13 1.09 0.58 15.44 2.67 0.04 1.11 0.92 0.94 15.39 2.87 0.04 1.05 0.89 15.34 2.97 0.07 1.09 0.93 15.44 2.87 0.04 1.05 0.89 15.36 2.92 0.07 1.01 0.92 0.94 15.35 2.97 0.09 1.03 1.02 1.03 1.0	35	1.07	15.4	2.75	0.1	1.09	1.06	15.42	2.70	0.13	1.1	1.14		1.19	
1.27 15.4 2.74 0.13 1.1 1.26 15.42 2.69 0.16 1.12 1.36 0.59 15.39 2.73 0.1 1.13 0.58 15.41 2.68 0.14 1.15 0.62 0.86 15.39 2.72 0.13 1.09 0.85 15.41 2.68 0.15 1.15 0.62 0.94 15.39 2.87 0.04 1.05 0.83 15.34 2.87 0.17 1.00 0.94 15.36 2.97 0.09 1.04 0.93 15.37 2.92 0.12 1.09 1.03 15.36 2.97 0.09 1.03 1.02 1.03 1.03 1.03 1.09 1.03 15.36 2.97 0.09 1.03 1.02 1.03 1.03 1.03 1.03 1.04 1.53 2.97 0.09 1.04 1.14 1.05 0.12 1.09 1.03 1.03 1.13 1.03	92	1.22		2.74	0.15	1.09	1.21	15.42	2.69	0.18	1.1	1.30		1.19	
0.59 15.39 2.73 0.1 1.13 0.58 15.41 2.68 0.13 1.15 0.62 0.86 15.42 2.72 0.13 1.09 0.85 15.44 2.67 0.16 1.11 0.92 0.94 15.39 2.87 0.04 1.05 0.89 15.34 2.97 0.07 1.07 1.00 0.94 15.36 2.97 0.09 1.04 0.93 15.36 2.92 0.01 1.00 0.94 15.36 2.97 0.09 1.03 1.02 1.03 1.13 1.03 1.0	7:57	1.27		2.74	0.13	Ξ:	1.26	15.42	2.69	0.16	1.12	1.36		1.21	
0.86 15.42 2.72 0.13 1.09 0.85 15.44 2.67 0.16 1.11 0.92 0.94 15.39 2.87 0.04 1.05 0.93 15.41 2.82 0.07 1.07 1.00 0.94 15.36 2.97 0.12 1.05 0.89 15.36 2.92 0.45 1.07 1.00 0.94 15.36 2.97 0.09 1.03 1.03 1.53 2.92 0.45 1.07 0.99 1.03 15.36 2.97 0.09 1.03 1.08 1.33 2.92 0.45 1.05 1.09 1.05 1.53 2.95 0.07 1.09 0.67 1.34 1.05 1.05 1.05 0.68 15.35 2.95 0.07 1.09 0.67 1.53 2.92 0.14 1.06 1.15 0.75 15.4 2.74 0.13 1.08 0.74 15.42 2.69 0.14 1.09	7:58	0.59		2.73	0.1	1.13	0.58	15.41	2.68	0.13	1.15	0.62		1.24	
0.94 15.39 2.87 0.04 1.05 0.93 15.41 2.82 0.07 1.07 1.00 0.94 15.34 2.97 0.12 1.05 0.89 15.36 2.92 0.15 1.07 0.95 0.94 15.35 2.97 0.09 1.04 0.83 15.37 2.92 0.15 1.06 0.99 1.03 15.36 2.97 0.09 1.03 1.08 1.53 2.92 0.15 1.09 0.99 1.15 1.53 2.95 0.07 1.09 1.04 1.14 15.36 2.92 0.15 1.15 0.75 1.54 2.99 0.07 1.09 0.67 1.53 2.94 0.11 0.71 1.06 0.74 1.53 2.94 0.11 0.71 1.07 0.88 15.42 2.89 0.14 1.09 0.95 0.89 15.42 2.74 0.13 1.07 0.98 15.45 2.69 0.14 </td <td>7:59</td> <td>0.86</td> <td></td> <td>2.72</td> <td>0.13</td> <td>1.09</td> <td>0.85</td> <td>15.44</td> <td>2.67</td> <td>0.16</td> <td>1.1</td> <td>0.92</td> <td></td> <td>1.20</td> <td></td>	7:59	0.86		2.72	0.13	1.09	0.85	15.44	2.67	0.16	1.1	0.92		1.20	
0.9 15.34 2.97 0.12 1.05 0.89 15.36 2.92 0.15 1.07 0.95 0.94 15.35 2.97 0.09 1.04 0.93 15.37 2.92 0.15 1.06 0.99 1.03 15.36 2.97 0.09 1.03 1.02 15.37 2.92 0.15 1.06 0.99 1.03 15.34 2.99 0.08 1.04 1.14 15.36 2.94 0.11 1.06 1.22 0.65 15.34 2.95 0.07 1.09 0.67 15.37 2.99 0.14 1.06 1.22 0.89 15.42 2.74 0.13 1.08 0.74 15.42 2.69 0.14 1.09 0.95 0.96 15.42 2.74 0.11 1.07 0.94 15.45 2.69 0.14 1.09 0.95 0.96 15.43 2.74 0.1 1.07 0.94 15.45 2.69 0.14 </td <td>8:00</td> <td>0.94</td> <td>15.39</td> <td>2.87</td> <td>0.04</td> <td>1.05</td> <td>0.93</td> <td>15.41</td> <td>2.82</td> <td>0.07</td> <td>1.07</td> <td>1.00</td> <td></td> <td>1.15</td> <td></td>	8:00	0.94	15.39	2.87	0.04	1.05	0.93	15.41	2.82	0.07	1.07	1.00		1.15	
0.94 15.35 2.87 0.09 1.04 0.93 15.37 2.92 0.12 1.06 0.99 1.03 15.36 2.97 0.09 1.03 1.02 15.38 2.92 0.12 1.06 0.99 1.09 15.34 2.97 0.09 1.03 1.08 15.36 2.92 0.17 1.09 1.15 0.68 15.34 2.99 0.00 1.04 1.14 15.36 2.94 0.11 1.06 1.22 0.78 15.34 2.79 0.07 1.09 0.74 15.37 2.90 0.11 1.07 0.88 15.44 2.69 0.14 1.09 0.74 1.09 0.95 0.95 1.64 1.09 0.95 0.14 1.09 0.99 0.99 0.99 1.545 2.69 0.14 1.09 0.95 0.95 1.545 2.69 0.14 1.09 0.95 0.95 1.545 2.69 0.14 1.09 0.95 <	8:01	0.9	15.34	2.97	0.12	1.05	0.89	15.36	2.92	0.15	1.07	0.95		1.14	
1,03 15,36 2,97 0.09 1,03 1,02 15,38 2,92 0.12 1,09 1,09 15,34 2,97 0.12 1,03 1,08 15,36 2,92 0.15 1,05 1,15 1,15 15,34 2,99 0.08 1,04 1,14 15,36 2,94 0,11 1,06 1,22 0,68 15,34 2,95 0.07 1,09 0,67 15,37 2,90 0,10 1,11 0,71 0,89 15,42 2,73 0,11 1,07 0,88 15,45 2,69 0,16 1,10 0,80 0,96 15,43 2,74 0,11 1,07 0,88 15,45 2,69 0,14 1,09 0,95 0,96 15,43 2,74 0,1 1,07 0,94 15,45 2,69 0,14 1,09 0,95 0,98 15,43 2,7 0,13 1,07 0,94 15,45 2,69 0,14 1,09 </td <td>8:02</td> <td>0.94</td> <td>15.35</td> <td>2.97</td> <td>0.09</td> <td>1.04</td> <td>0.93</td> <td>15.37</td> <td>2.92</td> <td>0.12</td> <td>1.06</td> <td>0.99</td> <td></td> <td>1.13</td> <td></td>	8:02	0.94	15.35	2.97	0.09	1.04	0.93	15.37	2.92	0.12	1.06	0.99		1.13	
1.09 15.34 2.97 0.12 1.03 1.08 15.36 2.92 0.15 1.05 1.15 1.15 15.34 2.99 0.08 1.04 1.14 15.36 2.94 0.11 1.06 1.22 0.68 15.35 2.99 0.08 1.04 1.14 15.36 2.94 0.11 1.06 1.22 0.75 15.42 2.74 0.13 1.08 0.74 1.54 2.69 0.16 1.10 0.80 0.96 15.43 2.74 0.11 1.07 0.88 15.44 2.68 0.14 1.09 0.95 0.96 15.43 2.74 0.11 1.07 0.94 15.45 2.69 0.13 1.07 0.94 15.45 2.69 0.13 1.07 0.94 15.45 2.69 0.14 1.09 1.02 1.05 15.43 2.74 0.13 1.07 1.04 15.44 2.64 0.16 1.09 1.	8:03	1.03	15.36	2.97	0.09	1.03	1.02	15.38	2.92	0.12	1.05	1.09		1.12	٠
1.15 15.34 2.99 0.08 1.04 1.14 15.36 2.94 0.11 1.06 1.22 0.68 15.35 2.95 0.07 1.09 0.67 15.37 2.90 0.01 1.11 0.71 0.68 15.34 2.74 0.13 1.08 0.74 15.42 2.69 0.16 1.10 0.80 0.96 15.43 2.74 0.11 1.07 0.98 15.44 2.68 0.14 1.09 0.95 0.95 15.43 2.74 0.11 1.07 0.94 15.45 2.69 0.13 1.07 0.94 15.45 2.69 0.13 1.07 0.97 15.45 2.69 0.13 1.07 0.97 15.44 2.64 0.16 1.09 1.05 1.05 15.42 2.69 0.13 1.07 1.04 15.44 2.64 0.16 1.09 1.05 1.05 1.05 0.10 1.07 1.04 15	8:04	1.09	15.34	2.97	0.12	1.03	1.08	15.36	2.92	0.15	1.05	1.15		1.1	
0.68 15.35 2.95 0.07 1.09 0.67 15.37 2.90 0.10 1.11 0.71 0.75 15.4 2.74 0.13 1.08 0.74 15.42 2.69 0.16 1.10 0.80 0.89 15.42 2.73 0.11 1.07 0.88 15.43 2.69 0.14 1.09 0.95 0.96 15.43 2.71 0.09 1.06 0.95 15.45 2.66 0.12 1.03 0.98 15.43 2.74 0.1 1.07 0.94 15.45 2.66 0.13 1.02 0.98 15.43 2.74 0.1 1.07 0.97 15.45 2.65 0.16 1.09 1.02 1.05 1.54 2.64 0.16 1.09 1.05 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 <td>8:05</td> <td>1.15</td> <td>15.34</td> <td>2.99</td> <td>0.08</td> <td>1.04</td> <td>1.14</td> <td>15.36</td> <td>2.94</td> <td>0.11</td> <td>1.06</td> <td>1.22</td> <td></td> <td>1.13</td> <td></td>	8:05	1.15	15.34	2.99	0.08	1.04	1.14	15.36	2.94	0.11	1.06	1.22		1.13	
0.75 15.4 2.74 0.13 1.08 0.74 15.42 2.69 0.16 1.10 0.80 0.89 15.42 2.73 0.11 1.07 0.88 15.44 2.68 0.14 1.09 0.95 0.96 15.43 2.71 0.09 1.06 0.95 15.45 2.66 0.12 1.03 0.98 15.43 2.74 0.1 1.07 0.94 15.45 2.69 0.13 1.07 0.97 15.45 2.65 0.16 1.09 1.05 1.05 15.42 2.69 0.13 1.07 1.04 1.54 2.64 0.16 1.09 1.12 1.16 15.35 2.95 0.12 1.07 1.15 15.37 2.90 0.14 1.09 1.39 1.16 15.35 2.95 0.11 1.11 0.56 1.53 2.95 0.11 1.11 0.56 1.53 2.95 0.13 1.30 0.74 1.09 </td <td>8:06</td> <td>0.68</td> <td>15.35</td> <td>2.95</td> <td>0.07</td> <td>1.09</td> <td>0.67</td> <td>15.37</td> <td>2.90</td> <td>0.10</td> <td>1.1</td> <td>0.71</td> <td></td> <td>1.18</td> <td></td>	8:06	0.68	15.35	2.95	0.07	1.09	0.67	15.37	2.90	0.10	1.1	0.71		1.18	
0.89 15.42 2.73 0.11 1.07 0.88 15.44 2.68 0.14 1.09 0.95 0.96 15.43 2.71 0.09 1.06 0.95 15.45 2.66 0.12 1.08 1.03 0.95 15.43 2.74 0.1 1.07 0.94 15.45 2.69 0.13 1.02 0.98 15.43 2.74 0.1 1.07 0.97 15.45 2.65 0.16 1.09 1.05 1.05 15.42 2.69 0.13 1.07 1.04 15.44 2.64 0.16 1.09 1.12 1.3 15.41 2.75 0.12 1.07 1.29 15.43 2.70 0.15 1.05 1.12 1.16 15.35 2.95 0.11 1.07 1.15 15.37 2.90 0.14 1.09 1.23 0.73 15.37 2.98 0.13 1.07 0.72 15.39 2.93 0.16 1.09 <td>8:07</td> <td>0.75</td> <td>15.4</td> <td>2.74</td> <td>0.13</td> <td>1.08</td> <td>0.74</td> <td>15.42</td> <td>2.69</td> <td>0.16</td> <td>1.10</td> <td>0.80</td> <td></td> <td>1.18</td> <td></td>	8:07	0.75	15.4	2.74	0.13	1.08	0.74	15.42	2.69	0.16	1.10	0.80		1.18	
0.96 15.43 2.71 0.09 1.06 0.95 15.45 2.66 0.12 1.08 1.03 0.95 15.43 2.74 0.1 1.07 0.94 15.45 2.69 0.13 1.02 1.02 0.98 15.43 2.7 0.13 1.07 0.97 15.45 2.65 0.16 1.09 1.05 1.05 15.42 2.69 0.13 1.07 1.04 15.44 2.64 0.16 1.09 1.12 1.3 15.41 2.75 0.12 1.07 1.29 15.43 2.70 0.15 1.05 1.16 15.35 2.95 0.11 1.07 1.15 15.37 2.90 0.14 1.09 1.23 0.73 15.37 2.98 0.13 1.07 0.72 15.39 2.93 0.16 1.09 0.77 0.75 15.38 2.98 0.01 1.07 0.72 15.40 2.93 0.01 1.07 <td>80:8</td> <td>0.89</td> <td>15.42</td> <td>2.73</td> <td>0.11</td> <td>1.07</td> <td>0.88</td> <td>15.44</td> <td>2.68</td> <td>0.14</td> <td>1.09</td> <td>0.95</td> <td></td> <td>1.18</td> <td></td>	80:8	0.89	15.42	2.73	0.11	1.07	0.88	15.44	2.68	0.14	1.09	0.95		1.18	
0.95 15.43 2.74 0.1 1.07 0.94 15.45 2.69 0.13 1.02 1.02 0.98 15.43 2.7 0.13 1.07 0.97 15.45 2.65 0.16 1.09 1.05 1.05 15.42 2.69 0.13 1.07 1.04 15.44 2.64 0.16 1.09 1.12 1.3 15.41 2.75 0.12 1.07 1.29 15.37 2.90 0.15 1.09 1.39 1.16 15.36 2.95 0.11 1.07 1.15 1.53 2.90 0.14 1.09 1.23 0.57 15.36 2.93 0.14 1.01 0.75 15.38 2.95 0.13 1.07 0.72 0.75 15.38 2.98 0.01 1.07 0.72 15.39 2.93 0.01 1.07 0.79	8:09	96.0	15.43	2.71	0.09	1.06	0.95	15,45	2.66	0.12	1.08	1.03		1.17	
0.98 15.43 2.7 0.13 1.07 0.97 15.45 2.65 0.16 1.09 1.05 1.05 15.42 2.69 0.13 1.07 1.04 15.44 2.64 0.16 1.09 1.12 1.3 15.41 2.75 0.12 1.07 1.29 15.33 2.70 0.15 1.09 1.12 1.16 15.35 2.95 0.11 1.07 1.15 1.53 2.90 0.14 1.09 1.23 0.57 15.36 2.9 0.13 1.11 0.56 15.38 2.95 0.13 1.13 0.60 0.75 15.38 2.9 0.13 1.07 0.72 15.9 2.93 0.01 1.09 0.77	8:10	0.95	15.43	2.74	0.1	1.07	0.94	15.45	2.69	0.13	1.09	1.02		1.18	
1.05 15.42 2.69 0.13 1.07 1.04 15.44 2.64 0.16 1.09 1.12 1.3 15.41 2.75 0.12 1.07 1.29 15.43 2.70 0.15 1.09 1.39 1.16 15.35 2.95 0.11 1.07 1.15 15.37 2.90 0.14 1.09 1.23 0.57 15.36 3 0.1 1.11 0.56 15.38 2.95 0.13 1.13 0.60 0.73 15.37 2.98 0.13 1.07 0.72 15.39 2.93 0.16 1.09 0.77 0.75 15.38 2.98 -0.02 1.05 0.74 15.40 2.93 0.01 1.07 0.79	8:11	0.98	15.43	2.7	0.13	1.07	0.97	15.45	2.65	0.16	1.09	1.05		1.18	
1,3 15,41 2,75 0.12 1.07 1.29 15,43 2,70 0.15 1.09 1.39 1,16 15,35 2,95 0.11 1.07 1.15 15,37 2,90 0.14 1.09 1.23 0,57 15,36 3 0.1 1,11 0.56 15,38 2,95 0.13 1,13 0.60 0,73 15,37 2,98 0.03 1,07 0.72 15,39 2,93 0.16 1,09 0.77 0,75 15,38 2,98 -0.02 1,05 0.74 15,40 2,93 0.01 1,07 0.79	8:12	1.05	15.42	2.69	0.13	1.07	1.04	15.44	2.64	0.16	1.09	1.12		1.18	
1.16 15.35 2.95 0.11 1.07 1.15 15.37 2.90 0.14 1.09 1.23 0.57 15.36 3 0.1 1.11 0.56 15.38 2.95 0.13 1.13 0.60 0.73 15.37 2.98 0.13 1.07 0.72 15.39 2.93 0.16 1.09 0.77 0.75 15.38 2.98 -0.02 1.05 0.74 15.40 2.93 0.01 1.07 0.79	8:13	13	15.41	2.75	0.12	1.07	1.29	15.43	2.70	0.15	1.09	1.39		1.17	
0.57 15.36 3 0.1 1.11 0.56 15.38 2.95 0.13 1.13 0.60 0.73 15.37 2.98 0.13 1.07 0.72 15.39 2.93 0.16 1.09 0.77 0.75 15.38 2.98 -0.02 1.05 0.74 15.40 2.93 0.01 1.07 0.79	8:14	1.16	15.35	2.95	0.11	1.07	1.15	15.37	2.90	0.14	1.09	1.23		1.16	
0.73 15.37 2.98 0.13 1.07 0.72 15.39 2.93 0.16 1.09 0.77 0.75 15.38 2.98 -0.02 1.05 0.74 15.40 2.93 0.01 1.07 0.79	8:15	0.57	15.36	9	0.1	1.11	0.56	15.38	2.95	0.13	1.13	09.0		1.21	
7 0.75 15.38 2.98 -0.02 1.05 0.74 15.40 2.93 0.01 1.07 0.79	8.16	0.73	15.37	2.98	0.13	1.07	0.72	15.39	2.93	0.16	1.09	0.77		1.16	
	2 7	2,5	15.38	2.98	-0.02	1.05	0.74	15.40	2.93	0.01	1.07	0.79		1.14	

ı				1										, ro	'n	· vo	-	_	_	7	9	2	2	3	0	0	0	4	5	-	80	&	œ		.	4	7	2	2	9	S.	4	د	
ō.	Š N	as ppmv	NO2				1.13							1.15	1.15	1.15	1.1	1.1	1.1	1.17	1.16	1.12	1.12	1.13	1.10	1.10	1.10	1.14	1.15	1.1	1.08	1.08	1.08	1.07	1.09	1.14	1.1	1.15	1.15	1.16	1.15	1.14	1.13	1.14
corrected for O ₂	TGOC	as ppmv	± υ																																									
CO		ខ	ppmv				1.19							1.07	1.01	1.09	0.97	1.39	1.40	1.14	0.74	1.10	1.29	1.08	1.30	1.37	1.46	1.31	0.69	1.09	1.09	1.1	1.12	1.34	1.3	1.10	1.22	1.33	1.16	1.35	1.26	1.05	1.83	1.30
•	Ň	as ppmv	NO,	1.02	0.03	1.05191	1.04	1.00	1.08		Š	as ppmv	NO,	1.05	1.05	1.05	1.03	1.03	1.03	1.08	1.07	1.04	1.04	1.04	1.01	1.01	1.01	1.04	1.05	1.02	1.00	1.00	1.0	1.00	1.02	1.06	1.07	1.05	1.05	1.06	1.05	1.04	1.04	1.06
	TG 0C	as ppmv	r. S	0.36	0.17	1.01918	0.20	-0.04	0.28	ATA	760C	as ppmv	Ξ̈́	0.02	-0.04	0.05	0.04	0.01	0.18	0.22	0.22	0.22	0.22	0.24	0.23	0.23	0.25	0.22	0.23	0.20	0.22	0.21	0.22	0.21	0.22	0.21	0.23	0.24	0.26	0.26	0.26	0.28	0.28	0.26
		8	percent	2.84	0.03	0.99176	2.79	2.64	2.94	CORRECTED DATA		ŝ	percent	2.64	2.64	2.64	2.88	2.89	2.91	2.91	2.91	2.91	2.87	2.70	2.71	2.68	5.66	2.68	2.66	2.81	2.91	2.91	2.93	2.92	2.94	2.92	2.74	2.68	2.68	5.66	2.68	2.65	5.66	2.87
		o'	percent	15.41	0.13	1.01139	15.46	15.39	15.50	CORR		ò	percent	15.48	15.50	15.49	15.44	15.43	15.41	15.42	15.42	15.43	15.42	15.48	15.47	15.48	15.48	15.49	15.50	15.47	15.43	15.43	15.44	15.41	15.39	15.41	15.48	15.48	15.50	15.47	15.49	15.49	15.48	15.41
ata		8	ppmv	1.08	00.0	1.01099	1.09	0.63	1.68			8	ppmv	0.98	0.92	1.00	06'0	1.28	1.30	1.06	0.69	1.02	1.19	0.99	1.19	1.25	1.34	1.20	0.63	1.00	1.01	1.03	1.03	1.24	1.22	1.02	1.12	1.22	1.06	1.24	1.15	96.0	1.68	1.21
Emission Concentration Data				Raw Avg.:	Avg. Zero:	Corr. Factor:	Corr. Avg.:	Minimum:	Maximum:		χον	as ppmv	NO,	1.03	1.03	1.03	1.01	1.01	1.01	1.06	1.05	1.02	1.02	1.02	0.99	66.0	66.0	1.02	1 03	-	0.98	0.98	96.0	0.98	-	1.04	1.05	1.03	1.03	1.04	1.03	1.02	1.02	1.04
on Conce						ပိ	Ū				TGOC	as ppmv	c, H,	0.19	0.13	0.19	0.13	0.18	0.35	0.39	0.39	0.39	0.39	0.41	0.4	0.4	0.42	0.39	0.4	0.37	0.39	0.38	0.39	0.38	0.39	0.38	0.4	0.41	0.43	0.43	0.43	0.44	0.44	0.43
Emissi										RAW DATA		8	percent	2.69	2.69	2.69	2.93	2.94	2.96	2.96	2.96	2.96	2.92	2.75	2.76	2.73	2.71	2.73	2.71	2.86	2.96	2.96	2.98	2.97	2.99	2.97	2.79	2.73	2.73	2.71	2.73	2.7	2.71	2.92
			ion									o	percent	15.44	15.46	15.45	15.4	15.39	15.37	15.38	15.38	15.39	15.38	15.44	15.43	15.44	15.44	15.45	15.46	15.43	15.39	15.39	15.4	15.37	15.35	15.37	15.44	15 44	15.46	15.43	15.45	15.45	15.44	15.37
	02		erating Station	Outlet								ខ	ppmv	0.97	0.91	0.99	0.89	1.27	1.29	1.05	0.68	1.01	1.18	0.98	1.18	1.24	1.33	1.19	0.62	0.99	-	1.02	1.02	1.23	1.21	101	=======================================		1 5	3 5	3 -	- 0	1.55	1.2
	101494.1.004.02	ccsi	Gianera Generating	Gas Turbine Outlet	Daniel Neal	19-Jul-00	6	100			I	Time	24-Hr	8:51	8:52	8:53	8:54	8:55	8:56	8:57	8:58	8:59	9:00	9:01	9:05	9:03	9:04	9:05	90:6	9:07	90.6	60:6	9:10	9:11	9:12	9.13	0.5	0.10	2.0	0.10		, d	9.19	9.21
	Job No.	Client:	Plant:	Location:	Operator:	Date:	Run No.	Condition:																																				

							•																																						
0,	NOX	as ppmv	NO2				1.14							1.15	1.12	1.10	1.09	1.09	1.10	1.13	1.19	1.18	1.14	1.15	1.11	1.10	1.10	1.14	1.13	1.12	1.09	1.08	1.10	1.12	1.20	1.19	1.17	1.16	1.16	1.16	1.15	1.17	1.21	1.14	1.15
corrected for O ₂	TG0C	as ppmv	τς C																																										٠
CO		8	ppmv				1.91							1.95	1.59	1.92	2.05	2.22	2.38	2.67	1.58	1.64	1.95	2.15	2.16	2.35	2.45	1.79	1.36	1.75	1.91	2.13	2.48	2.46	1.43	1.39	1.70	1.90	1.81	1.80	2.22	1.92	1.04	1.50	1.53
	NO _X	as ppmv	NO,	1.03	0.03	1.04046	1.04	0.99	+.1		Ň	as ppmv	NO,	1.07	1.04	1.01	1.00	1.00	1.00	1.04	1.09	1.08	1.05	1.05	1.01	1.01	1.01	1.06	1.05	1.02	1.00	0.99	1.00	1.02	1.10	1.08	1.07	1.06	1.07	1.07	1.06	1.09	-	1.06	1.06
	TGOC	as ppmv	ı, Υ	0.32	0.20	1.02263	0.12	-0.12	0.34	ATA	TGOC	as ppmv	r L U	0.30	0.29	0.30	0.29	0.30	0.29	0.33	0.30	0.34	0.27	0.08	0.10	0.04	0.05	0.04	90.0	0.05	90.0	90.0	0.08	0.04	0.03	0.08	0.04	0.03	0.05	6 .04	0.05	90'0	-0.12	9.	0.04
		co	percent	2.83	0.01	0.98527	2.78	2.61	2.93	CORRECTED DATA		00	percent	2.89	2.90	2.93	2.91	2.86	2.82	2.63	2.65	2.61	2.63	2.64	2.66	2.79	2.88	2.88	2.89	2.90	2.85	2.86	2.63	2.63	2.67	2.65	2.63	2.65	2.75	2.89	2.87	2.87	2.87	2.91	2.86
		o'	percent	15.41	0.13	1.01310	15.48	15.44	cc.cr	COR		o'	percent	15.45	15.47	15.45	15.46	15.45	15.49	15.51	15.53	15.52	15.50	15.52	15.53	15.46	15.46	15.45	15.46	15.49	15.47	15.45	15.53	15.52	15.51	15.55	15.51	15.53	15.48	15.46	15.47	15.44	15.48	15.44	15.46
)ata		ខ	ppmv	1.71	-0.03	1.00996	1.76	0.95	2.44			8	bpmv	1.80	1.46	1.77	1.89	2.06	2.19	2.44	1.44	1.50	1.78	1.96	1.96	2.17	2.26	1.65	1.26	1.60	1.76	1.96	2.26	2.25	1.31	1.26	1.55	1.73	1.66	1.66	2.05	1.71	0.95	1.39	1.4
Emission Concentration Data			•	Raw Avg.:	Avg. Zero:	Corr. Factor:	Corr. Avg.:	Minimum:	maximum:		× O N	as ppmv	NO,	1.05	1.02	-	0.99	0.99	0.99	1.02	1.07	1.06	1.03	1.03	-	-	-	1.04	1.03	1.01	0.99	0.98	0.99	1.01	1.08	1.06	1.05	1.04	1.05	1.05	1.04	1.07	1.09	1.04	1.04
ion Conc						Ō					1 60c	as ppmv	±ູ່ ບໍ	0.49	0.48	0.49	0.48	0.49	0.48	0.52	0.49	0.53	0.46	0.28	0.3	0.24	0.25	0.24	0.26	0.25	0.26	0.26	0.28	0.24	0.23	0.28	0.24	0.23	0.25	0.19	0.25	0.26	0.08	0.24	0.21
Emiss										RAW DATA		ပိ	percent	2.94	2.95	2.98	2.96	2.91	2.87	2.68	2.7	2.66	2.68	2.69	2.71	2.84	2.93	2.93	2.94	2.95	2.9	2.91	2.68	2.68	2.72	2.7	2.68	2.7	2.8	2.94	2.92	2.92	2.92	2.96	2.91
			ation									o'	percent	15.38	15.4	15.38	15.39	15.38	15.42	15.44	15.46	15.45	15.43	15.45	15.46	15.39	15.39	15.38	15.39	15.42	15.4	15.38	15.46	15.45	15.44	15.48	15.44	15.46	15.41	15.39	15.4	15.37	15.41	15.37	15.39
	4.02		nerating Station	• Outlet								8	ppmv	1.76	1.42	1.73	1.85	2.01	2.14	2.39	4.	1.46	1.74	1.92	1.92	2.12	2.21	1.61	1.22	1.56	1.72	1.92	2.21	2.2	1.27	1.22	1.51	1.69	1.62	1.62	2	1.73	0.92	1.35	1.37
	101494.1.004.02	ccsi	Gianera Genera	Gas Turbine Outlet	Daniel Neal	19~Inl~00	9	100		•	i	Time	24-Hr	11:21	11:22	11:23	11:24	11:25	11:26	11:27	11:28	11:29	11:30	11:31	11:32	11:33	11:34	11:35	11:36	11:37	11:38	11:39	11:40	11:41	11:42	11:43	11:44	11:45	11:46	11:47	11:48	11:49	11:50	11:51	11:52
	Job No.		Plant:	Location:	Operator:	Date:	Run No.	Condition:												٠																									

1		>		1			2							5	13	<u>-</u>	_	0	0	4	7	. 67	-	. 0	80	œ	9	7	5	e	4	8	_	2	4	7	-	0	ō.	ġ.	0	4	7	3	-
0,	NOx	as ppmv	NO ₂				1.12							1.15	1.13	1.11	1.11	1.10	1.10	1.14	1.17	1.13	=	1.1	1.08	1.08	1.09	1.17	1.15	1.13	1.14	1.13	Ξ.	1.12	1.14	1.17	. .	1.10	1.09	1.09	1.10	1.14	1.1	1.13	-
corrected for O ₂	TGOC	as ppmv	r. S																																										
COL		8	bpmv				1.88							1.35	1.56	2.02	2.10	2.26	2.31	2.44	1.39	1.57	1.91	1.79	2.02	2.28	2.36	1.50	1.55	1.71	1.71	1.73	1.88	2.03	1.73	1.06	1.38	1.66	1.89	2.15	2.53	2.57	1.49	1.97	2.20
	Ň	as ppmv	NO ₂	1.02	0.01	1.02661	1.04	1.01	1.09		Ň	as ppmv	NO ₂	1.07	1.05	1.03	1.02	1.01	1.02	1.05	1.08	1.05	1.03	1.02	1.01	1.01	1.02	1.08	1.06	1.04	1.04	1.04	1.02	1.03	1.06	1.09	1.04	1.02	1.02	1.02	1.02	1.05	1.08	1.04	1.02
	TGOC	as ppmv	G,H	0.23	90.0	1.02483	0.18	0.04	0.25	ATA	TGOC	as ppmv	c, T,	0.19	0.17	0.24	0.19	0.18	0.18	0.19	0.18	0.20	0.14	0.15	0.16	0.17	0.14	0.16	0.17	0.15	0.22	0.16	0.24	0.20	0.19	0.16	0.20	0.18	0.13	0.14	0.15	0.15	0.25	0.04	0.23
		°CO	percent	2.80	0.13	1.07117	2.86	2.71	3.05	CORRECTED DATA		ç Ç	percent	3.01	2.91	2.74	2.72	2.72	2.71	2.74	2.75	2.92	3.01	3.03	3.05	2.99	2.99	2.90	2.75	2.72	2.73	2.73	2.74	2.77	2.90	2.99	2.98	2.98	2.98	2.97	2.95	2.73	2.77	2.75	2.74
		°	percent	15.43	0.09	1.00756	15.46	15.40	15.51	CORF		°	percent	15.42	15.44	15.46	15.49	15.49	15.47	15.49	15.48	15.43	15.44	15.44	15.40	15.42	15.41	15.46	15.49	15.49	15.51	15.49	15.50	15.48	15.41	15.42	15.41	15.43	15.41	15.40	15.43	15.50	15.47	15.50	15.49
ata		0	ppmv	1.69	-0.03	1.00656	1.73	0.99	2.36			8	ppmv	1.26	1.44	1.86	1.92	2.07	2.12	2.23	1.28	1.46	1.77	1.66	1.88	2.11	2.19	1.38	1.42	1.57	1.56	1.59	1.72	1.86	1.61	0.99	1.29	1.54	1.76	2.00	2.35	2.36	1.37	1.80	2.01
Emission Concentration Data				Raw Avg.:	Avg. Zero:	Corr. Factor:	Corr. Avg.:	Minimum:	Maximum:		ΝΟχ	as ppmv	NO,	1.05	1.03	1.01	-	0.99	-	1.03	1.06	1.03	1.01	-	0.99	0.99	-	1.06	1.04	1.02	1.02	1.02	-	1.01	1.04	1.07	1.02	-	-	-	-	1.03	1.06	1.02	-
on Conc						Ö				A	TGOC	as ppmv	τ΄ Ό	0.25	0.23	0.29	0.25	0.24	0.24	0.25	0.24	0.26	0.2	0.21	0.22	0.23	0.5	0.22	0.23	0.21	0.27	0.22	0.29	0.26	0.25	0.22	0.26	0.24	0.19	0.2	0.21	0.21	0.3	0.1	0.28
Emissi										RAW DATA		00	percent	2.94	2.85	2.69	2.67	2.67	2.66	2.69	2.7	2.86	2.94	2.96	2.98	2.92	2.92	2.84	2.7	2.67	2.68	2.68	2.69	2.72	2.84	2.92	2.91	2.91	2.91	2.9	2.88	2.68	2.72	2.7	2.69
			tion									°	percent	15.39	15.41	15.43	15.46	15.46	15.44	15.46	15.45	15.4	15.41	15.41	15.37	15.39	15.38	15.43	15.46	15.46	15.48	15.46	15.47	15.45	15.38	15.39	15.38	15.4	15.38	15.37	15.4	15.47	15.44	15.47	15.46
	.02		erating Sta	Outlet								ပ	ppmv	1.22	4.	1.82	1.88	2.03	2.08	2.19	1.24	1.42	1.73	1.62	1.84	2.07	2.15	1.34	1.38	1.53	1.52	1.55	1.68	1.82	1.57	0.95	1.25	15	1 72	1 96	23	231	1.33	1.76	1.97
	101494.1.004.02	ccsi	Gianera Generating Station	Gas Turbine Outlet	Daniel Neal	19-Jul-00	7	100			I	Time	24-Hr	12:31	12:32	12:33	12:34	12:35	12:36	12:37	12:38	12:39	12:40	12:41	12:42	12:43	12:44	12:45	12:46	12:47	12:48	12:49	12:50	12:51	12:52	12:53	12:54	12:55	12:56	12:57	12:58	12:59	13.00	13:01	13:02
	Job No.	Clent:	Plant:	Location:	Operator:	Date:	Run No.	Condition:																																					

			Emiss	ion Conc	Emission Concentration Data	Jata				'	còri	corrected for O ₂	0,
101494.1.004.02									1600	ŏ N		1000	Š
;	,					ဗ	o'	8	as ppmv	as ppmv	ဗ	as ppmv	as ppmv
Gianera Generating Station	ation				•	ppmv	percent	percent	c, H	NO,	ppmv	C,H,	NO,
Gas Turbine Outlet					Raw Avg.:	1.28	15.43	2.79	0.22	1.02			
					Avg. Zero:	-0.05	0.08	0.23	0.04	0.01			
					Corr. Factor:	1.00521	1.00883	1.15992	1.02662	1.02714			
					Corr. Avg.:	1.34	15.49	2.97	0.19	1.04	1.46		1,13
					Minimum:	0.80	15.43	2.82	0.14	0.99			
	-				Maximum:	1.99	15.54	3.14	0.26	1.1			
α.	۳	α	RAW DATA				COR	CORRECTED DATA	DATA				
				TG 0C	NOX				760C	Š			
ó			ဝွ	as ppmv	as ppmv	8	o'	00	as ppmv	as ppmv			
percent		•	percent	ည် သ	NO.	hpmv	percent	percent	ς Έ	NO,			
	15.42		2.94	0.23	1.01	1.51	15.48	3.14	0.20	1.03	1.65		1 13
1.42 15.41	15.41		2.71	0.29	1.03	1.47	15.47	2.88	0.26	1.05	1.60		7 7
	15.48		2.67	0.27	-	1.78	15.54	2.83	0.24	1.02	1.96		
	15.46		2.66	0.27	1.01	1.67	15.52	2.82	0.24	1.03	1.83		7
•	15.45		2.7	0.23	1.02	1.94	15.51	2.87	0.20	1.04	2.12		
_	15.47		5.69	0.23	1.08	1.36	15.53	2.85	0.20	1	1 20		? ;
0.89 15.44	15.44		2.68	0.25	1.09	0.94	15.50	2.84	0.22				17.1
1.05 15.45	15.45		2.73	0.22	1.07	1.10	15.51	2.90	9	9	5 5		17.
_	15,39		2.92	0.2	1.05	1.04	15.45	3.13	44	4 67	7.		בי. פריי
	15.37		2.94	0.22	1.04	1.00	15.43	3 14		90.	2 6		ę ;
1.06 15.4	15.4		2.91	0.21	1.04	1.1	15.46	. F.	18	9. 1	2 5		1.14
1.2 15.4	15.4		2.9	0.21	1.03	1.25	15.46	3.10	18	105	136		: ;
-	15.39		2.9	0.19	1.04	1.23	15,45	3.10	0.16	1.06	133		
	15.41		2.92	0.17	1.05	1.25	15.47	3.12	0.14	1.07	1.36		1.16
•	15.43		2.78	0.19	1.08	0.80	15.49	2.96	0.16	1.10	0.87		120
	15.46		2.68	0.24	1.05	0.85	15.52	2.84	0.21	1.07	0.93		1.17
1.01 15.46	15.46		2.69	0.22	1.03	1.06	15.52	2.85	0.19	1.05	1.16		1.15
1.01 15.47	15.47		2.69	0.18	1.02	1.06	15.53	2.85	0.15	1.04	1.16		1.14
1.26 15.47	15.47		2.72	0.2	0.99	1.31	15,53	2.89	0.17	1.01	1.44		1.1
1.43 15.47	15.47		2.68	0.23	0.98	1.48	15.53	2.84	0.20	1.00	1.63		1.09
	15.45		2.7	0.22	0.97	1.96	15.51	2.87	0.19	0.99	2.14		1.08
•	15.41		2.89	0.21	1.02	1.37	15.47	3.09	0.18	1.	1.49		1.13
	15.39		2.92	0.2	1.04	0.99	15.45	3.12	0.17	1.06	1.07		1.14
1 29 15.4	15.4		2.91	0.22	0.99	1.34	15.46	3.11	0.19	1.01	1.45		1.09
•	15.41		2 89	0.0	0.98	1.45	15.47	3.09	0.17	1.00	1.58		1.08
_	7 1		9 6	100	86.0	1.45	15 46	3.11	0.18	1.00	1.57		1.08
	0. 1		6.0	2.0	98 0	1.56	15.46	3.44	0.48	1.00	1.69		1.08
	10.4		2.3	70.0	0.00	1.73	45.50	200	0 24	6	1 88		1.08
1.67 15.44	15.44		7.93	0.27	6.0	7/1	2.5	5 6		6.5			
1.93 15.45	15.45		2.69	0.23	0.99	1.99	15.51		0.20	P. 4	71.7		2.5
_	15.48		2.69	0.23	1.02	1.32	10.04	C . C	0.20	3 3	 		
_	15.47		2.69	0.22	1.02	0.97	15.53	2.83	9.0	50. F	90.1		<u>.</u>
_	15.45		2.69	0.23	0.99	1.39	15.51	2.85	0.20	1.01	1.52		1.10

B.4 Turbine Process Data

				Catalyst					
			Catalyst inlet	outlet temp.,	Discharge	Discharge	Exhaust gas	Electrical	Fuel flow
Date	Time	Inlet temp, F	temp., F	LL.	pressure, psi	temp., F	temp., F	power, kW	rate, lb/hr
7/18/00	08:20:00	62	968	1557	132	672	981	1379.1	936.8
7/18/00	08:21:00	62	968	1555	132	672	981	1381.9	937.2
7/18/00	08:22:00	62	896	1557	132	672	981	1384.6	939.4
7/18/00	08:23:00	62	896	1563	132	672	981	1385.5	940.7
7/18/00	08:24:00	62	894	1557	132	672	981	1384.4	937.2
7/18/00	08:25:00	62	894	1557	132	672	981	1379.2	940.1
7/18/00	08:26:00	62	895	1557	132	672	981	1380.9	939.4
7/18/00	08:27:00	62	895	1555	132	672	981	1382.1	938.8
7/18/00	08:28:00	62	895	1555	132	672	981	1380.7	940.1
7/18/00	08:29:00	64	895	1557	132	672	981	1378.7	940.4
7/18/00	08:30:00	64	895	1557	132	672	981	1379.2	938
7/18/00	08:31:00	64	895	1561	132	672	981	1375.9	938.3
7/18/00	08:32:00	64	895	1557	132	672	981	1375.3	937.3
7/18/00	08:33:00	64	895	1557	132	672	981	1375.3	938.1
7/18/00	08:34:00	62	895	1555	132	672	981	1378.5	934.8
7/18/00	08:35:00	64	897	1557	132	674	981	1378.9	936.5
7/18/00	08:36:00	64	897	1555	132	672	981	1376.8	935.7
7/18/00	08:37:00	64	895	1557	132	674	981	1377.9	939.1
7/18/00	08:38:00	64	897	1559	132	672	981	1372.4	939.9
7/18/00	08:39:00	64	895	1559	132	672	981	1371.2	937.1
7/18/00	08:40:00	64	895	1557	132	674	981	1371.1	934.3
7/18/00	08:41:00	64	895	1557	132	674	981	1369.8	935.6
7/18/00	08:42:00	64	895	1555	130	674	981	1369	936.9
7/18/00	08:43:00	64	895	1555	130	674	981	1370.4	936.6
7/18/00	08:44:00	64	895	1555	130	674	981	1368.2	935.6
7/18/00	08:45:00	64	895	1555	130	674	983	1371.3	935.4
7/18/00	08:46:00	64	897	1559	130	674	981	1368.4	933.8
7/18/00	08:47:00	64	895	1561	130	674	981	1369.3	935
7/18/00	08:48:00	64	895	1557	130	674	981	1369.4	933
7/18/00	08:49:00	64	895	1557	130	674	981	1374.9	936.5
7/18/00	08:50:00	64	895	1557	130	674	981	1371.7	938.7
7/18/00	08:51:00	64	895	1555	130	674	981	1374.4	936.8
7/18/00	08:52:00	64	895	1557	130	674	983	1369.1	933.2
verages:		63.4	895.3	1557	131.3	672.9	981.1	1375.6	937.2

(İ	: :	Catalyst inlet	Catalyst outlet	Discharge .	Discharge	Exhaust gas	Electrical	Fuel flow
Date	Time	Inlet temp, F	temp., F	temp., F	pressure, psi	temp., F	temp., F	power, kw	rate, ID/nr
7/18/00	09:30:00	49	968	1556	130	674	983	1362.8	933.4
7/18/00	09:31:00	64	896	1556	130	674	983	1359.5	931.9
7/18/00	09:32:00	64	896	1558	130	674	983	1366.7	937.1
7/18/00	09:33:00	64	896	1560	130	674	983	1367.8	934.1
7/18/00	09:34:00	64	896	1560	130	674	983	1366.3	934.4
7/18/00	09:35:00	64	894	1556	130	674	981	1363.9	934.1
7/18/00	09:36:00	64	968	1556	130	674	983	1364.2	931.3
7/18/00	09:37:00	64	896	1556	130	674	983	1361.9	931.2
7/18/00	09:38:00	64	896	1556	130	674	983	1361.6	932.4
7/18/00	09:39:00	64	968	1556	130	674	983	1363.8	935.1
7/18/00	09:40:00	64	896	1556	130	674	983	1362.7	930.6
7/18/00	09:41:00	99	896	1560	130	674	983	1361.5	932.9
7/18/00	09:42:00	99	896	1562	130	674	983	1362.9	931.6
7/18/00	09:43:00	99	896	1558	130	674	981	1356.9	932.7
7/18/00	09:44:00	99	896	1556	130	674	983	1360.7	931.3
7/18/00	09:45:00	99	896	1558	130	929	983	1360.9	930.5
7/18/00	09:46:00	99	895	1556	130	929	983	1363.9	935.1
7/18/00	09:47:00	99	897	1556	130	9/9	983	1359.5	935.1
7/18/00	09:48:00	99	895	1556	130	929	983	1362.1	931.2
7/18/00	09:49:00	99	895	1558	130	929	983	1362.1	934.6
7/18/00	09:50:00	99	895	1564	130	674	983	1362	934.5
7/18/00	09:51:00	99	895	1556	130	9/9	981	1357.3	929.2
7/18/00	09:52:00	99	897	1558	130	9/9	983	1350.1	931.1
7/18/00	09:53:00	99	895	1558	130	929	983	1356	930
7/18/00	09:54:00	99	895	1556	130	929	983	1356.7	931.3
7/18/00	09:55:00	99	897	1558	130	929	983	1354.1	932.2
7/18/00	09:56:00	99	895	1558	130	9/9	983	1351.5	927.8
7/18/00	09:57:00	99	895	1558	130	929	985	1350.7	926.3
7/18/00	09:58:00	99	897	1564	130	9/9	983	1353.1	931.4
7/18/00	09:59:00	99	895	1558	130	929	983	1353	932.2
7/18/00	10:00:00	99	897	1558	130	9/9	983	1347.4	929.3
7/18/00	10:01:00	99	895	1558	130	929	983	1346.5	928.4
7/18/00	10:02:00	99	897	1558	130	9/9	983	1344.2	926.5
Averages:		65.3	895.8	1557.8	130	675.0	982.9	1358.6	931.8

			Catalvet inlet	Catalyst	Discharge	Discharge	Exhaust das	Electrical	Fuel flow
Date	Time	Inlet temp, F	temp., F	Н	pressure, psi	temp., F	temp., F	power, kW	rate, lb/hr
7/18/00	16:15:00	78	904	1561	126	989	993	1254	896.1
7/18/00	16:16:00	78	904	1562	126	989	993	1248.2	897.2
7/18/00	16:17:00	78	904	1568	126	989	993	1257.1	891.6
7/18/00	16:18:00	78	904	1566	126	989	993	1243.1	892.2
7/18/00	16:19:00	78	904	1564	126	989	993	1242.1	892.5
7/18/00	16:20:00	78	906	1564	126	688	993	1245.8	890.3
7/18/00	16:21:00	78	904	1564	126	688	993	1245.5	893
7/18/00	16:22:00	78	904	1562	.126	688	993	1243.4	895.3
7/18/00	16:23:00	78	904	1562	126	989	995	1247.3	894.1
7/18/00	16:24:00	78	904	1562	126	989	993	1248.6	894.5
7/18/00	16:25:00	9/	904	1564	126	989	993	1252.3	893.5
7/18/00	16:26:00	9/	904	1568	126	989	993	1244.9	895.2
7/18/00	16:27:00	78	904	1562	126	989	993	1244.4	892.7
7/18/00	16:28:00	78	904	1562	126	989	993	1242.8	898.6
7/18/00	16:29:00	78	902	1562	126	989	995	1246	896.3
7/18/00	16:30:00	78	904	1562	126	989	993	1243.7	892.6
7/18/00	16:31:00	78	902	1560	126	989	993	1247.5	898.6
7/18/00	16:32:00	78	902	1560	126	989	995	1247.7	895.5
7/18/00	16:33:00	78	904	1564	126	989	993	1247.8	897.7
7/18/00	16:34:00	78	905	1564	126	989	993	1247	897.4
7/18/00	16:35:00	78	902	1560	126	989	993	1245.9	895
7/18/00	16:36:00	78	902	1560	126	989	993	1242.6	893.7
7/18/00	16:37:00	78	902	1560	126	989	995	1243.5	891.9
7/18/00	16:38:00	78	006	1560	126	688	995	1245	893.6
7/18/00	16:39:00	78	903	1562	126	989	982	1247.7	895.7
7/18/00	16:40:00	78	903	1562	126	989	995	1241.9	896.7
7/18/00	16:41:00	78	903	1564	126	989	966	1247.2	968
7/18/00	16:42:00	78	901	1564	126	989	993	1244.5	895.5
7/18/00	16:43:00	78	901	1560	126	989	993	1241.5	892.3
7/18/00	16:44:00	78	901	1560	126	989	993	1242.5	892.5
7/18/00	16:45:00	78	903	1562	126	688	993	1240.9	893.8
7/18/00	16:46:00	78	903	1560	126	688	995	1244	894.1
7/18/00	16:47:00	78	903	1560	126	688	995	1244.2	890.4
Averages:		6.77	903.1	1562.3	126	686.4	993.6	1245.8	894.4

				Catalyst					
			Catalyst inlet	outlet temp.,	Discharge	Discharge	Exhaust gas	Electrical	Fuel flow
Date	Time	Inlet temp, F	temp., F	ட	pressure, psi	temp., F	temp., F	power, kW	rate, lb/hr
7/18/00	18:00:00	78	906	1567	126	989	993	1244.1	890.5
7/18/00	18:01:00	78	906	1565	126	989	993	1240.6	890.7
7/18/00	18:02:00	78	906	1567	126	989	995	1244	894.2
7/18/00	18:03:00	92	206	1567	126	989	993	1242.3	891.3
7/18/00	18:04:00	92	206	1567	126	989	995	1242.6	891.7
7/18/00	18:05:00	92	905	1567	126	989	995	1246.4	891.5
7/18/00	18:06:00	92	206	1566	126	989	995	1244.2	888.7
7/18/00	18:07:00	92	206	1570	126	989	995	1247.4	891.8
7/18/00	18:08:00	9/	905	1568	126	989	993	1246.5	892.4
7/18/00	18:09:00	92	905	1566	126	989	993	1240.6	892.8
7/18/00	18:10:00	78	902	1564	126	989	993	1244.5	9.068
7/18/00	18:11:00	78	902	1561	126	989	993	1241.6	891.9
7/18/00	18:12:00	78	902	1563	126	989	993	1244.4	893.1
7/18/00	18:13:00	78	902	1561	126	989	993	1246.4	892.8
7/18/00	18:14:00	78	006	1563	126	989	993	1250.7	895
7/18/00	18:15:00	78	006	1561	126	989	993	1247.3	895.1
7/18/00	18:16:00	78	006	1567	126	989	993	1250.3	894.9
7/18/00	18:17:00	92	006	1563	126	989	991	1251.7	894.7
7/18/00	18:18:00	78	006	1561	126	989	993	1243.1	890.7
7/18/00	18:19:00	78	006	1561	126	989	993	1244.6	893.2
7/18/00	18:20:00	78	006	1561	126	989	993	1245.1	891.3
7/18/00	18:21:00	78	006	1561	126	989	993	1247.5	892.9
7/18/00	18:22:00	9/	006	1561	126	989	993	1248.1	893
7/18/00	18:23:00	9/	006	1561	126	989	993	1249.1	893.5
7/18/00	18:24:00	9/	902	1567	126	989	993	1245.1	893.8
7/18/00	18:25:00	78	902	1565	126	989	993	1240.3	890.4
7/18/00	18:26:00	78	006	1563	126	989	993	1243.8	893.3
7/18/00	18:27:00	92	006	1563	126	989	993	1246	893.8
7/18/00	18:28:00	92	902	1561	126	989	993	1248.9	895.8
7/18/00	18:29:00	92	902	1561	126	989	993	1250	895.3
7/18/00	18:30:00	92	905	1561	126	989	993	1248.4	895.2
7/18/00	18:31:00	92	006	1561	126	989	993	1252.8	897
7/18/00	18:32:00	92	006	1565	126	989	993	1258.9	896.2
Averages:		77.0	902.5	1563.8	126	989	993.2	1246.3	893.0

	Fuel flow	rate, lb/hr	903.5	905.5	905.5	904.9	206	902.3	206	907.3	902.8	8.906	904.1	904.6	905.1	905.8	900.5	902.3	901.5	902	8.006	8.906	902.6	910.3	8.906	902	906.4	911.3	911.3	912.8	915.2	912.3	913.6	912.8	914.2	8.906
	Electrical	power, kW	1275.9	1275.1	1274.5	1277.9	1275.5	1272.8	1276.5	1278	1277.6	1279.5	1276.4	1273.7	1284.5	1284.1	1277.7	1280	1279.6	1278.7	1280.5	1279	1281.4	1286.4	1281.4	1281.8	1286.7	1286	1284.6	1286.3	1294.8	1293.5	1292.8	1292.3	1288.7	1281.6
	Exhaust gas	temp., F	991	686	686	991	991	686	686	686	686	991	991	991	991	686	686	686	686	686	686	686	686	686	987	686	686	686	686	686	686	286	286	286	286	989.1
	Discharge	temp., F	684	684	684	684	682	682	682	682	682	682	684	682	682	682	682	682	682	682	682	682	682	682	682	682	682	682	682	682	682	089	089	682	682	682.2
	Discharge	pressure, psi	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	126	128	128	128	128	128	128	128	128	126.5
Catalyst	outlet temp.,	ш	1558	1558	1558	1558	1562	1562	1560	1558	1558	1560	1562	1562	1562	1567	1563	1561	1561	1561	1561	1559	1559	1563	1559	1557	1559	1557	1557	1557	1561	1565	1559	1557	1557	1559.9
	Catalyst inlet	temp., F	868	868	868	968	968	894	896	968	968	968	006	006	006	006	006	905	006	006	902	006	006	898	968	896	968	896	896	896	868	868	896	896	896	897.8
		Inlet temp, F	74	74	74	74	74	74	72	72	72	72	74	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72.4
		Time	19:08:00	19:09:00	19:10:00	19:11:00	19:12:00	19:13:00	19:14:00	19:15:00	19:16:00	19:17:00	19:18:00	19:19:00	19:20:00	19:21:00	19:22:00	19:23:00	19:24:00	19:25:00	19:26:00	19:27:00	19:28:00	19:29:00	19:30:00	19:31:00	19:32:00	19:33:00	19:34:00	19:35:00	19:36:00	19:37:00	19:38:00	19:39:00	19:40:00	
		Date	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	7/18/00	Averages:

			Catalyst inlet	Catalyst	Discharge	Discharge	Exhaust das	Electrical	Fuel flow
Date	Time	Inlet temp. F	temp F	L	pressure, psi	temp., F	temp., F	power, kW	rate, lb/hr
7/19/00	06:50:00	09	895	1554	132	670	626	1398.6	949.6
7/19/00	06:51:00	09	895	1554	132	670	626	1397.4	945.8
7/19/00	06:52:00	09	897	1554	132	670	626	1396.4	945.9
7/19/00	06:53:00	90	895	1552	132	670	626	1397.4	946.2
7/19/00	06:54:00	09	895	1554	132	029	626	1398.8	947.7
7/19/00	06:55:00	09	895	1554	132	670	626	1400.4	945.3
7/19/00	06:56:00	09	897	1560	132	670	979	1397.3	945.3
7/19/00	06:57:00	09	895	1556	132	670	979	1397.6	946.7
7/19/00	06:58:00	09	895	1554	132	670	979	1395.6	945.7
7/19/00	06:59:00	09	895	1554	132	670	979	1400.2	948.4
7/19/00	00:00:20	09	895	1554	132	670	979	1393.9	947.4
7/19/00	07:01:00	09	895	1554	132	670	979	1398	944.6
7/19/00	07:02:00	09	895	1554	132	670	979	1395.9	944.2
7/19/00	07:03:00	09	897	1554	132	670	979	1393	944.1
7/19/00	07:04:00	09	895	1554	132	670	979	1397.6	942.9
7/19/00	07:05:00	09	897	1560	132	670	979	1397.1	944
7/19/00	00:90:20	09	897	1558	132	670	979	1392.7	944.2
7/19/00	07:07:00	09	897	1556	132	670	979	1394.9	946.3
7/19/00	07:08:00	09	895	1554	132	670	626	1393.2	946
7/19/00	00:60:70	09	896	1554	132	670	979	1397.5	943.4
7/19/00	07:10:00	9	896	1554	132	672	979	1394	939.8
7/19/00	07:11:00	90	896	1554	132	672	979	1393	945.3
7/19/00	07:12:00	9	896	1554	132	670	979	1394.2	945.5
7/19/00	07:13:00	90	896	1554	132	670	6/6	1397.6	942.9
7/19/00	07:14:00	09	896	1560	132	670	626	1395.6	943.2
7/19/00	07:15:00	09	896	1556	132	670	626	1392.6	942.8
7/19/00	07:16:00	9	896	1554	132	670	626	1392.8	939.2
7/19/00	07:17:00	9	896	1554	132	670	626	1392.5	946.2
7/19/00	07:18:00	90	896	1554	132	670	626	1391.5	939.6
7/19/00	07:19:00	90	896	1554	132	029	626	1389.6	943.7
7/19/00	07:20:00	90	968	1554	132	029	626	1394.3	942.2
7/19/00	07:21:00	90	968	1554	132	672	626	1394.5	941.7
7/19/00	07:22:00	62	968	1554	132	029	626	1390	939.4
Averages:		60.1	895.8	1554.8	132	670.2	926	1395.3	944.4

			1000	Catalyst	, C	, de 100 i C		Teo:ricol	Firel flow
ć	Ë		Catalyst Inlet	outlet temp.,	Discilarge	Discilarige form	LAlidusi yas	Liecuicai	rate lh/hr
Date	Ime	Inlet temp, F	temp., F	1_	pressure, psi	temp., r	temp., r	power, kw	rate, io/iii
7/19/00	07:55:00	62	897	1555	132	672	981	1383.1	935.8
7/19/00	07:56:00	62	897	1555	132	672	981	1385.1	6.986
7/19/00	07:57:00	62	897	1559	132	672	981	1386.3	937.9
7/19/00	07:58:00	62	895	1557	132	672	6/6	1383.3	937.8
7/19/00	07:59:00	62	897	1555	132	672	979	1380.7	938.3
7/19/00	08:00:00	62	895	1555	132	672	981	1384.3	937.6
7/19/00	08:01:00	62	895	1555	132	672	981	1381	936.9
7/19/00	08:02:00	62	897	1555	132	672	981	1381.8	938.6
7/19/00	08:03:00	62	968	1555	132	672	981	1382.6	936.5
7/19/00	08:04:00	62	968	1555	132	672	981	1378.3	936.2
7/19/00	08:05:00	62	968	1555	132	672	981	1381.1	935.9
7/19/00	08:06:00	62	896	1561	132	672	981	1382.3	939.4
7/19/00	08:07:00	62	896	1557	132	672	981	1379.4	940.5
7/19/00	08:08:00	62	896	1555	132	672	981	1376.7	934.7
7/19/00	08:09:00	62	896	1555	132	672	981	1379.4	937.6
7/19/00	08:10:00	62	896	1553	132	674	981	1373.1	938.6
7/19/00	08:11:00	62	896	1555	132	672	981	1379.7	938.5
7/19/00	08:12:00	62	896	1555	132	672	981	1380.8	942.5
7/19/00	08:13:00	62	968	1555	132	672	981	1380.7	936.2
7/19/00	08:14:00	64	896	1555	132	674	981	1379.7	937.5
7/19/00	08:15:00		896	1559	132	672	981	1379.3	937.4
7/19/00	08:16:00	62	894	1555	132	672	626	1377.4	936.1
7/19/00	08:17:00	62	896	1555	132	674	981	1378	939.3
7/19/00	08:18:00	62	968	1557	132	672	981	1375.6	936.7
2/19/00	08:19:00	62	968	1555	132	674	981	1375.4	937.1
7/19/00	08:20:00	64	894	1555	132	674	981	1373.5	939.4
7/19/00	08:21:00	64	968	1553	130	674	981	1373	935.2
7/19/00	08:22:00	64	868	1555	130	674	981	1375	936.9
7/19/00	08:23:00	64	896	1560	130	674	981	1377.1	939.6
7/19/00	08:24:00	64	968	1558	130	672	981	1374.1	936.3
7/19/00	08:25:00	64	968	1554	130	672	981	1371.9	935.3
7/19/00	08:26:00	64	968	1554	130	674	981	1370.3	934.3
7/19/00	08:27:00	64	968	1556	130	674	981	1374.4	938.4
Averages:		62.6	968	1555.7	131.6	672.6	8.086	1378.6	937.5

; ;	Fuel flow	rate, lb/hr	935.3	933.3	933.3	933.3	932.4	933.9	929.5	932.7	934.3	936.9	937.1	934.6	932.2	931.4	929.1	932.2	930.1	933	933.6	932.2	934.1	927.8	933.7	931	931.8	934	931.9	930.4	931	927.4	931.5	932.9	930.8	932.4
	Electrical	power, kW	1360.3	1359.5	1356.9	1358.2	1361.5	1361.2	1361.1	1360.8	1360.5	1358.6	1360.4	1360.6	1360.4	1361.2	1362.6	1358.8	1359.7	1354.3	1356.3	1353.8	1358	1359.6	1356.8	1349.3	1354.3	1353.2	1353.4	1351.6	1351.1	1348.2	1354.7	1349.5	1348	1356.8
	Exhaust gas	temp., F	981	983	983	983	983	983	983	981	983	983	983	983	983	983	983	983	981	983	983	983	983	983	983	983	983	983	983	983	983	983	983	983	983	982.8
	Discharge	temp., F	674	674	674	674	674	674	674	674	674	674	9/9	929	674	674	674	674	674	674	674	929	674	674	674	674	674	674	929	674	9/9	9/9	674	674	929	674.4
	Discharge	pressure, psi	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130	130
Catalyst	outlet temp.,	ட	1555	1555	1555	1555	1555	1555	1563	1555	1557	1553	1555	1555	1555	1553	1563	1555	1555	1555	1555	1553	1553	1553	1563	1555	1557	1555	1555	1555	1555	1555	1563	1555	1555	1555.8
	Catalyst inlet	temp., F	897	897	895	897	897	897	897	895	895	897	897	895	895	895	897	895	895	897	895	895	895	895	897	895	897	897	897	897	897	897	897	895	897	896.2
		Inlet temp, F	64	64	64	64	64	64	64	64	64	64	64	64	64	99	99	99	99	64	99	99	64	99	99	99	99	99	99	99	99	99	99	99	99	65.1
		Time	00:00:60	09:01:00	09:02:00	09:03:00	09:04:00	00:00:60	00:90:60	09:02:00	00:80:60	00:60:60	09:10:00	09:11:00	09:12:00	09:13:00	09:14:00	09:15:00	09:16:00	09:17:00	09:18:00	09:19:00	09:20:00	09:21:00	09:22:00	09:23:00	09:24:00	09:25:00	09:26:00	09:27:00	09:28:00	09:29:00	09:30:00	09:31:00	09:32:00	
		Date	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	7/19/00	verages:

				Catalyst					
			Catalyst inlet	outlet temp.,	Discharge	Discharge	Exhaust gas	Electrical	Fuel flow
Date	Time	Inlet temp, F	temp., F	ш	pressure, psi	temp., F	temp., F	power, kW	rate, lb/hr
7/19/00	11:30:00	72	868	1557	128	089	286	1304.9	910.5
7/19/00	11:31:00	72	896	1555	128	089	987	1304.8	912
7/19/00	11:32:00	72	896	1553	128	089	286	1307.1	912.5
7/19/00	11:33:00	72	868	1553	128	089	286	1305.6	914.8
7/19/00	11:34:00	72	868	1553	128	089	686	1307.2	909.4
7/19/00	11:35:00	72	868	1555	128	089	686	1300.4	806
7/19/00	11:36:00	72	868	1557	128	682	686	1305.5	910.5
7/19/00	11:37:00	72	896	1557	128	680	286	1304.9	906.3
7/19/00	11:38:00	72	868	1555	128	680	286	1303.1	906
7/19/00	11:39:00	72	868	1553	128	682	686	1294.2	6.806
7/19/00	11:40:00	72	868	1555	128	682	686	1301.6	907.3
7/19/00	11:41:00	72	868	1553	128	089	286	1302.1	6.706
7/19/00	11:42:00	72	868	1553	128	682	686	1302.8	912.8
7/19/00	11:43:00	72	868	1555	128	680	686	1302.7	206
7/19/00	11:44:00	72	868	1559	128	089	686	1300.9	908.7
7/19/00	11:45:00	72	868	1555	128	680	686	1297.4	910.2
7/19/00	11:46:00	72	868	1555	128	680	286	1300.9	6.606
7/19/00	11:47:00	72	868	1553	128	682	686	1299.1	906.1
7/19/00	11:48:00	72	868	1553	128	682	686	1297.2	908.3
7/19/00	11:49:00	72	868	1553	128	682	686	1304.7	910.4
7/19/00	11:50:00	72	868	1559	128	680	686	1308.4	910.5
7/19/00	11:51:00	72	868	1559	128	680	686	1300.4	908.1
7/19/00	11:52:00	72	868	1555	128	089	686	1299.7	904.5
7/19/00	11:53:00	72	868	1553	128	682	686	1293.1	006
7/19/00	11:54:00	72	006	1557	128	682	686	1296.2	906.5
7/19/00	11:55:00	72	006	1557	128	682	686	1298	9.906
7/19/00	11:56:00	72	006	1555	128	682	686	1292	904.6
7/19/00	11:57:00	72	006	1555	128	682	686	1298.6	905.7
7/19/00	11:58:00	72	006	1561	128	682	686	1301.4	903.8
7/19/00	11:59:00	72	868	1559	128	682	686	1297.7	903.5
7/19/00	12:00:00	74	006	1555	128	682	686	1296.6	906.2
7/19/00	12:01:00	72	006	1555	128	682	686	1298.4	904.9
7/19/00	12:02:00	72	006	1553	128	682	686	1292.8	908.4
Averages:		72.1	898.3	1555.3	128	681.0	988.5	1300.6	6.706

				Catalyst				: :	i I
			Catalyst inlet	outlet temp.,	Discharge	Discharge		Electrical	Fuel flow
Date	Time	Inlet temp, F	temp., F	L	pressure, psi	temp., F	temp., F	power, kW	rate, Ib/hr
7/19/00	12:40:00	. 92	896	1558	128	682	991	1282.4	904.6
7/19/00	12:41:00	9/	896	1554	128	682	686	1277.4	903.4
7/19/00	12:42:00	9/	868	1554	128	684	991	1276.5	904.1
7/19/00	12:43:00	92	868	1555	128	684	991	1279.5	901.6
7/19/00	12:44:00	92	868	1553	128	684	991	1283.5	905.7
7/19/00	12:45:00	74	898	1555	128	684	991	1282.9	902.9
7/19/00	12:46:00	74	868	1559	128	684	991	1281.2	901.2
2/19/00	12:47:00	74	868	1559	128	682	686	1282.7	902.4
7/19/00	12:48:00	74	896	1555	128	682	686	1277.7	902.7
7/19/00	12:49:00	74	868	1555	128	684	991	1280.1	8.906
7/19/00	12:50:00	74	868	1555	128	684	991	1281.3	900.1
7/19/00	12:51:00	74	868	1555	128	684	991	1283.4	901
7/19/00	12:52:00	92	868	1555	128	684	991	1279.8	898.7
7/19/00	12:53:00	92	868	1557	128	684	991	1284.6	9.868
7/19/00	12:54:00	9/	868	1559	126	684	991	1282	9.768
7/19/00	12:55:00	92	868	1553	126	684	686	1275.3	897.4
7/19/00	12:56:00	92	868	1555	126	684	991	1273.5	898.4
7/19/00	12:57:00	92	006	1557	126	684	991	1269.4	896.5
7/19/00	12:58:00	92	902	1559	126	684	991	1272.9	832.8
7/19/00	12:59:00	9/	006	1557	126	684	991	1274.5	899.4
7/19/00	13:00:00	9/	006	1557	126	684	993	1270.9	896.3
7/19/00	13:01:00	92	006	1563	126	684	991	1267.9	898.2
7/19/00	13:02:00	92	006	1559	126	684	991	1272.7	895.1
7/19/00	13:03:00	92	006	1557	126	684	991	1267.2	895.8
7/19/00	13:04:00	92	006	1555	126	684	991	1264.2	895.7
7/19/00	13:05:00	92	868	1555	126	989	993	1263.7	897.4
7/19/00	13:06:00		868	1555	126	989	993	1263.8	897.2
7/19/00	13:07:00		868	1555	126	989	993	1263.2	836.8
7/19/00	13:08:00	92	868	1560	126	684	991	1270.5	868
7/19/00	13:09:00	76	868	1556	126	684	991	1269.4	898.9
7/19/00	13:10:00	78	896	1554	126	684	991	1269.5	895.9
7/19/00	13:11:00	78	868	1554	126	684	991	1268.2	893.4
7/19/00	13:12:00	78	868	1554	126	684	991	1266.9	898.9
Averages:		75.8	898.3	1556.2	126.8	683.9	991	1274.5	899.3

				Catalyst	o do di O	وويرطمون	Total of Ass	Flootrical	Filel flow
Date	Time	Inlet temn F		outiet teimp., F	pressure psi	temp. F	temp. F	power. kW	rate. lb/hr
7/19/00	13:46:00	76	868	1554	126	684	991	1269.1	899.3
7/19/00	13:47:00	92	006	1556	126	684	991	1268.2	8.668
7/19/00	13:48:00	92	006	1556	126	684	991	1273.5	899
7/19/00	13:49:00	9/	868	1556	126	684	991	1273.8	898.9
2/19/00	13:50:00	9/	006	1558	126	684	993	1271.7	896.9
7/19/00	13:51:00	9/	006	1562	126	684	991	1275.4	2.006
7/19/00	13:52:00	92	006	1560	126	684	991	1267.2	896.1
7/19/00	13:53:00	9/	902	1560	126	684	991	1264.5	893.9
7/19/00	13:54:00	9/	904	1560	126	684	991	1270	898.2
7/19/00	13:55:00	9/	904	1560	126	989	991	1264.7	897.7
7/19/00	13:56:00	9/	904	1560	126	684	991	1267.4	894.7
7/19/00	13:57:00	92	904	1560	126	684	991	1268.8	896.7
7/19/00	13:58:00	9/	906	1562	126	684	993	1268.5	896.3
7/19/00	13:59:00	9/	904	1566	126	684	991	1269.9	896.6
7/19/00	14:00:00	92	904	1564	126	684	991	1268.8	897.6
7/19/00	14:01:00	9/	904	1562	126	684	991	1263.8	895.2
7/19/00	14:02:00	92	904	1560	126	684	991	1266.5	893.1
7/19/00	14:03:00	92	904	1558	126	989	991	1264.3	894.5
7/19/00	14:04:00	92	901	1558	126	684	991	1268.8	901.8
7/19/00	14:05:00	92	901	1556	126	684	991	1264.5	901
7/19/00	14:06:00	92	899	1558	126	684	993	1265.1	868
7/19/00	14:07:00	92	901	1560	126	684	991	1260.3	897.1
7/19/00	14:08:00	92	899	1558	126	684	991	1260	897.3
7/19/00	14:09:00	92	897	1556	126	684	991	1264.8	899.9
7/19/00	14:10:00	9/	897	1556	126	684	991	1266.1	898.4
7/19/00	14:11:00	92	897	1556	126	684	991	1265.3	907.2
7/19/00	14:12:00	78	897	1556	126	989	993	1260.3	900.4
7/19/00	14:13:00	78	897	1556	126	989	993	1263.5	901.4
7/19/00	14:14:00	78	897	1558	126	989	993	1261.2	899.3
7/19/00	14:15:00	78	897	1562	126	684	991	1266.2	901.4
7/19/00	14:16:00	78	897	1556	126	684	991	1259.8	896.2
7/19/00	14:17:00	78	897	1556	126	684	991	1266.9	902.5
7/19/00	14:18:00	78	897	1556	126	684	991	1262.5	901.5
Averages:		76.4	900.3	1558.5	126	684.3	991.4	1266.4	898.4



ZALCO LABORATORIES, INC. Analytical & Consulting Services

4309 Armour Avenue Bakersfield, California 93308 (661) 395-0539 FAX (661) 395-3069

Catalytica			Laboratory No:	0007332-1
430 Ferguson Driv Mountain View	CA 94043		Date Received:	07/24/2000
			Date Analyzed Purchase Order	07/26/2000
Attention:	Steve Stein		a dadame Other.	•
CC:			Date Reprinted:	07/26/2000
Sample Description			Test Code:	1635
Gas Sample #07]: Sampled 07/20/00	by Clicat (Clicat's Cylind	confirm timico ou 60 er)		
CHONS	Chromatographic Analysis,	ASTM D-1945-81, ASTM D-3	35 88-89, GPA 214:	5.94
Constituent	Norm Mol%	Norm Wi%	GPM	CHONS
			100	0.1
Oxygen	0.017	0.032		Carbon, C
Nitrogen	1311	2.189		12,54
				Hydrogen, H
Carbon Dioxide	0.653	1.713		23.90
Carbon Monoxide	0.000	0.000		-
				Oxygen, O
Methone	95.589	91.448		1.28
Ethane	2.231	4.001		
Propane Isoflutane	0.136	0.358	0.037	Nitrogen, N
racionarie s-Rotage	0.015 0.020	0.051	0.005	2.19
s-ociale IsoPertone	0.006	0.068	0.005	
n-Perrane	0.004	0.026 0.018	0.002	Salfar, S
Hexanes +	0.019	0.095	0.001 0.008	0.00
Teta's:	100,000	100.000	0.060	100.00
	ulated at STP: degrees F.	60.00		H/C Ratio:
Measurement Base	Pressure at STP: psia	14.696	<u> </u>	0.33
Gross Bhu/Cu Ft.,	Dry Gas HHV 1012.5	n blesson busin		
Ideal Gress Bout to	Dry Gas HHV 22873.4			0.5790
Net Bra/Cu.Ft	Dry Gus LHV 912.	-l overely, tree		0.5799 0.04428
ideal Net Bts/Lb	Dry Gas LHV 20610.5	***		22.5824
Gross BlacCu.Ft., v				0.9979
			Gross or HHV:	Net or LHV:
	"F" Facto		8519.4	9454.8
W. 21	T. / TFFICTO	r, DSCF/M/MBox at 68F.	8649.1	9598.8
<i>r</i> /1	1 Factor		8682.0	9635.2
im Etherton		or, DSCF CO2/MMBiu60F.	1004.1	11143
aborato y Operatio		or, DSCF CO2MMBto68F.	1019.4 O responsible for report of	1131.3

APPENDIX C

Equipment Calibration Results

- C.1 Calibration Gas Certifications
- C.2 Calibration Results of Ambient Measurement Equipment

C.1 Calibration Gas Certifications



Dual-Analyzed Calibration Standard

1290 COMBERMERE STREET, TROY, MI 48083

Phone: 248-589-2950

Fax: 248-589-2134

CERTIFICATE OF ACCURACY: EPA Protocol Gas

Assay Laboratory

TROY,MI 48083

P.O. No.:

043766

MIDWEST RESEARCH

SCOTT SPECIALTY GASES

Project No.: 05-60837-001

DAN NEAL

Customer

425 VOLKER BLVD

KANSAS CITY MO 64110

ANALYTICAL INFORMATION

1290 COMBERMERE STREET

This certification was performed according to EPA Traceability Protocol For Assay & Certification of Gaseous Calibration Standards;

Procedure #G1; September, 1997.

Cylinder Number:

ALM048090

Certification Date:

5/05/00

Exp. Date:

5/05/2002

Cylinder Pressure * * *:

1900 PSIG

ANALYTICAL

COMPONENT

CERTIFIED CONCENTRATION (Moles)

ACCURACY**

TRACEABILITY

NITRIC OXIDE

+/-1%

Direct NIST and NMi

NITROGEN - OXYGEN FREE

PPM BALANCE

TOTAL OXIDES OF NITROGEN

203.7

201.85

PPM

Reference Value Only

Product certified as +/- 1% analytical accuracy is directly traceable to NIST or NMI standards.

REFERENCE STANDARD

TYPE/SRM NO.

EXPIRATION DATE

CYLINDER NUMBER

CONCENTRATION

COMPONENT

NTRM 1683

4/03/03

ALM033297

48.90 PPM

NITRIC OXIDE

INSTRUMENTATION

INSTRUMENT/MODEL/SERIAL#

BECKMAN/951/010177

DATE LAST CALIBRATED

05/05/00

ANALYTICAL PRINCIPLE

CHEMILUMINESCENCE

ANALYZER READINGS

(Z = Zero Gas

R = Reference Gas

T = Test Gas

r = Correlation Coefficient)

First Triad Analysis

Second Triad Analysis

Calibration Curve

NITRIC OXIDE

Date:04/28/00	Response Unit:MV	
Z1 = 0.0000	R1 = 100.00	T1 = 80.300
R2 = 100.00	Z2 = 0.0000	T2=80.300
Z3 = 0.0000	T3 = 80.300	R3 = 100.00
Avg. Concentration:	201.5	РРМ

Date: 05/05/00	Response Unit: MV	
Z1 = 0.0000	R1 = 100.00	T1 = 80.700
R2 = 100.00	Z2 = 0.0000	T2 = 80.600
Z3 = 0.0000	T3 = 80.600	R3 = 100.00
Avg. Concentration	a: 202.2	PPM

Concentr	ation = A + Bx	+ Cx2 + Dx3 + Ex4
r = .9999	91	1685
Constant	s:	A =288709
B = 2.59	4606	C = -1.017189E-3
D =	0	E = 0

APPROVED BY:

151

^{***} Do not use when cylinder pressure is below 150 psig.

^{**} Analytical accuracy is based on the requirements of EPA Protocal procedure G1, September 1997.

COMPLIANCE CLASS



Dual-Analyzed Calibration Standard

1290 COMBERMERE STREET, TROY, MI 48083

Phone: 248-589-2950

Fax: 248-589-2134

CERTIFICATE OF ACCURACY: EPA Protocol Gas

Assay Laboratory

Customer

P.O. No.:

REPLACEMENT 040897 MIDWEST RESEARCH

SCOTT SPECIALTY GASES 1290 COMBERMERE STREET Project No.: 05-59909-001

425 VOLKER BLVD

TROY,MI 48083

KANSAS CITY MO 64110

ANALYTICAL INFORMATION

This certification was performed according to EPA Traceability Protocol For Assay & Certification of Gaseous Calibration Standards;

September, 1997.

Cylinder Number:

ALM007829

Certification Date:

3/30/00

Exp. Date:

3/30/2003

Cylinder Pressure ***:

2000 PSIG

ANALYTICAL

CERTIFIED CONCENTRATION (Moles)

ACCURACY**

TRACEABILITY

OXYGEN

COMPONENT

38.4

+/-2%

NIST and NMi

NITROGEN

BALANCE

REFERENCE STANDARD

TYPE/SRM NO.

EXPIRATION DATE

CYLINDER NUMBER

CONCENTRATION

COMPONENT

NTRM 2657

1/02/01

ALM032762

1.950 %

OXYGEN

INSTRUMENTATION

INSTRUMENT/MODEL/SERIAL#

DATE LAST CALIBRATED

ANALYTICAL PRINCIPLE

ROSEMOUNT/755R/1000430

03-30-00

PARAMAGNETIC

^{***} Do not use when cylinder pressure is below 150 psig.

^{••} Analytical accuracy is based on the requirements of EPA Protocal procedures , September 1997



Dual-Analyzed Calibration Standard

1290 COMBERMERE STREET, TROY, MI 48083

Phone: 248-589-2950

Fax: 248-589-2134

CERTIFICATE OF ACCURACY: EPA Protocol Gas

Assay Laboratory

TROY,MI 48083

P.O. No.:

RECERTIFICATION

Customer

MIDWEST RESEARCH

SCOTT SPECIALTY GASES

1290 COMBERMERE STREET

Project No.: 05-55275-003

425 VOLKER BLVD

KANSAS CITY MO 64110

ANALYTICAL INFORMATION

This certification was performed according to EPA Traceability Protocol For Assay & Certification of Gaseous Calibration Standards;

Procedure #G1; September, 1997.

Cylinder Number:

AAL19060

Certification Date:

12/20/99

Exp. Date: 12/19/2002

Cylinder Pressure ***:

0900 PSIG

ANALYTICAL

ACCURACY**

TRACEABILITY

CARBON DIOXIDE

COMPONENT

· CERTIFIED CONCENTRATION (Moles)

40.05

+/-1%

Direct NIST and NMi

NITROGEN

BALANCE

%

REFERENCE STANDARD

TYPE/SRM NO.

EXPIRATION DATE

CYLINDER NUMBER

CONCENTRATION

COMPONENT

NTRM 1675

1/01/03

ALM025157

13.96 %

CARBON DIOXIDE

INSTRUMENTATION

INSTRUMENT/MODEL/SERIAL#

DATE LAST CALIBRATED

ANALYTICAL PRINCIPLE

VARIAN/3400/10693

12/20/99

THERMAL CONDUCTIVITY

ANALYZER READINGS

(Z = Zero Gas

R = Reference Gas

T = Test Gas

r = Correlation Coefficient)

First Triad Analysis

Second Triad Analysis

Calibration Curve

CARBON DIOXIDE

Date:12/20/99	Response Unit:AREA	
Z1 = 0.0000	R1 = 96260.	T1 = 271904
R2 = 95297.	Z2 = 0.0000	T2 = 272106
Z3 = 0.0000	T3 = 271926	R3 = 95131.
Avg. Concentration:	40.06	%

Concentration = A + Bx + Cx2 + Dx3 + Ex4r = 0.999997 A = -0.05308458 B = 0.00014779 C = 0

APPROVED BY:

153

^{***} Do not use when cylinder pressure is below 150 psig.

^{**} Analytical accuracy is based on the requirements of EPA Protocal procedure G1, September 1997. Product certified as +/- 1% analytical accuracy is directly traceable to NIST or NMI standards.



Dual-Analyzed Calibration Standard

1290 COMBERMERE STREET, TROY, MI 48083

Phone: 248-589-2950

Fax: 248-589-2134

CERTIFICATE OF ACCURACY: EPA Protocol Gas

Assay Laboratory

P.O. No.:

043766

Customer

SCOTT SPECIALTY GASES 1290 COMBERMERE STREET Project No.: 05-60837-002

MIDWEST RESEARCH

DAN NEAL

425 VOLKER BLVD

TROY,MI 48083

KANSAS CITY MO 64110

ANALYTICAL INFORMATION

This certification was performed according to EPA Traceability Protocol For Assay & Certification of Gaseous Calibration Standards;

Procedure #G1; September, 1997.

Cylinder Number:

AAL17607

Certification Date:

5/02/00

Exp. Date:

5/02/2003

Cylinder Pressure ***:

1900 PSiG

COMPONENT

CERTIFIED CONCENTRATION (Moles)

ACCURACY**

TRACEABILITY

CARBON MONOXIDE

+/-1%

ANALYTICAL

Direct NIST and NMi

NITROGEN

199.8

PPM

BALANCE

Do not use when cylinder pressure is below 150 psig.

** Analytical accuracy is based on the requirements of EPA Protocal procedure G1, September 1997.

Product certified as +/- 1% analytical accuracy is directly traceable to NIST or NMI standards.

REFERENCE STANDARD

TYPE/SRM NO.

EXPIRATION DATE

CYLINDER NUMBER

CONCENTRATION

COMPONENT

NTRM 1681

3/01/03

ALM034513

977.1 PPM

CARBON MONOXIDE

INSTRUMENTATION

INSTRUMENT/MODEL/SERIAL#

DATE LAST CALIBRATED

ANALYTICAL PRINCIPLE

A1A/220-2/57297601

05/02/00

NDIR

ANALYZER READINGS

(Z = Zero Gas

R = Reference Gas

T = Test Gas

r = Correlation Coefficient)

First Triad Analysis

Second Triad Analysis

Calibration Curve

CARBON MONOXIDE

Date:04/24/00	Response Unit:NV	
21 = 0.0000	R1 = 100.00	T1 = 25.600
R2 = 100.00	Z2 = 0.0000	T2 = 25.600
23 = 0.0000	T3 = 25.600	R3 = 100.00
Avg. Concentration:	199.8	PPM

Date: 05/02/00	Response Unit: MV	
Z1 = 0.0000	R1 = 100.00	T1 = 25.500
R2 = 100.00	Z2 = 0.0000	T2 = 25.600
Z3 = 0.0000	T3 = 25.600	R3 = 100.00
Avg. Concentration	n: 199.8	PPM

Concentration = A + Bx + Cx2 + Dx3 + Ex4 r = .999997 A = .2123653 Constants: C = 2.034362E-2 B = 7.245147 D = 4.893673E-5 E = 0

APPROVED BY:

154



Dual-Analyzed Calibration Standard

1290 COMBERMERE STREET, TROY, MI 48083

Phone: 248-589-2950

Fax: 248-589-2134

CERTIFICATE OF ACCURACY: EPA Protocol Gas

Assay Laboratory

TROY,MI 48083

P.O. No.:

043766

Project No.: 05-60837-003

Customer

MIDWEST RESEARCH

DAN NEAL

425 VOLKER BLVD

KANSAS CITY MO 64110

ANALYTICAL INFORMATION

SCOTT SPECIALTY GASES

1290 COMBERMERE STREET

This certification was performed according to EPA Traceability Protocol For Assay & Certification of Gaseous Calibration Standards;

Procedure #G1; September, 1997.

Cylinder Number:

ALMG23230

Certification Date:

5/05/00

Exp. Date:

5/05/2003

Cylinder Pressure * * *:

2000 PSIG

ANALYTICAL

CERTIFIED CONCENTRATION (Moles)

ACCURACY**

TRACEABILITY

PROPANE

+/-1%

Direct NIST and NMi

NITROGEN

COMPONENT

190.6

PPM

BALANCE

- *** Do not use when cylinder pressure is below 150 psig.
- •• Analytical accuracy is based on the requirements of EPA Protocal procedure G1, September 1997.

Product certified as +/- 1% analytical accuracy is directly traceable to NIST or NMI standards.

REFERENCE STANDARD

TYPE/SRM NO.

EXPIRATION DATE

CYLINDER NUMBER

CONCENTRATION

COMPONENT

NTRM 1669

10/02/02

ALM025209

497.0 PPM

PROPANE

INSTRUMENTATION

INSTRUMENT/MODEL/SERIAL#

ANALYTICAL PRINCIPLE

VARIAN/1400/08982426

DATE LAST CALIBRATED 05/05/00

FLAME IONIZATION

ANALYZER READINGS

(Z = Zero Gas

R = Reference Gas

T = Test Gas

r = Correlation Coefficient)

Second Triad Analysis First Triad Analysis

Calibration Curve

PROPANE

Date:05/05/00 Response Unit:PPM Z1 = 0.0000R1 = 12960. T1 = 4978.1R2 = 12960. Z2 = 0.0000T2 = 4955.473 = 0.0000T3 = 4973.3R3 = 12960. 190.6 PPM Avg. Concentration:

Concentration = A + Bx + Cx2 + Dx3 + Ex4

r = 1.00000

Constants:

A = -5.236957E02

B = 3.835281E-02 C = 0

D = 0

E = 0

Scott Specialty Gases

RATA CLASS **Dual-Analyzed Calibration Standard**

1290 COMBERMERE STREET, TROY, MI 48083

Phone: 248-589-2950

Fax: 248-589-2134

CERTIFICATE OF ACCURACY: EPA Protocol Gas

Assay Laboratory

TROY,MI 48083

P.O. No.:

044167

Customer

MIDWEST RESEARCH

SCOTT SPECIALTY GASES 1290 COMBERMERE STREET

Project No.: 05-61970-002

425 VOLKER BLVD

KANSAS CITY MO 64110

ANALYTICAL

ANALYTICAL INFORMATION

This cartification was performed according to EPA Traceability Protocol For Assay & Certification of Gaseous Calibration Standards;

Procedure #G1; September, 1997.

Cylinder Number:

AAL7388

Certification Date:

6/01/00

Exp. Date:

6/01/2002

Cylinder Pressure * * *:

1900 PSIG

COMPONENT

CERTIFIED CONCENTRATION (Moles)

ACCURACY**

TRACEABILITY

NITRIC OXIDE

25.59 PPM

+/-1%

Direct NIST and NMi

NITROGEN - OXYGEN FREE

BALANCE

Reference Value Only

TOTAL OXIDES OF NITROGEN

25.7 PPM

** Analytical accuracy is based on the requirements of EPA Protocal procedure G1, September 1997. Product certified as 1/ 1% analytical occuracy is directly traceable to NIST or NMI standards.

REFERENCE STANDARD

TYPE/SRM NO.

EXPIRATION DATE

CYLINDER NUMBER

CONCENTRATION

COMPONENT

SHM 2629A

6/03/01

*** Do not use when cylinder pressure is below 150 psig.

CAL01C967

18.93 PPM

NITRIC OXIDE

INSTRUMENTATION

INSTRUMENT/MODEL/SERIAL#

HORIBA/OPE235/583956034

DATE LAST CALIBRATED 06/01/00

ANALYTICAL PRINCIPLE CHEMILUMENECENCE

ANALYZER READINGS

(Z = Zero Gas R = Reference Gas T = Test Gas

r = Correlation Coefficient)

First Triad Analysis

Second Triad Analysis

Callbration Curve

NITRIC OXIDE

Avg. Concentration:

Outs:05/22/00 41 - 0.00000

Response Unit:MV

H1 - 100,0000 T1 = 51.00000

25.58

RZ = 100.0000 ZZ = 0.00000

T2 - 60.70000

73 - 0.00000 T3 - 50.70000

83 = 100.0000

Date: 06/01/00 Response Unit: MV

Z1 = 0.00000 R1 = 100,0000 T1 = 50,90000

Z2 w 0.00000 T2 = 50.90000

T3 = 50.80000 23 = 0.00000R3 = 100.0000

Avg. Concentration:

25.59 PPM Concentration = A + 8x + Cx2 + Dx3 + Ex4

r= 1.0

Constants: A=0.001376

8-0.611783

C = -0.00017

2828A

D-0 E-0



Dual-Analyzed Calibration Standard

1290 COMBERMERE STREET, TROY, MI 48083

Phone: 248-589-2950

Fax: 248-589-2134

CERTIFICATE OF ACCURACY: EPA Protocol Gas

Assay Laboratory

P.O. No.:

Customer 044167

MIDWEST RESEARCH

SCOTT SPECIALTY GASES 1290 COMBERMERE STREET Project No.: 05-61970-001

425 VOLKER BLVD

KANSAS CITY MO 64110

TROY,MI 48083

ANALYTICAL INFORMATION

This certification was performed according to EPA Traceability Protocol For Assay & Certification of Gaseous Calibration Standards;

Procedure #G1; September, 1997.

Cylinder Number:

ALM055608

Certification Date:

6/01/00

Exp. Date:

6/01/2002

Cylinder Pressure ***:

1900 PSIG

ANALYTICAL

TRACEABILITY

COMPONENT NITRIC OXIDE CERTIFIED CONCENTRATION (Moles)

ACCURACY** +/- 1%

Direct NIST and NMi

NITROGEN - OXYGEN FREE

PPM 503.45

BALANCE

TOTAL OXIDES OF NITROGEN

PPM

Reference Value Only

the not use when cylinder pressure is below 150 psig.

Analytical accuracy is based on the requirements of EPA Protocal procedure G1, September 1997.

Freduct certified as +/ 1% analytical accuracy is directly traceable to NIST or NNII standards.

REFERENCE STANDARD

TYPE/SRM NO.

EXPIRATION DATE

CYLINDER NUMBER

CONCENTRATION

COMPONENT

N1BM 1686

2/01/03

AAL9242

495.3 PPM

NITRIC OXIDE

INSTRUMENTATION

HCCKMAN/951/010177

INSTRUMENT/MODEL/SERIAL#

DATE LAST CALIBRATED

ANALYTICAL PRINCIPLE

06/01/00

CHEMILUMINESCENCE

ANALYZER READINGS

(Z = Zero Gas

R = Reference Gas T = Test Gas

r = Correlation Coefficient:

First Triad Analysis

Second Triad Analysis

Calibration Curve

NITRIC OXIDE

Date:05/23/00 Response Unit:MV #1 = 10U.0000 21-0.00000

H2-100.0000 Z2=0.00000 13 - 49.80000 73 - 0.00000

T1-49.70000

Avg. Concentration:

503.3

T2 = 49,80000 A3 = 100.0000

Date: 06/01/00 Response Unit: MV

Z1 = 0.00000 R1 - 55.00000 T1 = 56.20000

92 = 55.00000 Z2 = 0.00000 23 - 0.00000 T3 = 65.90000

Avg. Concentration:

T2 - 55.80000 R3 = 56.00000

503.6

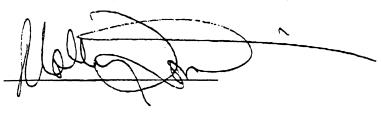
Concentration = A + Bx + Cx2 + Dx3 + Ex4

r = .999**99**7

A - 9.398621 Constants:

8 = -0.00699 C = 0

E = 0



C.2 Calibration Results of Ambient Measurement Equipment

ANEROID BAROMETER CALIBRATION CHECK

Location: Kansas City, Missouri

Altitude Above Sea Level: 850 feet

Latitude: 39° 05.8' north

Meteorological Gravity: 32.1551 feet/second²

Mercury Barometer Description: Sargent Welch, Cat. S-4519, Lot 791802000

I. New

MRI Project No. 101494.1.004.02

Date: 6/9/2000

Time: 07:15

Readings Obtained By: D. Neal

Observed Barometer Reading:

29.22 in. Hg

Mercury Column Temperature:

70 °F

Correction For Temperature:

-0.11 in. Hg

Correction For Gravity:

-0.02 in. Hg

Corrected Barometric Pressure:

29.09 in. Hg

Aneroid Barometer I.D. No.:

Y-2101

Reading Before Adjustment:

29.08 in. Hg

Calibration Check Result:

within 0.1 in. Hg

Reading After Adjustment:

99.08 in. Hg

Remarks:

BAROMETR.WK4 10/19/98 (rev. BAROMETR.WK4 06/09/2000 07:18 AM)

Code: MRI-0729 Revision: 0

Effective: 3/7/97 Page: 7 of 7

Hygrometer Calibration

mri # <u>Y-61</u>	<u>//7</u> - Mode	1 # Testo 61.	Serial #_	00267890)	
	Type: Digital					
	olution(s) used:					
1. Salt: <u>4</u> C	SÝÝ0-75 Date of prepa	aration: 12-3	-99 Approxim	ate Humidity:	//-3	
	cument: ASTM E					
2 Sale /2	CO3 Date of prepare	104-05 (1991	aa .	00, 01A, 09, 19	///.	
Ref. Doo	cument: ASTM E	104-85 (1991) 🕅 J. Res. NE	3S, 81A, 89, 19	77.	
3. Salt: 16	C/ 5440-89 C/ Date of prep	aration: 3-20-	<u>oo</u> Approxim	ate Humidity:_	75.4	
	cument: ASTM E					
	nermometer used:					
	0600 Serial #					
			Date last	certification	<u> </u>	
			_		•	
As Found:	Temperature: Hy	grometer = :	21-8°C 57):	= 218°C	Tolerance =	+ 0.4°C
Reference		Defense				
temperature	Temperature instability +	Reference		Urionomia	Hygrometer	
(°C)	uncertainty ^a	system humidity	uncertainty (incl. T-rel.)	Hygrometer reading	acceptance criteria	
229	+ 1,=	11.3	<1	/O. o	± 3	
22.6	+	43.2	<1	40.3	± 3	
226	/+ =	75.4	< 1	70.8	± 3	
	emperature: S	ne	•			i
22.9	+ =	11.3	<1	12.4	£3	
22-6	+ 1/1 =	43.2	<1	426	±3	
22-6	+ =	75.4	<1	73.8	±3	
Includes stated	e to accuracy limits of ref. uncertainty of the system umn (use linear interpolati	from the literature	plus uncertainties de	rived from the temp rom the literature).	erature	
This hygrome	eter 🔀 Passed	Failed	d Calibration.			
This hygrome	eter has been tagged					
Performed by	1: Dac Ip	10 N	Date:_6	-6-00		
Reviewed by	200		Date: 4	0/8/00		

Code: MRI-0701 Revision: 4 Effective: 6/25/99 Page: 12 of 12

Attachment 1 Instrument Found Out of Tolerance

Instrument: Digital Hygromoter Testo 615
Manufacturer: Cale Parmer
MRI Number: Y-6/17
Serial Number:
Acceptance Criteria: ± 3% RH
Date of calibration or test that revealed the out of tolerance condition: 10-6-00
Date of previous calibration: $10-26-99$
Responsible person: Neal (Must receive a copy of this report)
Tested/Calibrated by: Date: 6-6-00
Reviewed by: Date: 6/8/00
Comments/details of out of tolerance condition:
Hygrometer read 4.6% RH low at 75%
Hygrometer was adjusted to meet tolerance
I hereby certify that I have received a copy of this report and will notify the appropriate people and take the appropriate actions necessary to determine what data may have been corrupted and what corrective actions are indicated.
Signed: Mewer usen. Signed: Mewer usen.
Date: 6-8-00
NEW INSTRUMENT, NEVER USED.

Code: MRI-0729 Revision: 0 Effective: 3/7/97 Page: 7 of 7

Hygrometer Calibration

MRI #_ Y-	6118	Model #	# Testo 615	Serial #_	0031899C)		
Hygrometer type: Digital Manufacturer: Cole Parmer								
Reference Solution(s) used:								
1. Salt: 40 5440-75 Date of preparation: 12-3-99 Approximate Humidity: 11.3%								
Ref. Document: ASTM E 104-85 (1991) J. Res. NBS, 81A, 89, 1977.								
2. Salt: <u>k</u>	Salt: K2CO3 Date of preparation: 12-3-99 Approximate Humidity: 43.2							
Ref. Document: ☐ASTM E 104-85 (1991) ☑J. Res. NBS, 81A, 89, 1977.								
3. Salt: Na C/ Date of preparation: 3-20-00 Approximate Humidity: 75.4								
Ref. Document: ASTM E 104-85 (1991) J. Res. NBS, 81A, 89, 1977.								
Reference Thermometer used: 152(Accuracy: ±00/3°C								
MRI # <u>Y-6600</u> Serial # <u>98063</u> Date last Certification: <u>8-19-99</u>								
As Found: Temperature: Hygrometer = 22.2°C 5TD = 22.1°C Tolerance I C.								
			33	Reference				
Reference		1	Reference	system		Hygrometer		
temperature instability +		system	uncertainty	Hygrometer	acceptance			
	(°G) uncertainty ^a		hur Shiry	(inci. T-rel.) ^b	reading	criteria		
-225			11.3	<	12.9	±3		
22.5	+N/A	€	43.2	<	42.5	±3		
22.5	1	=	75.4	< /	73.2	±3		
As Left: Temperature: Same								
	+	=						
	+	=	SAME					
	+	=					1	
Uncertainty due to accuracy limits of ref. thermometer (in ±°C). Includes stated uncertainty of the system from the literature plus uncertainties derived from the temperature uncertainty column (use linear interpolation of the temperature/humidity tables from the literature).								
Calculation: WA								
This hygrometer Passed								
This hygrometer has been tagged.								
Performed by: Date: 66-00 Reviewed by: Date: 6/8/00								
Reviewed by: Date: 6/8/00								

MRI-QAVMRI-0729.DOC